Doc: IEEE 802.4L/90-12

IEEE 802.4L

Through-the-Air Physical Media, Radio

Running Objectives and Directions Document

Seventh issue

This document provides a base for the discussions of the IEEE 802.4L Working Group.

Each decision will be marked in this document along with the reference to the motion on which the decision has been based (column Base) and with the reference of the document on which the present decision is based (Doc no).

After each meeting a new document will be prepared to reflect the decisions made at the meeting.

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Subject	Base	Doc no
1. Scope		2
To define an alternative Physical Layer for Through-the-air communication, which is	PAR	4L/87-014
part of a local area network using 802.4 media access techniques and which is primarily for		
mobile environments.		
2. Purpose		
To provide LAN access to moving automatic machines and other stations for which wireless attachment is appropriate.	PAR	4L/87-014
To add description of standards criteria for through-the-air transmission parameters to		
support Physical Layer Service.		
To prepare, if necessary, a petition to the FCC for rule making which authorizes use of		
radio spectrum for wireless LAN.		
3. Directions		
3.1 Design Principles		
- 1. Meet FCC rules - spreading, scrambling, power, etc.	Jul 89	4L/89-11
- 2. Meet 802.4 requirements implicit in ISO DIS 8802-4 1-10	Jul 89	4L/89-11
-3. Economy	Jul 89	4L/89-11
- 4. Permit adjacent 802.4L-conformant radio LANs	Jul 89	4L/89-11
- 5. Provide for both single-channel (direct peer-to-peer) and dual-channel (head-ended)	Jul 89	4L/89-11
operation		
-6. Single-channel system size: The objective is to permit a system diameter of 300 m. The	Jul 89	4L/89-11
minimum acceptable system diameter is 100 m.	1 _ 1 1 1 1	
-7. Modulation technique must support office, retail and industrial environments.	Jul 89	4L/89-11
- 8. Want high data rate at required BER and outage.	Nov 89	4L/89-17
- 9. Robust with respect to multipath	Nov 89	4L/89-17
- 10. Want to accommodate relative motion between Transmitter and Receiver	Nov 89	4L/89-17
- 11. For a given operating band (902-928 MHz, 2400-2483.5 MHz, 5725-5875 MHz), want the interoperability relationship of differing moderns to form a direct inclusion	Nov 89	4L/89-17
relationship (full and not partial ordering).		
points of interoperability.		
finish definition of the primary air interface before considering any other interfaces.		
3.2 System plan		
The radio system plan for one community of users is proposed to be a single frequency	T 80	41 (00 00
bus mode with head end, but will accommodate single frequency station-to-station operation for	Jan 89	4L/89-02
small systems. The physical layer including the head end and radio system shall support the	Jul 89	4L/89-11
existing 802.4 MAC. (Among other things, this implies that when any station is transmitting,		
all stations must hear something.)		
In the single frequency bus mode with head end normal token rotation shall be used,	May 89	
only for stations in the outskirt, immediate response mode will be considered. (see issue 5)	Jul 89	
Whatever plan is evolved, it shall be suitable for use under current FCC part 15	Jul 88	
regulations, in particular the three bands, 902-928 MHz, 2400-2483.5 MHz, and 5725-5875 MHz.		
The 902-928 MHz band will be used in the first standard. At least 2 channels will be	Jan 90	

Subject	Base	Doc no

3.2 Directions (cont..d)

	one of the contract (contract)		
3.2	System plan (contd)		
	To separate transmissions of stations of nearby networks the preamble will contain a	14 00	
Net	work Identification.	May 89	
		May 89	
3.3	System Design Parameters		
Rela	ation to the Objective List in [3.1]	Jul 89	4L/89-11
1.	Use a 7-bit (length-127) scrambler if the adopted chip rate is < 127 . [1] The preferred polynomial is $1 + X^{-4} + X^{-7}$. [1+3]		
2.	Choose a modulation technique that does not include an amplitude modulation	Jul 89	4L/89-11
	component, for [3] and to lower technical risk.	301 09	41/09-11
3.	Permit differential demodulation for fast acquisition, to provide robustness for the time-	Jul 89	4L/89-11
	varying (fading) radio channel, and to simplify the receiver [3]. The primary	244 07	41407-11
	disadvantage of this approach is a 2.3 dB (theoretical) loss in S/N.		
4.	Use some form of quaternary PSK as a reasonable means of decreasing signaling rate	Jul 89	4L/89-11
	(for multipath) without excessively compromising S/N or [3,7].		.20,11
5.	Spread the minimum amount practical [1,3]. The preferred spreading code is	Jul 89	4L/89-11
	+ - ++ - + + + This is a known Barker code, with bounded auto-correlation,		.20711
	bounded periodic auto-correlation, and bounded odd periodic auto-correlation, and good		
	spectral properties.		
6	Filtering should consider adjacent channel single frequency (single channel) and	Jul 89	4L/89 11
	simultaneous dual frequency (dual channel) operation. [4,5]	Jan 90	4L/90-01
7.	Initial focus should be on 902-928 MHz band. [3]	Jul 89	4L/89-11
8.	The design goal for the overhead of each Ph-PDU be 25 octets or less. This	Mar 90	4L/90-S
	includes synchronization pattern, network id, CRC on the Ph-PDU content, and FEC		
	flush. Note that the overhead can be different for the forward and reverse channel.		
3.4	Modulation		
	Differential Phase Modulation shall be used.	Nov 88/1	4L/88-02
Doc:	IEEE p802.4L/89-16 is adopted as the basis for the description of the modulator.	Nov 89	4L/89-17
	For the spreading sequence at least 10 and not more than 15 chips shall be used. This	Nov 88/3	4L/88-02
provi	des a processing gain of between 10 and 15 allowing frequency division multiplexing of	110.00,5	11200-02
	cated LANs		
3.5	Encoding		
ciana	The goal is to encode the preamble and the frame delimiters without increasing the	Sep 89	4L/89-15
orgila	constellation.		
Barke	It is suggested to encode the MAC non-data symbol by a different chip sequence (e.g. er-11 backwards).	Sep 89	4L/89-15

Subject Base Doc no

Directions (cont..d)

3.6 Data Rate

The data rate for comparison purposes shall be 1 Mbit/s. We can only consider the IEEE data rates of 1 to 20 Mbit/s.

Jan 89

3.7 Distribution System

The design model shall assume a 16 antenna array in a square grid. For purpose of analysis, it will be assumed that the antenna array is driven by one power splitter with equal length loss less cable from the splitter to each antenna.

3.8 Performance definition

The performance of the Token Bus standard will be expressed in the number of MAC Service Data Units with undetected errors per time unit, at 0 frame overhead.

May 89

The performance requirement is: less then one MSDU with undetected errors per year at 200 bit data units.

The frame loss rate shall be less then 1 per 10 8 frames transmitted.

3.9 Bit Error Ratio

The Bit Error Ratio (BER) at the MAC/PHY interface shall be 10^{-8} or less achievable in all but 10^{-3} or less of the area of spatial coverage of the system in a minimally-conformant system, and where additional antenna and receiver diversity can be used to reduce the area of outage as required.

Sep 89 4L/89-15 Jan 90 4L/90-01

3.10 Outage

MAC protocol assumes the communication channel is always available. Since the radio medium is known to have an outage rate on the order of 10E-2, a method is required to reduce outage rate to less than 10E-5.

Jul 88

3.11 Velocity ranges

The following are the ranges for the velocity of the stations: 902-928 MHz 0 - 53.7 miles/h

Jan 89

2400-2483.5 MHz

0 - 20.0 miles/h

5725-5875 MHz

0 - 8.3 miles/h

3.12 Transmission Power

XMTR power output: 1 W max

Station antenna gain: TBD

Station antenna directivity: TBD

Receiver noise figure: 6 dB at 902-928 MHz

Jan 89 Jan 89

Jan 89 Jan 89

8 dB at 2400-2483.5 MHz

Jan 89

10 dB at 5725-5875 MHz

Jan 89 Nov 89

For a distributed antenna system, we assume that each transmitter should be measured separately (for complying with the regulation). The transmit carriers should not be phase locked but should be approximately the same frequency.

4L/89-15

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Directions (cont..d)

3.13 Error correction codes

The goal is to avoid the use of Forward Error Correction code, if possible.

Sep 89

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Allowable overhead:

1.2x TBD

Jan 89

Type: Spectral efficiency:

TBD

Jan 89

3.14 Propagation

Office/retail environment:

6 dB/octave under 10 meters

Jan 89

footnote explaining what the terms "retail", "factory" and "office" represented.

environment	slope dB/octave	standard deviation dB	exp	RMS Delay spread (within 20 dB from max peak) ns	Coherence Time
open retail	10-13	4-7	3.3-4.2	80-140	Total (1981)
factory	5.4-8.4	5-10	1.8-2.4	100-140	
office	10-12	2-7	3.3-4.0	<50	The state of the s

Table 1. Channel characteristics

Coherence time is defined as follows:

Given a time-variant (wide-sense stationary) channel impulse response of $c(\tau;t) = \alpha(\tau;t) \, e^{-j2pfc\tau} \, , \text{ where } \tau \text{ is the delay and } \alpha(\tau;t) \text{ is the attenuation of the signal components at delay } \tau \text{ at time instant } t.$

Let C(f;t) =

$$\int_{c(\tau;t)}^{\infty} e^{-\phi 2\pi\phi \tau} dt$$

be the Fourier transform of this impulse response.

 $2\varphi_{c}(\mathrm{f}_{1}.\mathrm{f}_{2};\!\Delta\mathrm{t}) = \ 1/2 \ \mathrm{E}\left[(c^{*}(\mathrm{f}_{1};\!\mathrm{t}) \ C(\mathrm{f}_{2};\!\mathrm{t}\!+\!\Delta\mathrm{t})\right] = \varphi_{c}(\Delta\mathrm{f};\!\Delta\mathrm{t}) \ ,$

where E is expectation, is called the spaced-frequency spaced-time correlation function. If you hold Δf to 0 you have the spaced-time correlation function. The period of time over which the magnitude of this function is essentially non-zero is the coherence time of the channel.

the environment is not static and thus Doppler effects may occur even when the sending and receiving stations are not themselves moving (with respect to the earth, each other, the surrounding "building", etc.).

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Directions (cont..d)

Table prepared

Nov 89

4L/89-

17

Table updated

Jan 90

Noise:

Jan 89

at 902-928 MHz

10 dB above thermal

at 2400-2483.5 MHz

thermal

Jan 89

Contributions on noise are requested in the following format:

Device	Band	distance from source	Power *) level	Numb	er of hits p	er second shold	
1	Ja			-10 dB	-20 dB	-30 dB	-40 dB
		m	dBm				and the second
						a ' ,	
				a gr		4	
					-		A FIRE TO KIND OF THE ST

Table 2. Characteristics of impulsive noise generators

Table prepared

Nov 89

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Directions (cont..d)

Device	Freq	Power		Bandwidth	Duty cycle
		EIRP	Receive level	R Z	
	MHz	W	dBm	kHz	
(1)	(2)	(3)	(4)	(5)	(6)
Pager	931.6125	340		15	5 sec/call 1 call/5 min
Radio Channel	904		in the state of some	30	continuous
Pager	930.0	ante alterito de la Viva. Os casos de la especto po	- 50 indoor	15	5 se/call 1 call/min
Field disturbance sensors	902-928	0.075	e Ben de la Ben et Ben d'alle d'Arnort La santa de Mangara	<1	continuous
Part 15 devices	902-928 2400-2483.5 5725-5875	.00075			i i i i i i i i i i i i i i i i i i i
Digital oscillators				3.18.*	
Digital devices		of more less to the		e de faithe a e tha	

Table 3. Characteristics of Constant Wave Interferers

Subject Doc no Base

Directions (cont..d)

NOTES: * reference antenna:

Nov 89 Jan 90

4L/89-17 4L/90-01

dipole for the appropriate band

distance from source > 1 m

vary measurements over a sphere with

at least 10 measurements

* for impulsive noise measurements:

make the measurements in the

time domain

* for CW measurements:

include a graph of frequency versus

time behavior for sweeping

devices, e.g. microwave ovens.

It appears that the magnetron has a negative resistance on turn-on and turn-off, and this causes relaxation oscillations at the beginning and end of each power cycle, which cause an apparent broadband emission. In reality, during the beginning and end of each power cycle, the magnetron produces a series of very short bursts of carrier (<< 300 ns each) with decaying power and a frequency which changes slightly during the burst, and with more substantial changes in frequency from one burst to the next.

In the middle of each power cycle the magnetron just stays on, with occasional instantaneous frequency changes due to shifts in mode-locking caused by the changing magnetron plate voltage and the motion of the stirrer in the oven cavity. (See addendum L1, and IEEE 802.4L-89/19 for time domain pictures of this phenomenon.) These instantaneous changes may be accompanied by additional bursts. (See IEEE 802.4L/90-8a figure 4-46.)

3.15 Antenna

Jan 89

3.16 Higher Laver concerns

When considering the use of the immediate response mode for stations in the outskirts of the coverage area, thus avoiding the higher probability of losing the Token, the implication is that a station can use only the responder services of LLC type 3.

Use of LLC types 1 or 2, or the initiator services of LLC type 3, will cause the station to try to get and later pass the token.

Sep 89 4L/89-15

4. Meeting Plan

Type	Dates	Place	Objective
Interim	May 14-18, 90	Atlanta, GA	Prepare second 802.4 draft
			1 - 2 - 12 - 12 - 12 - 12 - 12 - 12 - 1
Plenary	Jul 9-13, 90	Denver, CO	Se∞nd 802.4 draft
Interim	Sep, 90	?	Prepare 802.4 Voting draft
Plenary	Nov 12-16, 90	Kauai, HI	802.4 Ballot
Interim	Jan, 1990	?	prepare TCCC voting draft
Plenary	Mar 11-15, 1991	East coast	TCCC Ballot
	Mail 11-15, 1551	Last Wast	rece Ballot
Interim	May, 1991	?	Prepare Final draft
Plenary	Jul 8-12, 1991	West Coast	Final Draft
Plenary	Nov 11-15, 1991	Ft Lauderdale, FL	. PM

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5. Possible Document Outline

- 20. Radio Bus Physical Layer
 - 20.1 Nomenclature
 - 20.2 Object
 - 20.3 Compatibility Considerations
 - 20.4 Operational Overview
 - 20.5 General Overview
 - 20.6 Application of Network Management
 - 20.7 Functional, Electrical and Mechanical Specifications
 - 20.8 Environmental Specifications
- 21. Radio Bus Medium
 - 21.1 Nomenclature
 - 21.2 Object
 - 21.3 Compatibility Considerations
 - 21.4 General Overview
 - 21.5 Functional, Electrical and Mechanical Specifications
 - 21.6 Environmental Specifications
 - 21.7 Transmission Path Delay Considerations
 - 21.8 Documentation
 - 21.9 Network Sizing
 - 21.10 Guidelines

6. Issues

- 1 Is a Bit Error Ratio (BER) of 10** 8 detected and 10** 9 achievable with operation with a dual frequency head end distribution system.
- 2 Is the BER described in issue 1 achievable for direct station to station operation and what is the condition to achieve this BER.
- 3 What Forward Error Correcting Code (FEC) is suited for channels with burst errors characteristics.
- 4 Considering the agreement that non-data will not be encoded as a PHY symbol: Find a method of start and end delimeter encoding, e.g. use a combination of an alternative constellation and corrolation.
- 4a What is the characteristic of the impulse noise in the various media.
- 5 What are the implicatios on the LLC when the immediate response mode is required to communicate with stations in the outskirt?
- 6 How should a distributed antenna system be represented for ruling measurements.
- What are the trade-offs in data rate vs noise immunity (long vs short codes) [refer to doc: IEEE p802.4L/89-17, pages 6-8]
- What are the trade-offs of long codes vs short codes at higher frequencies (wider bands) and multiple channels (FDM vs CDM) [refer to doc: IEEE p802.4L/89-17, pages 6-8]
- What are the noise characteristics for various devices [refer to tables 2 and 3 above]
- 10 Is table 1 above accurate?
- Data on coherence time is needed. Part of the data could be recovered from Oshawa measurements and from Rappaport's report. More measurements are to be made when the results prove some parameters have been missed.

7. Referenced papers.

The following papers are of interest to the taskgroup members:

Environmental Monitoring for Human Safety Part 1: Compliance with ANSI Standards. By John Coppola and David Krautheimer, Narda Microwave Corporation. - RF Design--.

RF Radiation Hazards: An update on Standards and Regulations. By Mark Gomez, Assistant Editor, and Gary A. Breed, Editor. - RF Design, October 1987

RF Radiation Hazards: Power Density Predeiction for Communications Systems. By Gary A. Breed, Editor. - RF Design, December 1987

Microprocessor Interference to VHF Radios. By Daryl Gerke, PE Kimmel Gerke & Associates, LTD. - RF Design, March 1988

<u>Distributed Antennas for Indoor Radio Communications</u>. By Adel A.M. Saleh, A.J. Rustako, Jr and R.S. Roman. - IEEE Transactions on Communications, Vol. Com-35, No12, December 1987

<u>UHF Fading in Factories</u>. By Theodore S. Rappaport and Clare D. McGillem. - IEEE Journal on selected Areas in Communications. Vol. 7. No 1. January 1989

<u>Indoor Radio Communications for Factories of the Future</u>. By Theodore S. Rappaport. - IEEE Communications Magazine. May 1989.

A differential offset OPSK modulation/demodulation technique for point-to-multipoint radio systems. By Tho Le-Ngoe. GLOBECOM 87.

Highly Efficient Digital Mobile Communications with a Linear Modulation Method. (p/4 QPSK) By Yoshihito Akaiwa and Yoshinori Nagata. - IEEE Journal on Selected Areas in Communications. Vol. SAC-5, No. 5, June 1987, pp.890-895.