## Clause 162 Comments

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IEEE P802.3ck Task Force
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## Cable Assembly COM

Topic	Comments
Channel variables	124-129, 217-221, 230
eta0	69, 78, 11161
PN skew	204
Reference DFE	Minimum tap limits - 247 Span - 248 RSS limit - 240, 250
Package transmission line model	150
Units	151 (CC with 163.10 and 120F.4.1)

# COM

## Cable Assembly COM: Channel Variables

C#	SubClause	Description	
124	162.11.7.1.1	Channel: Change "host (transmitter or receiver)" to "host receiver" on p. 162.	
125	162.11.7.1.2	7.1.2 Change "S^(HOSP)" to "S^(HOSPR)" in Equation (162-13) and in p. 162 text.	
126	162.11.7.1.2	7.1.2 Change "S^(HOSP)" to "S^(HOSPR)" in Equation (162-14) and in p. 162 text.	
127	162.11.7.1.2 Change "S^(HOSPT)" to "S^(HOTxSP)" in Equation (162-13) and in p. 162 text.		
128	162.11.7.1.2	Change "S^(HOSPT)" to "S^(HOTxSP)" in Equation (162-14) and in p. 162 text.	
129	162.11.7.1.1	Remove extraneous "or" on p. 162.	
217	162.11.7.1.1	S(HOSPT) definition: Change to "is the host transmitter PCB signal path"	
218	162.11.7.1.1	S(HOSPR) definition: Change to "is the host receiver PCB signal path"	
219	162.11.7.1.1	.1 Change S(HSPT) to S(HOSPR) on p. 161.	
220	162.11.7.1.1	Change S(HSPT) to S(HOSPR) on p. 154, 162, 163.	
221	162.11.7.1.1	Change S(HSTxP) to S(HOSPT) on p. 162, line 49.	
230	162.11.7.1.1	Change wording of S(HOSPT) and S(HOSPR) definitions on p. 162	

See slides with marked up images.

### CA COM Channel

#### **Comments:**

124 125 126 127

128 129 217 218

219 220 221 230

230

transmitter's host PCB signal path receiver's host PCB signal path

Need to fix naming for NE and FE XTK S parameters

CAFXT CANXT

Was the intent in D1.2

D1.2 Page 162

220

162.11.7.1.2 Channel crosstalk paths

is equal to zero

 $S^{(HOSPT)}$ 

S(HOSPR)

 $S^{(CASP)}$ 

The MDI is the significant contributor to crosstalk and is included in and characterized by the cable assembly crosstalk measurements. Crosstalk includes a near-end path where the aggressor is the PMD transmitter, and in some cases, additional near-end, far-end, and alien far-end crosstalk paths where the aggressors are other PMD transmitters that are connected to the same cable assembly.

is the host transmitter er PCB signal path

is the host (transmitter or receiver) PCB signal path

is the cable assembly signal path (TP1 to TP4)

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For the channel crosstalk paths, the receiver PCB model is S(HOSP) as defined in 162.11.7.1.1. The aggressor S(HOSTxP) transmitter host PCB model is denoted as S(HOSPT) and is calculated from Equation (93A-13) and Equation (93A-14) using  $z_p = 110.3$  mm in length and the parameter values given in Table 162-17, representing an insertion loss of 4.33 dB at 26.56 GHz.

The scattering parameters of the channel near-end crosstalk paths are calculated using Equation (162–13). The scattering parameters of the channel alien far-end crosstalk paths are calculated using Equation (162–14).

$$SCHNXT_p^{(k)} = cascade(cascade(S^{(HOSPT)}, S^{(CANXTk)}), S^{(HOSP)})$$
 (162–13)

 $SCHNXT_p^{(k)}$  is the near-end crosstalk path

is the host receiver PCB signal path defined in 162.11.7.1.1

STXP is the aggressor transmitter PCB signal path

 $S^{(CANXIK)}$  is the cable assembly near-end crosstalk path k (TP1 to TP4) k is the index of the near-end crosstalk path

 $SCHAFXT_p^{(k)} = cascade(cascade(S^{(HOTxSP)}, S^{(CAFXTk)}), S^{(HOSPR)})$  126 219 220 (162–14)

where

where

## CA COM Channel (2)

01.2 Page 154	The scattering parameters of the test channel are measured at the test references as illustrated in Figure 110-3b using the cable assembly test fixtures specified in Annex 162B.1.	42 43
	The insertion loss at 26.56 GHz of the signal path between the test references in Figure 110–3b is within the limits in Table 162–13.  The COM is calculated using the method and parameters of 162.11.7 with the following considerations:	44 45 46 47 48
	<ul> <li>a) The channel signal path is SCHS<sub>p</sub> = cascade(S<sup>(CTSP)</sup>, S<sup>(HOSP)</sup>), where cascade() is defined in 93A.1.2.1, S<sup>(HOSP)</sup> is defined in 162.11.7.1.1, and S<sup>(CTSP)</sup> is the measured channel between the test references in Figure 110–3b.</li> <li>b) The COM parameters are as modified by Table 162–13.</li> </ul>	49 50 51 52 53
01.2 Page 161	The scattering parameters of the channel signal path from TP0 to TP5 are calculated using Equation (162–12). The transmitter and receiver PCB signal paths are denoted as $S^{(HOSTxP)}$ and $S^{(HOSP)}$ , and are calculated using Equation (162–12) and Equation (162–11), respectively. The PCB transmission line scattering parameters are denoted as $S^{(l)}$ and are calculated from Equation (93A–13) and Equation (93A–14) using $z_p$ =110.3 mm in length and the parameter values given in Table 162–17, representing an insertion loss of 4.33 dB at $S^{(HOSPR)}$	54 50 51 52 53 54
	$S^{(HOSPR)}$ 126	219
01.2 Page 163	is the host receiver PCB signal path defined in 162.11.7.1.1 $S^{(HOSPT)}$ is the aggressor transmitter PCB signal path	1
$127   S^{(HOSTx)}$		

## CA COM: $\eta_0$ (C# 69, 78, 11161)

• 07/19 Baseline: 8.20e-9 V<sup>2</sup>/GHz

• 01/20 Change: 1.0e-8 V<sup>2</sup>/GHz (Straw poll #10 & #11)

• 07/20 proposals:

C#	Proposed value	Referenced presentations
69	9e-9	lim_3ck_01a_1119 mellitz_3ck_03a_1119
78	8.37e-9	champion_3ck_adhoc_01_031120
11161	1e-9	

### Proposed response:

Reject. The current value was adopted based on results of straw polls #10 & 11 at the 01/2020 interim meeting. The comment provides evidence that some channels fail COM. However, having an interoperable link requires both pass cables and receivers, and both need to be addressed.

### C#204 PN Skew

- Proposed response: Reject
- Refer to the response to comment #206.
  - Same proposal for CL163.

CI 162 SC 162.11.7 P 159 L 34

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Status D

COM

COM receiver reference model does not excite common mode and model is fully symmetrical between P/N. Unless COM reference model has common mode excitation only differential aspect of the S4P exercised.

#### SuggestedRemedy

Comment Type TR

Non-idealities in COM can be introduced by following:

- -Termination mismatch P/N 3%
- Package P +/- 10%
- -Package N +/- 10%

But the total RLM should still be 95%.

Proposed Response Response Status W

PROPOSED REJECT

The proposed remedy does not provide a clear change to the draft.

C/ 163 SC 163.10 P 184 L 14

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status R COM parameter

COM receiver reference model does not excite common mode and model is fully symmetrical between P/N. Unless COM reference model has common mode excitation only differential aspect of the S4P exercised.

#### SuggestedRemedy

Non-idealities in COM can be introduced by following:

- -Termination mismatch P/N 3%
- Package P +/- 10%
- -Package N +/- 10%

But the total RLM should still be 95%.

Response Response Status C

REJECT

COM mode impairment is indeed not fully considered in COM. However the suggested remedy does not provide clear information to implement.

There is no consensus to implement the suggested remedy at this time. More empirical evidence and consensus building is required.

## C #247 Reference DFE minimum tap limits

- Add minimum DFE tap weight limits
   & update AN93A.1:
  - bmin(1) = +0.3
  - bmin(2) = +0.05
  - bmin(>2) = -0.03
- References:

kasapi\_3ck\_01\_1119 heck\_3ck\_01\_0919 heck\_3ck\_adhoc\_01\_061720

Proposed response: Accept.

C/ 162 SC 162.11.7 P 160 L 48 # 247

Dawe, Piers Nvidia

Comment Type TR Comment Status D

CA COM

It isn't reasonable to expect a real receiver to provide a DFE tap strength of -0.85. Therefore, the channel should not be specified as if the receiver can do that. Further, there is an advantage in knowing that the sign of a tap can't change.

kasapi\_3ck\_01\_1119 slide 7 shows the first DFE tap >0.42 for the critical channels.

Another analysis showed the same for 27 backplane channels. Slide 6 of

heck\_3ck\_01\_0919 (107 channels) shows that the DFE taps are 2 and 3 are always strongly positive, and no taps <-0.045, yet the draft would allow such untypical/hypothetical channels.

We wanted to check that low loss channels would not do something surprising before adopting sensible limits that don't burden real channels. See new Heck presentation. Remember that channels that go a little outside a tap weight pay a very small increase in COM for the excess ISI noise that they cause (see another comment), so the limits for the smaller taps should be set a bit tighter than the worst channel we want to pass. Cable channels are smoother than backplane channels but can have higher loss:

#### SuggestedRemedy

Add minimum tap weight limits:

Tap 1: min +0.3

Tap 2: min +0.05

All other taps: min -0.03 (tighter than for KR).

Turn the existing "Normalized DFE coefficient magnitude limit"s into "Normalized DFE coefficient limit"s.

Update definition of COM in 93A.1.

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE

For task force discussion.

Referenced presentation is here:

http://www.ieee802.org/3/ck/public/adhoc/jun17\_20/heck\_3ck\_adhoc\_01\_061720.pdf

### C #248 Reference DFE Tail

• Proposes: Remove tap positions 25-40.

- Proposed response: Reject
- Refer to the response to C#262
  - Identical proposal for CL163

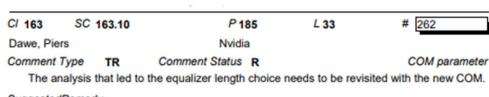
CI 162	SC	162.11.7	P 1	61	L 4		#	248	
Dawe, Piers	s		Nvidi	а					
Comment T	ype	TR	Comment Status	D				CAC	СОМ
The ana	alysis	that led to	the equalizer length	choice	needs to b	e revisited w	rith t	the new Co	OM.

#### SuggestedRemedy

If there is a significant improvement with the latest COM, remove positions 25-40 and define positions 13-24 as the tail, with 2 or 3 floating groups of 3 taps and an RSS limit.

### Proposed Response Response Status W PROPOSED REJECT

The task force adopted the reference equalizer based upon review of data for an extensive set of contributed channels. Commenter is encouraged to present analysis to support the suggested remedy.



#### SuggestedRemedy

If there is a significant improvement with the latest COM, remove positions 25-40 and define positions 13-24 as the tail, with 2 or 3 floating groups of 3 taps and an RSS limit.

Response Response Status C

This comment does not provide sufficient evidence the suggested remedy will not disqualify channels the task force has agreed to pass.

### C #249 Reference DFE Tail RSS

 Proposes: Apply a DFE RSS to tap positions 13-24

Proposed response: Reject

- Refer to the response to C#263
  - Identical proposal for CL163

CI 162 SC 162.11.7 P 161 L 6 # 249

Dawe, Piers Nvidia

Comment Type TR Comment Status D CA COM

The spec allows a channel to have its COM calculated with 9 taps in the range 13 to 24 clipped at +/-0.05 - which means that the channel's pulse response could be a little worse than +/-0.05 for these taps. That's a very bad channel! We don't need to provide all the receiver power and complexity to cope with it.

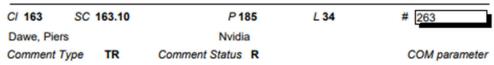
#### SuggestedRemedy

Use another DFE root-sum-of-squares limit for positions 13-24.

Proposed Response Response Status W

PROPOSED REJECT

The task force adopted the floating tap RSS limit based upon review of data for an extensive set of contributed channels. The comment proposes to change the limit if certain conditions are met. Without supporting data, the task force cannot verify whether those conditions are met. The commenter is encouraged to provide analysis to support the suggested remedy.



The spec allows a channel to have its COM calculated with 9 taps in the range 13 to 24 clipped at +/-0.05 - which means that the channel's pulse response could be a little worse than +/-0.05 for these taps. That's a very bad channel! We don't need to provide all the receiver power and complexity to cope with it.

#### SuggestedRemedy

Use another DFE root-sum-of-squares limit for positions 13-24.

Response Status C

REJECT

The suggested remedy does not provide clear information to implement. Sufficient evidence has not been provided to justify the proposed change. More empirical evidence and consensus building is required.

### C# 250 Ref DFE Tail

Proposes: Tighter DFE RSS requirement

Proposed response: Reject

- Refer to the response to C#264
  - Identical proposal for CL163

C/ 162 SC 162.11.7 P 185 L 36 # 250

Dawe, Piers Nvidia

Comment Type TR Comment Status D

CA COM

As the effect of exceeding the DFE floating tap tail root-sum-of-squares limit increases parabolically as the channel exceeds the limit, the limit must be set a little lower than the worst channel we wish to allow to have an effect at the right point. OAch4 with COM 2.75 gave an unconstrained RSS\_tail of 0.022, but CR channels should be smoother than OAch4. Setting the limit 0.01 lower than that might affect its COM by 0.1 dB (vs. no limit) which seems like a gentle effect. However, it seems that the latest COM gives a more optimistic result anyway: this channel may not need the tail taps at all.

#### SuggestedRemedy

If there is no improvement with the latest COM AND the via capacitances in 162.11.7.1.1 fully represent the tail pulse response of the hosts, change the DFE floating tap tail root-sum-of-squares limit to 0.012.

If the tail pulse response of the hosts is not all in this COM calculation, the COM equalizer should differ to the KR one, for the same silicon.

If there is a small improvement with the latest COM or the tail pulse response of the hosts is not all in this COM calculation, further reduce the limit accordingly.

If there is a significant improvement, remove taps 25-40 and apply a tail tap RSS limit to positions 13-24.

#### Proposed Response

Response Status W

#### PROPOSED REJECT

The task force adopted the floating tap RSS limit based upon review of data for an extensive set of contributed channels. The comment proposes to change the limit if certain conditions are met. Without supporting data, the task force cannot verify whether those conditions are met. The commenter is encouraged to provide analysis to support the suggested remedy.

CI 163 SC 163.10 P185 L 36 # 264

Dawe, Piers Nvidia

Comment Type TR Comment Status R COM parameter

As the effect of exceeding the DFE floating tap tail root-sum-of-squares limit increases parabolically as the channel exceeds the limit, the limit must be set a little lower than the worst channel we wish to allow to have an effect at the right point. OAch4 with COM 2.75 gave an unconstrained RSS\_tail of 0.022. Setting the limit 0.01 lower than that might affect its COM by 0.1 dB (vs. no limit) which seems like a gentle effect. However, it seems that the latest COM gives a more optimistic result anyway; this channel may not need the tail taps at all.

#### SuggestedRemedy

If there is no improvement with the latest COM, change the DFE floating tap tail root-sumof-squares limit to 0.012.

If there is a small improvement with the latest COM, further reduce the limit accordingly. If there is a significant improvement with the latest COM, remove taps 25-40 and apply a tail tap RSS limit to positions 13-24.

#### Response Status C

REJECT

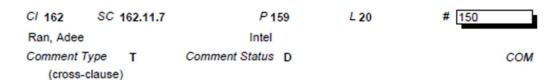
The simulations to make the determinations in the suggested remedy are not available.

There is no consensus to implement the suggested remedy at this time. More empirical evidence and consensus building is required.

## C#150 Package transmission line model

- Proposes: Specify 100G models in CL162.
  - Differ from existing models in AN93A.
- Proposed response:

Accept in principle. Implement with editorial license.



The transmission line parameters in the package model in COM have been the same since 802.3, and are hard-coded in Table 93A–3.

In the COM spreadsheets used in this project there are somewhat different values for these parameters (presented in

http://www.ieee802.org/3/ck/public/19\_01/benartsi\_3ck\_01\_0119.pdf, but not explicitly adopted into any of the drafts).

Validation of a proposed package model has been presented at the same meeting (http://www.ieee802.org/3/ck/public/19\_01/heck\_3ck\_01\_0119.pdf), but with the old TL parameters. So it is not clear if the modified parameters are in consensus.

#### SuggestedRemedy

If there is consensus that the parameters should change, then a new table should be created for the new values and used in 162,163, and 120F, and possibly a provision should be made in Annex 93A to use differnt parameters if supplied.

Otherwise, the COM spreadsheets should rever to use the existing values (out of scope of the editorial team...)

Proposed Response

Response Status W

PROPOSED ACCEPT IN PRINCIPLE

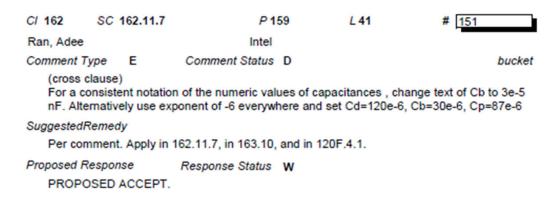
Pending task force discussion.

Implement with editorial license.

The referenced presentations are here: http://www.ieee802.org/3/ck/public/19\_01/benartsi\_3ck\_01\_0119.pdf http://www.ieee802.org/3/ck/public/19\_01/heck\_3ck\_01\_0119.pdf

### C# 151 Unit Consistency

- Change Cb value from 0.3e-6 nF to 3.0e-5 nF.
  - i.e. don't use leading '0'.
- Proposed response: Accept
- Note: also applies to 163.10 and 120F.4.1



## RX & TX

Topic	Comments
RX	259
TX ACCM	203
TX measurement filter	136
TX host IL	40
TX linear fit & Vf	255, 141
TX EQ	144, 258, 256

## RX & TX Characteristics

### C#203 AC Common Mode

- Proposed response: Reject
- Refer to response to C#28.

C/ 162 SC 162.9.3 P148 L24 # 203

Comment Status D

Ghiasi, Ali Ghiasi Quantum/Inphi

AC CM

30 mV AC common mode has significant amount of penalty given that RLCD  $\sim$ RLDC or 12 dB depending on the loss of the channel the penalty can be 1-3 mV RMS

SuggestedRemedy

Comment Type TR

Consider reducing 30 mV RMS to 17.5 mV RMS

Proposed Response Status W

PROPOSED REJECT

The comment needs to provide supporting analysis to address additional considerations (e.g. design and manufacturing variation).

Resolve using the response to comment #28.

C/ 163 SC 163.9.1 P177 L38 # 28

Wu, Mau-Lin Mediatek

Comment Type T Comment Status R common mode noise

The 'AC common-mode RMS voltage (max.)' is 30 mV, which is the same as that in 802.3cd. By combining this spec with P/N skew mismatch of backplane channel, it will induce crosstalk to differential signal at receiver. From 50G to 100G, it's difficult to improve the P/N skew mismatch to half. Based on that, we shall modify AC common-mode RMS voltage. We shall align this spec to that in C2M (120G).

SuggestedRemedy

Change 30 mV to 17.5 mV.

Response Status C

REJECT.

Note that comment #205 and #54 request the same change.

The suggested remedy does not provide sufficient evidence that the proposed threshold is feasible and necessary. Further evidence and consensus building is encouraged.

This applies to both KR and C2C.

### C# 255 Linear Fit Pulse

- Proposes: Define Nv and set it to 40, consistent with span of the reference DFE.
- Background:
  - CL85 defines Nw as the equalizer length
  - CL136 defines Nv as the equalizer length
  - CL162 uses Nv without definition and has it set to 200.
- Proposed response: Accept in principle.

Add text to define Nv (consistent with 136.9.3) and set Nv=40.

Back in Clause 85, the DFE has 14 taps (Nb), the linear fit pulse length Np is 8 and the equalizer length Nw is 7. So the SNDR measurement doesn't forgive reflections in the transmitted waveform that the DFE can't equalise. Here, we have a DFE with up to 40 UI, Np is 200. Nv is 200? Or do we still use Nw of 7 from Clause 85?

#### SuggestedRemedy

Is Nv meant to be Nw?
I wonder if 200 (for something) is far too long

Proposed Response Status W

PROPOSED REJECT

The linear fit pulse method is based upon the method specified in CL136 for 50G PAM signaling, which used Np=200.

### C# 141 Vf

- Proposes: Replace reference to 136.9.3.1.2 with wording taken from that subclause.
  - Eliminates one level of sub-referencing
- Proposed response: Accept

SC 162.9.3.1.2 P 151

Ran, Adee

"The steady-state voltage vf is defined in 136.9.3.1.2, and is determined using Nv=200"

Comment Status D

The definition in 136.9.3.1.2 is concise, and includes yet another reference to clause 85. The value of Nv is significantly different. It would help readers if we reduce the depth of references.

#### SuggestedRemedy

Comment Type

Change this sentence to the following (in a separate paragraph):

"The steady-state voltage vf is defined to be the sum of the linear fit pulse response p(1) through p(M×Nv) divided by M

(refer to 85.8.3.3 step 3)" where Nv=200 is the length of the pulse response in UI."

Proposed Response

Response Status W

PROPOSED ACCEPT

## Tx c(0): C#144 & #258

- Proposes: Set minimum value for c(0)
- Proposed response: Accept.

CI 162 SC 162.9.3.1.5 P 152 L 19 # 144

Ran, Adee Intel

Comment Type T Comment Status D bucket

There is no requirement in the transmitter characteristics for the range of c(0).

While the maximum is 1 by definition of the measurement method, the minimum is only implied by the minimum value of c(-1) and an assumption that the sum of absolute coefficients is capped at 1 (which may not be true in all implementations).

Even assuming that the sum is not larger than 1, the implied minimum of c(0) is 0.66, while the COM search range assumes 0.54 is possible.

#### SuggestedRemedy

(cross-clause)

Add the following paragraph before the NOTE:

Having received sufficient "decrement" requests so that it is at its minimum value, c(0) shall be less than or equal to 0.54.

Add a row in table 162-9: "value at minimum state for c(0) (max.)" with reference to this subclause and value 0.54.

Add similar rows in table 163-5 and table 120F-1.

Proposed Response Response Status W
PROPOSED ACCEPT

C/ 162 SC 162.9.3.1.5 P152 L3 # 258

Dawe, Piers Nvidia

Comment Type T Comment Status D bucket

There seem to be rules here to ensure that c(-3), c(-2), c(-1) and c(1) can be moved over defined ranges, but not for c(0).

#### SuggestedRemedy

What is the intention? What should attempting to adjust c(0) be able to achieve and what is out of bounds?

Write down whatever information is missing in Table 162-9 and here. If it isn't missing, put it in in Table 162-9 and cross-reference it from this section.

Adjust Clause 163 consistent with this.

Proposed Response Response Status W
PROPOSED ACCEPT IN PRINCIPLE

Resolve using the response to comment #144.

## C# 256 ic\_req

- Proposes: Define ic\_req and add references.
- Proposed response:

Accept in principle. ic\_req is defined in Table 162-7. Add reference to it.

C/ 162 SC 162.9.3.1.3 P 151 L 21 # 256

Dawe, Piers Nvidia

Comment Type T Comment Status D

bucket

"ic\_req" appears without explanation. I can see that it may be mapped to an MDIO register, but those registers follow the hardware, they don't define it. The reader doesn't know it's in Figure 136-9 because you haven't told him, and anyway that's too arcane.

SuggestedRemedy

Explain what it is, with appropriate references to 162.8.11 and 136.8.11.something.

Proposed Response Response Status W
PROPOSED ACCEPT IN PRINCIPLE

Implement the suggested remedy with editorial license, adding description with reference to the definition in Table 162-7.