

# IEEE802.3at Task Force

## Vport ad hoc

### Conversion from Ipeak domain to Ppeak Domain

Rational behind the remedy for comment #86, Draft D3.0

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# Objectives

- The ratio between  $I_{port\_peak}$  to  $I_{port\_avg}$  was set to the same ratio as used in 802.3af i.e.  $K_i=0.4/0.35$ .
- In the PD we changed the parameters from  $I_{peak}$  to  $P_{peak}$  as we find it easier for matching behavior to legacy 802.3af PDs.
- As a result we want to define the ratio between  $P_{peak}$  to  $P_{class}$  in order to keep the same current ratio  $I_{peak}/I_{port}=0.4/0.35$  in Type 2 (Class 4) PDs.
- The PD model is approximated to constant power load
- $P_{pd}$  is the PD requested power i.e.  $P_{class}$
- $P_{pd\_peak}$  is the peak PD power during PD load dynamic changes i.e. PD current is up to  $(0.4/0.35)*I_{pd}$  for 50msec max.
- $V_{overload}$  is the PD input voltage during  $P_{pd\_peak}$



# Equation Derivations

- Objective: Keep the ratio  $K_i = \frac{I_{pd\_peak}}{I_{pd}} = \frac{0.4}{0.35} = 1.142857$
- We need to find:  $K_p = \frac{P_{pd\_peak}}{P_{pd}}$
- →  $P_{peak} = K_p \cdot P_{class}$
- From previous work<sup>1</sup> we can derive  $I_{port}$  and  $I_{port\_peak}$  as function of system parameters:

$$V_{pd} = \frac{V_{pse} + \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{class})}}{2}$$

$$I_{pd} = \frac{V_{pse} - V_{pd}}{R_{ch}}$$

$$\therefore I_{pd} = \frac{V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})}}{2 \cdot R_{ch}}$$

$$V_{pd\_overload} = \frac{V_{pse} + \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot K_p \cdot P_{pd})}}{2}$$

$$I_{pd\_peak} = \frac{V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot K_p \cdot P_{pd})}}{2 \cdot R_{ch}}$$



# Equation Derivations

$$K_i = \frac{I_{pd\_peak}}{I_{pd}} = \frac{0.4}{0.35} = \frac{\frac{V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot K_p \cdot P_{pd})}}{2 \cdot R_{ch}}}{\frac{V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})}}{2 \cdot R_{ch}}}$$

$$K_i = \frac{V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot K_p \cdot P_{pd})}}{V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})}}$$

$$\sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot K_p \cdot P_{pd})} = V_{pse} - K_i \cdot \left( V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})} \right)$$

$$(V_{pse}^2 - 4 \cdot R_{ch} \cdot K_p \cdot P_{pd}) = \left( V_{pse} - K_i \cdot \left( V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})} \right) \right)^2$$

$$(V_{pse}^2 - \left( V_{pse} - K_i \cdot \left( V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})} \right) \right)^2) = 4 \cdot R_{ch} \cdot K_p \cdot P_{pd}$$

$$K_p = \frac{V_{pse}^2 - \left( V_{pse} - K_i \cdot \left( V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})} \right) \right)^2}{4 \cdot R_{ch} \cdot P_{pd}}$$



# Results

■ Solving for  $K_p$  for the worst case conditions:

- $R_{ch}=12.5$  ohms
- $V_{pse}=50V$
- $K_i=0.4/0.35$
- $P_{pd}=25.5W$  for  $I_{cable}=600mA$

$$K_p = \frac{V_{pse}^2 - \left( V_{pse} - K_i \cdot \left( V_{pse} - \sqrt{(V_{pse}^2 - 4 \cdot R_{ch} \cdot P_{pd})} \right) \right)^2}{4 \cdot R_{ch} \cdot P_{pd}} =$$
$$= \frac{50^2 - \left( 50 - \frac{0.4}{0.35} \cdot \left( 50 - \sqrt{(50^2 - 4 \cdot 12.5 \cdot 25.5)} \right) \right)^2}{4 \cdot 12.5 \cdot 25.5} = 1.114$$



# References

- 1. [http://www.ieee802.org/3/at/public/jan08/darshan\\_3\\_0108.pdf](http://www.ieee802.org/3/at/public/jan08/darshan_3_0108.pdf) pages 22 and 23 done for 29.5W/0.72A PD showing how we got  $K_i$  and  $K_p$ .

