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Toward a System Impairment Model

Ad hoc modelling committee: David Falconer, Carleton University Tom Kolze, Broadcom Yigal Leiba, Breezecom John Liebetreu, Sicom *With thanks also to:* Naftali Chayat, Breezecom Lucille Rouault, ENST/NIST Val Rhodes, Intel Benoit Verbaere, ENST/NIST

Process

- Identify primary performance degradation sources
- Model and parameterize these sources
- Establish performance metrics
- Establish baseline characterization techniques

Performance degradation sources

- Phase noise
- Power amplifier
- Multi-path
- Model parameters may be
 - Set by group and simulated by contributors
 - Stated and simulated by contributors

Phase noise assumptions

- <u>Purpose</u>: weighing sensitivity of different proposals to phase noise – not an interface specification
- Transmitter mmW up-converter and receiver mmW down-converter are expected to dominate phase noise
- Based on PLL-oscillator model

SSB phase noise PSD, L(f)



Phase noise model

- The model has four parameters
 - Corner frequency for crystal phase noise
 - Corner frequency for PLL loop
 - LO noise floor level
 - PLL phase noise level
- Two parameters for ease of simulation are a zero at 1Hz, and a pole at 100MHz
- To ease simulation, 1/f noise is not accounted for

Phase noise notes

- Thermal noise, discrete spurs and demodulator induced phase noise are **NOT** included in this model.
- Model is to be used for comparison purposes, **NOT** for precise performance evaluation

Power amplifier model

- Two model are proposed
 - Saleh model
 - Rapp model

Saleh model

- Characterize non-linearity in terms of AM/AM and AM/PM conversion functions
- Complex PA envelope is given by $Z = A(r) \cdot \exp\{j \cdot (\mathbf{y} + \mathbf{f}(r))\}$
- AM/AM conversion $A(r)=2r/(1+r^2)$
- AM/PM conversion $f(r)=2f_0\cdot r^2/(1+r^2)$
- A.A.M.Saleh "frequency-independent and frequency-dependant non-linear models of TWT amplifiers" IEEE trans. Commun. Vol COM-29, pp. 1715-1720, Nov 1981

Rapp model

• A family of saturation curves

$$v_{OUT} = v_{IN} / (1 + (|v_{IN}| / v_{SAT})^{2P})^{1/(2P)}$$

- Where $P_{SAT} = |v_{SAT}|^2$ is the saturated power of the amplifier (P=2)
- The performance metric is lowest backoff, where $Backoff = -10\log(Avg(|v_{OUT}|^2)/P_{SAT})$

Review of Channel Models and/or Measurements for mm-Wave Fixed Wireless Channels with Highly Directional Antennas

- Papazian et al. measurements in Northglen:
 - P.B. Papazian et al., "Study of the Local Multipoint Distribution Channel", IEEE Trans. Broadcasting, June 1997.
- ETSI/BRAN models:
 - ETSI/BRAN document HAPHY151TL03, "Channel model suitable for bands over 20 GHz", 21 Sept. 1999.
- 802.11 model adapted to BBW (N. Chayat):
 - "Some Models for Comparing PHY Proposals", N. Chayat, IEEE80216pc-YY/nn, Jan. 12, 2000
- CITR measurements in Ottawa:
 - "Multipath Measurements and Modelling for Fixed Broadband Wireless Systems in a Residential Environment", D. Falconer, IEEE80216pc-00/01, Dec. 20, 1999.

ETSI/BRAN



 $\phi = \pi (1-0.8(40 \text{ ns.})/T_{\text{symbol}}))$

Based on measurements in Europe by Telia

ETSI/BRAN (cont.) and Papazian



L7/Papazian:

 $\phi = \pi (1-0.8(20 \text{ ns.})/\text{T}_{\text{symbol}}))$



Adapted 802.11 Model



Suitable for:

•Low antennas/ non LOS with many incoming echoes

•Or wide antenna beams

Model Suggested in IEEE802.16tc-00-01

- Based on deviations of measured responses from their means.
- Echoes are zero-mean complex gaussian.



A Measured Kanata Response





A "Straw Man" Model



Time variation? -- slow compared to symbol rate

A "Straw Man" Model (cont.)



A=0.4, B=0.8 -π<ψ<π 0<τ<100 ns.