

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 45 SC 45.2.1.115a P 46 L 13 # 1

Anslow, Pete Independent

Comment Type E Comment Status X

When a new subclause is inserted between two existing subclauses of the same level (e.g., between 45.2.114 and 45.2.115) the new subclause number is the same as the lower of the two with "a" added. This is 45.2.114a in the example. See 2020 IEEE SA Style manual: <https://mentor.ieee.org/myproject/Public/mytools/draft/styleman.pdf#page=40>  
The same principle applies to inserted tables.  
This needs to be corrected for 45.2.1.115a, Table 45-93a, 45.2.1.126a, Table 45-100a

*SuggestedRemedy*

Change the numbering of 45.2.1.115a, Table 45-93a, 45.2.1.126a, and Table 45-100a to be 45.2.1.114a, Table 45-92a, 45.2.1.125a, and Table 45-99a, respectively.

Proposed Response Response Status O

CI 45 SC 45.2.1.135a P 55 L 11 # 2

Anslow, Pete Independent

Comment Type E Comment Status X

Changes for table footnotes b and c are not shown correctly.  
Similar issues in Tables 45-103b, 45-103c, and 45-103d.

*SuggestedRemedy*

In Table 45-103a:  
in the row for 1.1120.4:2 underline the added "c"  
Underline the whole of table footnotes b and c  
In Table 45-103b:  
in the row for 1.1220.5:3 underline the added "b"  
Underline the whole of table footnote b  
In Table 45-103c:  
in the row for 1.1320.4:2 underline the added "c"  
Underline the whole of table footnotes b and c  
In Table 45-103d:  
in the row for 1.1420.5:3 underline the added "b"  
Underline the whole of table footnote b

Proposed Response Response Status O

CI 45 SC 45.2.1.137a P 56 L 41 # 3

Anslow, Pete Independent

Comment Type E Comment Status X

Table 45-103c concerns register 1.1320, but there are 4 instances of 1.1120 in the table.

*SuggestedRemedy*

Change 1.1120 to 1.1320 in four places.

Proposed Response Response Status O

CI A SC A P 205 L 8 # 4

Anslow, Pete Independent

Comment Type E Comment Status X

"OIF-CEI-05, ..." should appear in the bibliography after "[B55] OIF-CEI-04.0, ..."

*SuggestedRemedy*

Change the numbering from [B22a] to [B55a]

Proposed Response Response Status O

CI 30 SC 30.6.1.1.5 P 36 L 32 # 5

Hajduczenia, Marek Charter Communications

Comment Type E Comment Status X

"as specified in Clause 73 (see 73.6.5) and" - I see very little value in adding Clause and then subclause information - subclause information is sufficient

*SuggestedRemedy*

Change to "as specified in 73.6.5 and"

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 45 SC 45.2.1.115a P 46 L 37 # 6

Hajduczenia, Marek Charter Communications

Comment Type E Comment Status X

Lots of unnecessary empty lines in between subclauses, tables, and text blocks.

*SuggestedRemedy*

Please remove all unnecessary white (empty) lines between (for example) 45.2.1.115 and 45.2.1.117 - these continue until at least page 54

Proposed Response Response Status O

Cl 80 SC 80.1.4 P 73 L 47 # 7

Hajduczenia, Marek Charter Communications

Comment Type E Comment Status X

Dead link "Clause 91 or Clause 161"

*SuggestedRemedy*

Add live hyperlink for these two clause numbers

Proposed Response Response Status O

Cl 162 SC 162.9.4.1 P 161 L 4 # 8

Brown, Matt Huawei

Comment Type T Comment Status X

Specification of the nominal unit interval is unnecessary and redundant (since it can easily be derived from the nominal signaling rate). It is not specified for KR, C2C, or C2M. For consistency with sister Clauses/Annexes, this specification should be removed.

*SuggestedRemedy*

Delete the sentence "This translates to a nominal unit interval of 18.82353 ps."

Proposed Response Response Status O

[Editor's note: Changed page from 162 to 161.]

Cl 163 SC 163.9.3 P 190 L 24 # 9

Brown, Matt Huawei

Comment Type TR Comment Status X

For the KR receiver, there is no requirement specified to meet the specifications over the entire signaling rate range. See 162.9.4.1 for a relevant example.

*SuggestedRemedy*

Add a new subclause before 163.9.3.1 with heading "Receiver signaling rate" and content as follows:

"A PHY shall comply with the receiver requirements of 163.9.3.4 and 163.9.3.5 for any signaling rate in the range 53.125 GBd ± 100 ppm."

Add a new row in Table 163-8 specifying the signaling rate range and reference the new subclause.

Proposed Response Response Status O

Cl 120F SC 120F.3.2 P 222 L 38 # 10

Brown, Matt Huawei

Comment Type TR Comment Status X

For the C2C receiver, there is no requirement specified to meet the specifications over the entire signaling rate range. See 162.9.4.1 for a relevant example.

*SuggestedRemedy*

Add a new subclause before 120F.3.2.1 with heading "Receiver signaling rate" and content as follows:

"The receiver shall comply with the requirements of 120F.3.2.3 and 120F.3.2.4 for any signaling rate in the range 53.125 GBd ± 100 ppm."

Add a new row in Table 120F-4 specifying the signaling rate range and reference the new subclause.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.3 P 243 L 25 # 11

Brown, Matt

Huawei

Comment Type TR Comment Status X

For the C2M host input, there is no clear requirement to meet the specifications over the entire signaling rate range. See 162.9.4.1 for a relevant example.

*SuggestedRemedy*

Add a new subclause before 120G.3.3.1 with heading "Host input signaling rate" and content as follows:

"The host input shall comply with the requirements of 120G.3.3.3 for any signaling rate in the range 53.125 GBd ± 100 ppm."

In Table 120G-7 add a reference to the new subclause for the signaling rate row.

Proposed Response Response Status O

CI 120G SC 120G.3.4 P 247 L 27 # 12

Brown, Matt

Huawei

Comment Type TR Comment Status X

For the C2M module input, there is no clear requirement to meet the specifications over the entire signaling rate range. See 162.9.4.1 for a relevant example.

*SuggestedRemedy*

Add a new subclause before 120G.3.4.1 with heading "Module input signaling rate" and content as follows:

"The module input shall comply with the requirements of 120G.3.4.1 for any signaling rate in the range 53.125 GBd ± 100 ppm."

In Table 120G-10 add a reference to the new subclause in the signaling rate row.

Proposed Response Response Status O

CI 120G SC 120G.3.3.3.1 P 245 L 33 # 13

Brown, Matt

Huawei

Comment Type TR Comment Status D

In previous drafts we aligned KR, CR, and C2C such that they share the same jitter tolerance table, Table 162-15 and added a new frequency point at 0.4 MHz. The same table should be used for C2M.

*SuggestedRemedy*

Delete Table 120G-9.

At page 245 line 1, change the sentence to: "Sinusoidal jitter is applied with frequency and peak-to-peak amplitude according to each case in Table 162-15.

At page 248 line3, change the sentence to: "The amount of applied peak-to-peak sinusoidal jitter used for the module stressed input test is given in Table 162-15."

In Table 120G-8 and Table 120G-11, change "Table 120G-9" to "Table 162-15".

Proposed Response Response Status O

[Editor's note: Changed subclause from 120G.3.3.3 to 120G.3.3.3.1.]

CI 120G SC 120G.3.1 P 237 L 17 # 14

Brown, Matt

Huawei

Comment Type ER Comment Status X

The eye height is defined by the measurement method in 120G.3.1.5 and it is not necessary to qualify it as being "differential". If so, the VEC should also be qualified as "differential".

*SuggestedRemedy*

Change "Eye height, differential (min)" to "Eye height (min)"

Proposed Response Response Status O

CI 120F SC 120F.3.2.4 P 225 L 1 # 15

Brown, Matt

Huawei

Comment Type TR Comment Status X

In the exception list in 120F.3.2.4, the last exception (item d) is a repeat of an exception (item i) in 120F.3.2.3. Since 120F.3.2.4, is referencing 120F.3.2.3, the exception in item d is not required.

*SuggestedRemedy*

In 120F.3.2.4, delete the last exception (item d).

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 120F SC 120F.4 P 225 L 49 # 16

Brown, Matt Huawei

Comment Type ER Comment Status X

It would be beneficial to include a specification summary table for the C2C channel similar to the Tables for C2C TX (Table 120F-1), C2C RX (Table 120G-4), and CR Channel (Table 162-16).

*SuggestedRemedy*  
Create a new table similar to Table 162-16 to summarize the C2M channel characteristics including related introductory text.

Proposed Response Response Status

Cl 00 SC P 0 L 0 # 19

Brown, Matt Huawei

Comment Type ER Comment Status X

In various clauses and annexes we specify various insertion loss, conversion loss, and return loss characteristics. The wording to identify and the variable names used to define these characteristics is inconsistent.

*SuggestedRemedy*  
Use consistent terminology and variable names to describe and specify the various terms. A presentation will be provided to explain further and provide proposals.

Proposed Response Response Status

Cl 163 SC 163.10 P 193 L 43 # 17

Brown, Matt Huawei

Comment Type ER Comment Status X

It would be beneficial to include a specification summary table for the KR channel similar to the Tables for KR TX (Table 120F-5), KR RX (Table 163-8), and CR Channel (Table 162-16). The text in 163.10 is not complete and can be replaced with a summary table.

*SuggestedRemedy*  
Delete the current text in 163.10.  
Create a new table similar to Table 162-16 to summarize the KR channel characteristics including related introductory text.

Proposed Response Response Status

Cl 120G SC 120G.3.1.5 P 239 L 8 # 20

Brown, Matt Huawei

Comment Type ER Comment Status X

An acronym for vertical eye closure (VEC) is defined in the first sentence of 120G.3.1.5. However, the acronym is rarely used in 120G and the full name is normally used. Since this acronym was not defined in 120E, where the base methodology is defined, 120G should continue to use the full name only.

*SuggestedRemedy*  
Delete all instance of the acronym VEC in 120G.  
Alternately, where appropriate, replace all instances of "vertical eye closure" with the acronym VEC.

Proposed Response Response Status

Cl 162 SC 162.11.5 P 168 L 37 # 18

Brown, Matt Huawei

Comment Type E Comment Status X

In a previous draft, a new parameter was added to constrain the CR channel differential to common-mode conversion loss. The term used to identify this parameter is: "difference between the cable assembly differential to common-mode conversion loss and the cable assembly insertion loss". The purpose of this parameter might not be immediately clear to a new reader of this standard and would benefit from a brief explanation.

*SuggestedRemedy*  
Add an explanation of the purpose of this parameter. Perhaps: "This parameter constrains the amount of common-mode noise present at the transmitter that is converted to differential noise at the receiver relative to the signal level at the receiver."

Proposed Response Response Status

Cl 120G SC 120G.3.4.1.1 P 247 L 53 # 21

Brown, Matt Huawei

Comment Type ER Comment Status D

Grammar

*SuggestedRemedy*  
Change "Eye height vertical eye closure are measured"  
To "Eye height and vertical eye closure are measured"

Proposed Response Response Status

[Editor's note: Changed line from 43 to 53.]

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 163B SC 163B.1 P 297 L 12 # 22

Brown, Matt Huawei  
 Comment Type E Comment Status D

The test point name TP0a is now obsolete. References to TP0a in Annex 163B are also references to TP0v, but for a specific example.

*SuggestedRemedy*

In 163B.1 delete the second sentence.  
 In the first paragraph in 163B.2 change TP0a to TP0v.  
 In the heading of Table 163B-1, change TP0a to TP0v.

Proposed Response Response Status O

[Editor's note: Changed line from 297 to 12.]

Cl 162 SC 162.9.3 P 154 L 7 # 23

Brown, Matt Huawei  
 Comment Type T Comment Status X

In Table 162-10, the nominal unit interval is specified. This seems unnecessary and redundant (since it can easily be derived from the nominal signaling rate). It is not specified for KR, C2C, or C2C. For consistency with sister Clauses/Annexes, this specification should be removed.

*SuggestedRemedy*

In Table 162-10, remove row specifying the "Unit interval (nominal)".

Proposed Response Response Status O

Cl 136 SC 136.8.11 P 115 L 29 # 24

Marris, Arthur Cadence Design Systems  
 Comment Type TR Comment Status X

Need to point out that the Clause 136 control function is not just for 50G lane PMDs

*SuggestedRemedy*

Add the following extra paragraph to the end of 136.8.11:  
 "The PMD control function specified in this clause is not only used by 50 Gb/s per lane PMDs, but also by other PMDs, such as the 100 Gb/s per lane PMDs specified in Clause 162."

Proposed Response Response Status O

Cl 162A SC 162A.5 P 263 L 28 # 25

Laubach, Mark IEEE Member / Self  
 Comment Type E Comment Status X

"usingEquation" needs a space

*SuggestedRemedy*

Change to "using Equation"

Proposed Response Response Status O

Cl 91 SC 91.6 P 85 L 28 # 26

Laubach, Mark IEEE Member / Self  
 Comment Type E Comment Status X

Line breaking of "threshold" after the "t" doesn't look good.

*SuggestedRemedy*

Perhaps resizing the columns can make it look better or forcing a newline before the "t"?

Proposed Response Response Status O

Cl 119 SC 119.6.4.12 P 99 L 41 # 27

Laubach, Mark IEEE Member / Self  
 Comment Type E Comment Status X

Line break of "status" after "stat" doesn't look good.

*SuggestedRemedy*

Perhaps forcing a newline before "status"?

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.3 P 243 L 24 # 28

Mellitz, Richard Samtec

Comment Type TR Comment Status X

Reports of high VEC measurements were reported in calvin\_3ck\_02\_1020 suggest 50 nUI of Sj is a strong factor. The value of Sj seems to be inherited from older specification. Hence there does not seem to be a tie between Tx jitter measured and Rx jitter injected.

*SuggestedRemedy*

Based on extrapolation from J3u in 162 and 163 add to table 120G-6  
 Jitter (max)  
 Jrms = 0.23 UI refer to 120F.3.1.3  
 J4u = 0.129 UI refer to 120F.3.1.3  
 Even-odd jitter, pk-pk = 0.023 UI refer to 120F.3.1.3

Proposed Response Response Status O

CI 120G SC 120G.3.4 P 247 L 25 # 29

Mellitz, Richard Samtec

Comment Type TR Comment Status D

Reports of high VEC measurements were reported in calvin\_3ck\_02\_1020 suggest 50 nUI of Sj is a strong factor. The value of Sj seems to be inherited from older specification. Hence there does not seem to be a tie between Tx jitter measured and Rx jitter injected.

*SuggestedRemedy*

Based on extrapolation from J3u in 162 and 163 add to table 120G-10  
 Jitter (max)  
 Jrms = 0.23 UI refer to 120F.3.1.3  
 J4u = 0.129 UI refer to 120F.3.1.3  
 Even-odd jitter, pk-pk = 0.023 UI refer to 120F.3.1.3

Proposed Response Response Status O

[Editor's note: Changed subclause from 120G.3.2 to 120G.3.4.]

CI 120G SC 120G.3.3.3.1 P 245 L 49 # 30

Mellitz, Richard Samtec

Comment Type TR Comment Status X

There is more than a few dB VEC difference between simulations using the COM computation script using 0.025 UI of Add and measurements using 50 mUI of Sj for a 16 dB channel. The measured VEC with 50 mUI of Sj approaches 15.7 dB, The actual jitter injected during the a receiver compliance test may introduce a degree of instrument and test set up jitter uncertainty or amplification at the receiver test point.

*SuggestedRemedy*

Change p245 line 49  
 Random jitter and bounded uncorrelated jitter are added such that the output of the pattern generator approximates the output jitter profile given by maximum JRMS and maximum J4u, and complies with the even-odd jitter specification, in Table 120F-1.  
 To  
 Random jitter and bounded uncorrelated jitter are added such that the input to the host approximates the output jitter profile given by maximum JRMS and maximum J4u, and complies with the even-odd jitter specification, in Table 120G-6.  
 Other solutions are possible like lowering injected Sj to 20 mUI.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 248 L 12 # 31

Mellitz, Richard Samtec

Comment Type TR Comment Status X

There is more than a few dB VEC difference between simulations using the COM computation script using 0.025 UI of Add and measurements using 50 mUI of Sj for a 16 dB channel. The measured VEC with 50 mUI of Sj approaches 15.7 dB. The actual jitter injected during the a receiver compliance test may introduce a degree of instrument and test set up jitter uncertainty or amplification at the receiver test point.

*SuggestedRemedy*

Change p245 line 49  
 Random jitter and bounded uncorrelated jitter are added such that the output of the pattern generator approximates the output jitter profile given by maximum JRMS and maximum J4u, and complies with the even-odd jitter specification, in Table 120F-1.  
 To  
 Random jitter and bounded uncorrelated jitter are added such that the input to the host approximates the output jitter profile given by maximum JRMS and maximum J4u, and complies with the even-odd jitter specification, in Table 120G-10.  
 Other solutions are possible like lowering injected Sj to 20 mUI.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.9.3.4 P 158 L 39 # 32  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 "Meeting even-odd jitter requirement with only one CRU bandwidth is sufficient" is not clear  
 SuggestedRemedy  
 What is the intention of only one CRU bandwidth, please make it clear.  
 Proposed Response Response Status **O**

CI 162 SC 162.9.4.3 P 161 L 36 # 33  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 Table 162-14 references table 110-8 and figure 110-3b, but unlike CL 110 for the case of low loss channel Test 1 frequency dependent attenuator is zero because the loss of cable assembly=test channel loss  
 SuggestedRemedy  
 If the low loss channel also include frequency dependent attenuator then please increase loss by 4.75 dB, if the intention was to not include frequency dependent attenuator then a note would be helpful  
 Proposed Response Response Status **O**

CI 120G SC 120G.3.2 P 240 L 10 # 34  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **D**  
 Given that now we have AUI-S/L far end eye would be AUI-S min eye opening  
 SuggestedRemedy  
 The eye opening with 50 mUI rectangular window for AUI-L is VEO=11 mV, see ghiasi\_3ck\_01\_0121  
 Proposed Response Response Status **O**  
 [Editor's note: Changed page/line from 164/13 to 240/10.]

CI 162 SC 162.9.4.4.2 P 164 L 25 # 35  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **ER** Comment Status **D**  
 Receiver jitter tolerance test point B to F test frequencies are ~2.5x but test point A and B are a decade apart  
 SuggestedRemedy  
 Please add additional test frequency between A and B at 133 KHz with amplitude of 1.5 UI  
 Proposed Response Response Status **O**  
 [Editor's note: Changed page from 234 to 164.]

CI 162 SC 162.11.7.2 P 174 L 8 # 36  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 Table 162-20 should be updated with MDI supporting 112G  
 SuggestedRemedy  
 Please replace SFP+ with SFP112  
 SFP-DD with SFP-DD112  
 QSFP+ with QSFP112  
 Proposed Response Response Status **O**

CI 163 SC 163.10.7 P 198 L 31 # 37  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 Given that we have increased Baudrate it is logical to increase 3 dB cutoff by factor 2  
 SuggestedRemedy  
 Please increase 3 dB cutoff from 50 KHz to 100 KHz given that this standard is operating at 2x Baudrate of 802.3cd. It is well understood that if one needs to support 50G PAM4 then DC block corner frequency will be 50 KHz, but keeping 50 KHz for 100G PAM4 it just will force 200G gets force to 50 KHz assuming one generation support  
 Proposed Response Response Status **O**

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 162 SC 162.11 P 165 L 43 # 38

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

Given that we have increased Baudrate it is logical to increase 3 dB cutoff by factor 2

*SuggestedRemedy*

Please increase 3 dB cutoff from 50 KHz to 100 KHz given that this standard is operating at 2x Baudrate of 802.3cd. It is well understood that if one needs to support 50G PAM4 then DC block corner frequency will be 50 KHz, but keeping 50 KHz for 100G PAM4 it just will force 200G gets force to 50 KHz assuming one generation support

Proposed Response Response Status O

Cl 120G SC 120G.3.1 P 237 L 17 # 39

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

VEC limit of 12 dB and VEO limit of 10 mV results in well constructed host to fail, this was not the case prior to adding timing window of +/-50 mUI.

*SuggestedRemedy*

The agreement was not to shift the burden for host or module when we defined new values for VEC and VEO based on timing window  $t_s = \pm 50$  mUI. Unfortunately the VEC and VEO limits result in host that passed now will fail. Propose new limits for VEO=8 mV and VEC=13.5 dB and see ghiasi\_3ck\_01\_0421

Proposed Response Response Status O

Cl 120G SC 120G.3.2.1 P 240 L 37 # 40

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

Table 120G-4 defines AUI short and long but with proper reference

*SuggestedRemedy*

Please reference table 120G-5

Proposed Response Response Status O

Cl 120G SC 120G.3.2.2.1 P 242 L 10 # 41

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status D

Table 120G-5 PCB length are for the reference MCB but based on construction the MCB loss may vary

*SuggestedRemedy*

Add note to the table that above PCB length assumes an MCB loss of 2.4 dB, please also list the PCB losses in dB instead of every reader trying to calculate

80 mm = 3.1 dB  
160 mm = 6.6 dB  
244.7 mm = 9.6 dB

To account for any difference in MTF loss from 6.6 dB it would be better to list the dB value for the trace+MTF and list the PCB lengths as reference, in that case then

80 mm becomes = 3.1+6.6 = 9.7 dB  
160 mm becomes = 6.6+6.6 dB=13.2 dB  
244.7 mm 9.6 + 6.6 dB=16.2 dB

Looking at Ghiasi\_3ck\_01\_0421 there are several issues with above limits:

1. Max trace loss need to be reduced from 244.7 mm to 239.7 mm so the max loss is 16 dB
2. Current 160 mm max range for short results in excess VEC propose to reduce 132.6 mm (5.2 dB)

The proposed optimized new limits become:  
Short 6.6 - 11.8 dB (include 6.6 dB MTF loss)  
Long 9.7 - 16 dB (include 6.6 dB MTF loss)

Proposed Response Response Status O

[Editor's note: Changed subclause from 120G.3.2.2 to 120G.3.2.2.1.]

Cl 120G SC 120G.3.1 P 237 L 17 # 42

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status X

VEC limit of 12 dB and VEO limit of 10 mV results in well constructed host to fail, this was not the case prior to adding timing window of +/-50 mUI.

*SuggestedRemedy*

The agreement was not to shift the burden for host or module when we defined new values for VEC and VEO based on timing window  $t_s = \pm 50$  mUI. Unfortunately the VEC and VEO limits result in host that passed now will fail.

Propose new limits for VEO=8 mV and VEC=13.25 to 13.75 dB and see ghiasi\_3ck\_01\_0421

Proposed Response Response Status W

[Editor's note: Changed page from 233 to 237 and subclause from 120G.3.1.5 to 120G.3.1]



EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.3.3.1 P 245 L 25 # 43  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **T** Comment Status **X**  
 Receiver jitter tolerance test point B to F test frequencies are ~2.5x but test point A and B are a decade apart  
 SuggestedRemedy  
 Please add additional test frequency between A and B at 133 KHz with amplitude of 1.5 UI  
 Proposed Response Response Status **O**

CI 120G SC 120G.3.4.1 P 247 L 46 # 46  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **D**  
 Table 120G-10 needs to be updated now that measurements are with 50 mUI window  
 SuggestedRemedy  
 See ghiasi\_3ck\_01\_0121 and reduce eye height window from 15 mV to 9.5 mV  
 See ghiasi\_3ck\_01\_0121 and reduce eye height window from 7.5 dB to 14+/- 0.5 dB  
 Proposed Response Response Status **O**  
 [Editor's note: Changed page from 240 to 247.]

CI 120G SC 120G.5.2 P 252 L 16 # 44  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 gDC max value may result in very large VEC > 20 dB when module are tuned in the middle of range if plugged into min loss host.  
 SuggestedRemedy  
 Suggest reducing gDC from -2 to -1 and see ghiasi\_3ck\_01\_0421  
 Proposed Response Response Status **O**

CI 120G SC 120G.5.2 P 253 L 27 # 47  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 The new C2M test procedure no longer require eye opening measurement with introduction of timing window tx=+- 50 mUI, given the amount f change it will be very confusing for the reader to follow the procedure!  
 SuggestedRemedy  
 Please include a figure and full procedure in CL120G instead of referencing 120E  
 Proposed Response Response Status **O**

CI 162C SC 162C.1 P 277 L 20 # 45  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 Table 162C-1 should be updated with MDI supporting 112G  
 SuggestedRemedy  
 Please replace SFP+ with SFP112  
 SFP-DD with SFP-DD112  
 QSFP+ with QSFP112  
 Proposed Response Response Status **O**

CI 162B SC 162B.1.3.1 P 269 L 36 # 48  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 FOMILD of 0.13 dB is horibale for an MTF and it is signficnalty larger than Lim 2 inch channel with 5 dB  
 SuggestedRemedy  
 Reduce reduce ILD to 0.075, please ghiasi\_3ck\_01\_0421  
 Proposed Response Response Status **O**

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 163 SC 163.9.2.2 P 189 L 38 # 49  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 No reference to Annex 163B which provide referene ERL  
 SuggestedRemedy  
 Please provide reference to CL 163B  
 Proposed Response Response Status **O**

Cl 162B SC 162B.2 P 297 L 22 # 53  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 We have provided reference ERL for only 31 mm package  
 SuggestedRemedy  
 Please also provide ERL data for the 12 mm package as well  
 Proposed Response Response Status **O**

Cl 162 SC 162.11.7 P 170 L 18 # 50  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **ER** Comment Status **D**  
 Unit for Zc should be ohms not Farad  
 SuggestedRemedy  
 Change to ohms  
 Proposed Response Response Status **O**  
 [Editor's note: Changed subclause from 162.11.7.1 to 162.11.7.]

Cl 120F SC 120F.3.1.1 P 220 L 22 # 54  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 No reference to Annex 163B which provide referene ERL  
 SuggestedRemedy  
 Please provide reference to CL 163B and explain that dERL of -3 dB would mean in case of reference package ERL 9.95 dB  
 Proposed Response Response Status **O**

Cl 162 SC 162.11.7 P 170 L 17 # 51  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **D**  
 Package delay Thao missing from table  
 SuggestedRemedy  
 Add package delay thao 5.79e-3 ns/mm  
 Proposed Response Response Status **O**  
 [Editor's note: Changed subclause from 162.11.7.1 to 162.11.7.]

Cl 163 SC 163.9.3 P 190 L 16 # 55  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **X**  
 No reference to Annex 163B which provide referene ERL  
 SuggestedRemedy  
 Please provide reference to CL 163B  
 Proposed Response Response Status **O**

Cl 163 SC 163.10.1 P 194 L 13 # 52  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **TR** Comment Status **D**  
 Package delay Thao missing from table  
 SuggestedRemedy  
 Add package delay thao 5.79e-3 ns/mm  
 Proposed Response Response Status **O**  
 [Editor's note: Changed page from 170 to 194.]

Cl 120G SC 120G.3.2.1 P 240 L 27 # 56  
 Ghiasi, Ali Ghiasi Quantum/Inphi  
 Comment Type **T** Comment Status **X**  
 Short and long are not very descriptive  
 SuggestedRemedy  
 Please replace short and long with "lower loss hosts" and "higher loss hosts"  
 Proposed Response Response Status **O**

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.11.7 P 170 L 41 # 57  
 Brown, Matt Huawei  
 Comment Type T Comment Status D  
 In Table 162-18 COM parameters for cable assembly, the step size for c(1) is 0.02 while in Table 163-10 (KR) and Table 120F-7 (C2C) the step size is 0.05. There is no reason for these values to be different.  
 SuggestedRemedy  
 Change the C(1) step size in Table 162-18 to 0.05 or alternately change C(1) step size in 163-10 and Table 120F-7 to 0.02.  
 Proposed Response Response Status O  
 [Editor's note: Changed subclause from 162.11.7.1 to 162.11.7.]

CI 162 SC 162.9.4.6 P 165 L 2 # 58  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 For Equation (162-9) specifying a limit for receiver differential to common-mode return loss there is no graph illustrating the limit.  
 SuggestedRemedy  
 Add figure with graph for Equation (162-9).  
 Proposed Response Response Status O

CI 162 SC 162.11.4 P 168 L 31 # 59  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Change Figure title to be consistent with text.  
 SuggestedRemedy  
 Change title to "Cable assembly differential to common-mode return loss"  
 Proposed Response Response Status O

CI 120F SC 120F.3.1 P 219 L 16 # 60  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 Change "Common-mode return loss" to "Common-mode to common-mode return loss" in Table 120F-1 and in PICS item TC8 in 120F.5.4.1.  
 Proposed Response Response Status O

CI 120F SC 120F.3.2.2 P 223 L 2 # 61  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 In Equation 120F-1 and in the variable list that follows, change variable name RL\_dcm to Return\_Loss.  
 Proposed Response Response Status O

CI 120G SC 120G.3.1.1 P 237 L 36 # 62  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 In Equation 120G-1 and in the variable list that follows, change variable name RLDC to Return\_Loss.  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.3.1 P 243 L 34 # 63  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 In Equation 120G-2 and in the variable list that follows, change variable name RLCD to Return\_Loss.  
 Proposed Response Response Status O

CI 162B SC 162B.1.3.5 P 272 L 31 # 66  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 In Equation 162B-8 and in the variable list that follows, change variable name CMDRL to Return\_Loss.  
 Proposed Response Response Status O

CI 162B SC 162B.1.3.4 P 271 L 26 # 64  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 Change "common-mode return loss" to "Common-mode to common-mode return loss" in four places and in PICS item TF5.  
 Proposed Response Response Status O

CI 162 SC 162.11.5 P 169 L 20 # 67  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Change Figure 162-7 title to be consistent with text.  
 SuggestedRemedy  
 Change title to "Cable assembly differential to common-mode conversion loss"  
 Proposed Response Response Status O

CI 162B SC 162B.1.3.4 P 271 L 30 # 65  
 Brown, Matt Huawei  
 Comment Type E Comment Status X  
 Align terminology with other clauses.  
 SuggestedRemedy  
 In Equation 162B-7 and in the variable list that follows, change variable name CMRL to Return\_Loss.  
 Proposed Response Response Status O

CI 1 SC 1.1.3.2 P 31 L 18 # 68  
 Wienckowski, Natalie General Motors  
 Comment Type E Comment Status X  
 Subject/verb agreement (each is singular) & grammar ("of" does not belong).  
 SuggestedRemedy  
 Change: For each of chip-to-chip and chip-to-module interfaces  
 To: For each chip-to-chip and chip-to-module interface  
 The same change is needed on P31L35 & P31L50.  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 1 SC 1.4.36 P 33 L 5 # 69

Wienckowski, Natalie General Motors

Comment Type E Comment Status X

Subject/verb agreement (each is singular) & grammar ("of" does not belong).

*SuggestedRemedy*

Change: For each of chip-to-module and chip-to-chip interconnections  
 To: For each chip-to-module and chip-to-chip interconnection  
 The same change is needed on P33L33 & P34L5.

Proposed Response Response Status O

Cl 30 SC 30.5.1.1.2 P 35 L 17 # 70

Wienckowski, Natalie General Motors

Comment Type E Comment Status X

Inconsistent wording for the cable type  
 P32L30, P33L17, P33L44, P73L31, P73L35: shielded balanced copper cabling  
 P35L17, P35L27, P35L37: shielded copper balanced cable

*SuggestedRemedy*

Change: shielded copper balanced cable  
 To: shielded balanced copper cabling  
 on P35L17, P35L27, & P35L37.

Proposed Response Response Status O

Cl 00 SC 0 P 0 L 0 # 71

Wienckowski, Natalie General Motors

Comment Type E Comment Status X

For all additions to tables, if there are rows before or after the rows shown in the spec, there needs to be a blank, merged row with an elipses in it to indicate all places where there are additional rows not shown. Search for "unchanged rows not shown" to find places where this is needed.

*SuggestedRemedy*

Add additional rows, merged row with an elipses in it, to the top and/or bottom of tables as needed to indicate additional rows that are not shown.

Proposed Response Response Status O

Cl 45 SC 45.2.1.135a P 55 L 12 # 72

Wienckowski, Natalie General Motors

Comment Type T Comment Status X

Unused bit combinations should be "reserved"

*SuggestedRemedy*

add a row with "0 1 x =Reserved" and  
 add a row with "1 0 0 =Reserved"  
 This also needs to be done on P56L7, P57L13, P58L7, & P152L23.

Proposed Response Response Status O

Cl 161 SC 161.5.2.6 P 123 L 41 # 73

Wienckowski, Natalie General Motors

Comment Type T Comment Status X

I believe there is a typo as it doesn't make sense to transmit PCS lane 0 on both FEC lanes 0 and 1. The second "0" should be "1" on FEC lane 1. This change also makes it match with Figure 161-3.

*SuggestedRemedy*

Change: the alignment marker payloads corresponding to PCS lanes 0, 5, 9, 13, and 17 are transmitted on FEC lane 1,  
 To: the alignment marker payloads corresponding to PCS lanes 1, 5, 9, 13, and 17 are transmitted on FEC lane 1,

Proposed Response Response Status O

Cl 1 SC 1.1.3.2 P 31 L 18 # 74

Huber, Tom Nokia

Comment Type E Comment Status X

Awkward grammar: "For each of chip-to-chip and chip-to-module interfaces, four widths of CAUI-n/100GAUI-n are defined..."

*SuggestedRemedy*

The introductory clause seems unnecessary since the preceding sentence already establishes the use of CAUI-n/100GAUI-n for C2C and C2M interfaces. Change to "Four widths of CAUI-n and 100GAUI-n are defined..."

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 1 SC 1.1.3.2 P31 L 34 # 75  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 Awkward grammar: "For each of chip-to-chip and chip-to-module interfaces, three widths of 200GAUI-n are defined...".  
*SuggestedRemedy*  
 The introductory clause seems unnecessary since the preceding sentence already establishes the use of 200GAUI-n for C2C and C2M interfaces. Change to "Three widths of 200GAUI-n are defined...".  
 Proposed Response Response Status

Cl 1 SC 1.4.87 P33 L 33 # 78  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 Awkward grammar: "For each of chip-to-chip and chip-to-module interfaces, three widths of 200GAUI-n are defined...".  
*SuggestedRemedy*  
 The introductory clause seems unnecessary since the preceding sentence already establishes the use of 200GAUI-n for C2C and C2M interfaces. Change to "Three widths of 200GAUI-n are defined...".  
 Proposed Response Response Status

Cl 1 SC 1.1.3.2 P31 L 50 # 76  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 Awkward grammar: "For each of chip-to-chip and chip-to-module interfaces, three widths of 400GAUI-n are defined...".  
*SuggestedRemedy*  
 The introductory clause seems unnecessary since the preceding sentence already establishes the use of 400GAUI-n for C2C and C2M interfaces. Change to "Three widths of 400GAUI-n are defined...".  
 Proposed Response Response Status

Cl 1 SC 1.4.111 P34 L 5 # 79  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 Awkward grammar: "For each of chip-to-chip and chip-to-module interfaces, three widths of 400GAUI-n are defined...".  
*SuggestedRemedy*  
 The introductory clause seems unnecessary since the preceding sentence already establishes the use of 400GAUI-n for C2C and C2M interfaces. Change to "Three widths of 400GAUI-n are defined...".  
 Proposed Response Response Status

Cl 1 SC 1.4.36 P33 L 5 # 77  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 Awkward grammar: "For each of chip-to-chip and chip-to-module interfaces, four widths of CAUI-n/100GAUI-n are defined...".  
*SuggestedRemedy*  
 The introductory clause seems unnecessary since the preceding sentence already establishes the use of CAUI-n/100GAUI-n for C2C and C2M interfaces. Change to "Four widths of CAUI-n and 100GAUI-n are defined...".  
 Proposed Response Response Status

Cl 69 SC 69.1.2 P63 L 6 # 80  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 The editing instruction indicates that unchanged items are not included, yet items i) and j) have no changes indicated.  
*SuggestedRemedy*  
 Remove items i) and j), or change the editing instruction to indicate that 'some unmodified items are not included'.  
 Proposed Response Response Status

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 69 SC 69.2.3 P 64 L 48 # 81  
 Huber, Tom Nokia  
 Comment Type T Comment Status X  
 Not part of the new text for table 69-3b, but the title of clause 137 is incorrect in the table  
 SuggestedRemedy  
 Change 100GBASE-KR4 PMD to 200GBASE-KR4 PMD  
 Proposed Response Response Status O

CI 116 SC 116.1.2 P 90 L 44 # 84  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 The last part of the text that is new, "for 400GBASE-KR4", is not shown as changed text (with an underline)  
 SuggestedRemedy  
 Underline "for 400GBASE-KR4" so all changed text is identified.  
 Proposed Response Response Status O

CI 91 SC 91.6 P 85 L 26 # 82  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 The newly inserted row is not marked as such. Other tables with a mix of inserted rows and existing rows have underlined text for the new rows.  
 SuggestedRemedy  
 Underline the text of the new row.  
 Proposed Response Response Status O

CI 161 SC 161.5.2.6 P 123 L 41 # 85  
 Huber, Tom Nokia  
 Comment Type T Comment Status X  
 Incorrect list of PCS lanes for FEC lane 1: 0, 5, 9, 13, and 17  
 SuggestedRemedy  
 Change 0 to 1.  
 Proposed Response Response Status O

CI 91 SC 91.6.2f P 86 L 7 # 83  
 Huber, Tom Nokia  
 Comment Type E Comment Status X  
 Awkward grammar - "When 100G\_RS\_FEC\_Enable variable is set..."  
 SuggestedRemedy  
 Add 'the' in front of 10G\_RS\_FEC\_Enable: "When the 100G\_RS\_FEC\_Enable variable is set..."  
 Proposed Response Response Status O

CI 162 SC 162.14.3 P 176 L 31 # 86  
 Huber, Tom Nokia  
 Comment Type T Comment Status X  
 Status for implementing the 100G FECs should be CR1 rather than CR2  
 SuggestedRemedy  
 Change CR2 to CR1  
 Proposed Response Response Status O

CI 163 SC 163.13.3 P 200 L 13 # 87  
 Huber, Tom Nokia  
 Comment Type T Comment Status X  
 Status for implementing the clause 135 PMA should be KR1 rather than KR  
 SuggestedRemedy  
 Change KR to KR1  
 Proposed Response Response Status O

CI 162B SC 162B.1.3.1 P 269 L 36 # 88  
 Tracy, Nathan TE Connectivity  
 Comment Type **TR** Comment Status **D**  
 FOM\_ILD limit of 0.13 dB does not allow for manufacturing variations of mated test boards  
 Suggested Remedy  
 change limit to 0.18dB  
 Proposed Response Response Status **O**  
 [Editor's note: Changed subclause from 162B.1.3 to 162B.1.3.1.]

CI 30 SC 30.5.1.1.16 P 35 L 50 # 89  
 Slavick, Jeff Broadcom  
 Comment Type **T** Comment Status **D**  
 aFECmode was updated to include an enumeration for the Interleave FEC found in CI161, but the text has not been updated.  
 Suggested Remedy  
 Change the BEHAVIOR DEFINED AS: to read as follows:  
 A read-write value that indicates the mode of operation of the FEC sublayer for forward error correction (see 65.2, Clause 74, Clause 91, Clause 108, and Clause 161).  
 A GET operation returns the current mode of operation of the PHY. A SET operation changes the mode of operation of the PHY to the indicated value. The enumerations "BASE-R enabled", "RS-FEC enabled" and "RS-FEC-Int enabled" are only used by PHYs which support more than one type of FEC operation. For 25GBASE-CR, 25GBASE CR-S, 25GBASE-KR, and 25GBASE-KR-S PHYs operation in the no-FEC mode maps to the enumeration "disabled", operation in the BASE-R FEC mode maps to the enumeration "BASE-R enabled", and operation in the RS-FEC mode maps to the enumeration "RS-FEC enabled" (see 110.6 and 111.6). For 100GBASE-CR1 and 100GBASE-KR1 PHYs operation in RS-FEC mode maps to the enumeration "RS-FEC enabled" (see 91.6.2f) and operation in interleaved RS-FEC mode maps to the enumeration "RS-FEC-Int enabled" (see 161.6.23).  
 When Clause 73 Auto-Negotiation is enabled for a 25GBASE-R PHY, a SET operation is not allowed and a GET operation maps to the variables FEC\_enable in Clause 74 and FEC\_enable in Clause 108. When Clause 73 Auto-Negotiation is enabled for a non-25GBASE-R PHY supporting Clause 74 FEC a SET operation is not allowed and a GET operation maps to the variable FEC\_enable in Clause 74. When Clause 73 Auto-Negotiation is enabled for a 100GBASE--R PHY supporting Clause 161 FEC a SET operation is not allowed and a GET operation maps to the variable 100G\_RS\_FEC\_enable in Clause 91 and 100G\_RS\_FEC\_Int\_enable in Clause 161.  
 If a Clause 45 MDIO Interface is present, then this attribute maps to the appropriate FEC control register based upon the PHY type and the FEC operating mode (see 45.2.10.3, 45.2.1.102 and 45.2.1.110).  
 Proposed Response Response Status **O**  
 [Editor's note: Changed comment type from TR to T.]



EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 30 SC 30.5.1.1.17 P 36 L 35 # 90  
 Slavick, Jeff Broadcom  
 Comment Type T Comment Status D  
 aFECCorrectedBlocks needs to add the RS-FEC-Int into the laundry list of FEC types  
 SuggestedRemedy  
 Bring in the last paragraph of 30.5.1.1.17 and change "RS-FEC" to "RS-FEC and RS-FEC-Int"  
 Proposed Response Response Status O  
 [Editor's note: Changed comment type from TR to T.]

CI 30 SC 30.5.1.1.18 P 36 L 35 # 91  
 Slavick, Jeff Broadcom  
 Comment Type T Comment Status D  
 aFECUncorrectedBlocks needs to add the RS-FEC-Int into the laundry list of FEC types  
 SuggestedRemedy  
 Bring in the last paragraph of 30.5.1.1.18 and change "RS-FEC" to "RS-FEC and RS-FEC-Int"  
 Proposed Response Response Status O  
 [Editor's note: Changed comment type from TR to T.]

CI 45 SC 45.2.7.12a.a P 60 L 52 # 92  
 Slavick, Jeff Broadcom  
 Comment Type T Comment Status X  
 The RS-FEC-Int negotiated field is valid for all 100GBASE-P PHYs that supporting negotiating it. But text some "some" so  
 SuggestedRemedy  
 Align the text with how RS-FEC negotiated reads. Change the last sentence to read "This bit is set only when RS-FEC-Int operation been negotiated for a 100GBASE-P PHY supporting negotiation of RS-FEC-Int operation."  
 Proposed Response Response Status O

CI FM SC 0 P 3 L 2 # 93  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status D  
 Abstract does not mention addition of Annex 163A and 163B  
 SuggestedRemedy  
 Annex 120F, Annex 120G, Annex 162A through Annex 162D, Annex 163A and Annex 163B  
 Proposed Response Response Status O  
 [Editor's note: Changed clause from 00 to FM.]

CI FM SC 0 P 13 L 29 # 94  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status D  
 Abstract does not mention addition of Annex 163A and 163B  
 SuggestedRemedy  
 Annex 120F, Annex 120G, Annex 162A through Annex 162D, Annex 163A and Annex 163B  
 Proposed Response Response Status O  
 [Editor's note: Changed clause from 00 to FM and page from 13 to 14.]

CI 1 SC 1.4.36 P 33 L 10 # 95  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status X  
 Remove full-stop before closing brace  
 SuggestedRemedy  
 for 100GAUI-1)  
 Proposed Response Response Status O

CI 1 SC 1.4.87 P 33 L 37 # 96  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status X  
 Remove full-stop before closing brace  
 SuggestedRemedy  
 200GAUI-2)  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 1 SC 1.4.111 P 34 L 9 # 97  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status X  
 Remove full-stop before closing brace  
 SuggestedRemedy  
 400GAUI-4)  
 Proposed Response Response Status O

Cl 69 SC 69.2.3 P 63 L 43 # 98  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status X  
 Typo-error; 200Gb/s mentioned as 100Gb/s  
 SuggestedRemedy  
 the PMD defined in Clause163, and specifies 200Gb/s operation using 4-level PAM over two differential  
 Proposed Response Response Status O

Cl 162 SC 162.1 P 140 L 26 # 99  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status X  
 Typo-error for Clause number corresponding to RS/CGMII functions  
 SuggestedRemedy  
 Correct Clause number to "81" instead of "80" in row 1 and row 2 of Table 162-1  
 Proposed Response Response Status O

Cl 163 SC 163.1 P 181 L 24 # 100  
 Kabra, Lokesh Synopsys Inc  
 Comment Type E Comment Status X  
 Typo-error for Clause number corresponding to RS/CGMII functions  
 SuggestedRemedy  
 Correct Clause number to "81" instead of "80" in row 1 and row 2 of Table 162-2  
 Proposed Response Response Status O

Cl 120 SC 120.5.2 P 102 L 11 # 101  
 Ran, Adeo Cisco  
 Comment Type E Comment Status X  
 "when the number of physical lanes is 2 or 4" is inconsistent with the remainder of this sentence which has "8 or 4", and with the first paragraph of 120.5.  
 Other places with "2 or 4" are 120.5.5 (P102 L25), 120.5.7.1 (P103 L12 and L20), and 120.5.11.2 (P104 L16) - in those cases the corresponding 400G PMA is stated as having "4 or 8" lanes. That is an inconsistency in the base document, which may be fixed in the revision project, so I'm not proposing changing those cases now.

SuggestedRemedy  
 Change "2 or 4" to "4 or 2", at this point only in 102.5.2.  
 Proposed Response Response Status O

Cl 120 SC 120.7.3 P 106 L 30 # 102  
 Ran, Adeo Cisco  
 Comment Type ER Comment Status X  
 In items UNAU and DNAUI, "through Annex 120G" is a newly inserted text.  
 SuggestedRemedy  
 Mark with underline in both cases.  
 Proposed Response Response Status O

Cl 135 SC 135.1.4 P 109 L 15 # 103  
 Ran, Adeo Cisco  
 Comment Type E Comment Status X  
 In Figure 135-2, in "PMA (4:n)" the letter "n" is not italicized (it is italic everywhere else).  
 Also, in "PMA (n:p)", "n" is italic but "p" is not (but p is italic in the legend).  
 Also applies to Figure 120A-8 in 120A.5 where p and n are used but not italicized.  
 SuggestedRemedy  
 Change the format of the "n" and "p" to italic, across both figures.  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 135 SC 135.1.4 P 109 L 27 # 104  
 Ran, Adees Cisco  
 Comment Type E Comment Status X  
 The term "PHY" does not appear in the new Figure 135-2, so it is not required in the legend.  
 SuggestedRemedy  
 Delete "PHY = PHYSICAL LAYER DEVICE".  
 Proposed Response Response Status O

Cl 135 SC 135.7.3 P 113 L 6 # 105  
 Ran, Adees Cisco  
 Comment Type TR Comment Status X  
 PICS item NLA in 802.3cd has only the options 2, 4, or N/A for 100G. This project adds 100GAUI-1 for which the value should be 1.  
 SuggestedRemedy  
 Bring in item NLA and add 1 as an optional value.  
 Proposed Response Response Status O

Cl 136 SC 136.8.11.7.2 P 116 L 10 # 106  
 Ran, Adees Cisco  
 Comment Type E Comment Status X  
 Missing space after "=".  
 SuggestedRemedy  
 Insert space.  
 Proposed Response Response Status O

Cl 136 SC 136.8.11.7.3 P 116 L 14 # 107  
 Ran, Adees Cisco  
 Comment Type TR Comment Status X  
 In the base document (802.3cd), 136.8.11.7.3 defines holdoff\_timer as being started only when entering the TIMEOUT state.  
 In this project we added a holdoff\_timer also when entering QUIET.  
 SuggestedRemedy  
 Bring in 136.8.11.7.3 and insert "or the QUIET state" after "the TIMEOUT state".  
 Proposed Response Response Status O

Cl 136 SC 136.9 P 118 L 1 # 108  
 Ran, Adees Cisco  
 Comment Type ER Comment Status X  
 The table to be modified is in 136.14.4.1 "PMD functional specifications", so the current subclause numbering is incorrect.  
 SuggestedRemedy  
 Change the 1st-level subclause number from 9 to 14, including the editorial instruction.  
 Proposed Response Response Status O

Cl 152 SC 152.6.2a P 119 L 29 # 109  
 Ran, Adees Cisco  
 Comment Type E Comment Status X  
 In 802.3 the word "sublayer" is conventionally used with no hyphen.  
 SuggestedRemedy  
 change "sub-layer" to "sublayer".  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 163 SC 163.9.2 P 187 L 40 # 110

Ran, Adeo Cisco

Comment Type E Comment Status X

Numerical values in standards are exact, so there should be no trailing zeros after the decimal point. This is the common practice in 802.3 (see [https://www.ieee802.org/3/WG\\_tools/editorial/requirements/words.html#numbers](https://www.ieee802.org/3/WG_tools/editorial/requirements/words.html#numbers)).

SuggestedRemedy

Change "1.0" to "1".

Proposed Response Response Status O

Cl 93A SC 93A.1.2.3 P 209 L 47 # 111

Ran, Adeo Cisco

Comment Type E Comment Status X

"unless alternate values are provided by the clause that invokes this method"

The word "alternate" seems odd here, I think "alternative" is more common for this meaning. It can also be simply "other".

(Note: in section 6, "alternative" appears 13 times and "alternate" appears 3 times, both with the same meaning. This may be handled by maintenance)

SuggestedRemedy

Change "alternate" to "alternative".

Proposed Response Response Status O

Cl 93A SC 93A.1.2.4 P 211 L 9 # 112

Ran, Adeo Cisco

Comment Type E Comment Status X

Figure 93A–2 includes network elements which represent components of the package and device model, but there is no description of these elements; the definitions are scattered through 93A.1.2 and its subclauses (some of which are not in this amendment). To an unexperienced reader it will be much harder than necessary to understand what each element is.

The suggested remedy is to add a legend to the figure. Alternatively, labels and arrows can be used instead.

SuggestedRemedy

Add a legend to Figure 93A–2, with text based on the following:

S<sup>(d)</sup> = scattering parameters corresponding to C<sub>d</sub>

S<sup>(l)</sup> = scattering parameters corresponding to a transmission line with length z<sub>p</sub>

S<sup>(s)</sup> = scattering parameters corresponding to L<sub>s</sub>

(and so on)

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 93A SC 93A.5.2 P 214 L 34 # 113

Ran, Adeo Cisco

Comment Type TR Comment Status X

This amendment uses T<sub>fx</sub> as a parameter of ERL calculation.

T<sub>fx</sub> originally appears in Equation (93A-62), which is not included in this amendment (added by 802.3cd), with the text

"T<sub>fx</sub> is twice the propagation delay in ns associated with the test fixture, obtained by measurement or inspection"

This text does not hold for the cases where the ERL is defined in this amendment; in some cases T<sub>fx</sub> is defined as 0 or 0.2 ns (regardless of the test fixture), in other cases it is twice the delay between two specified test points (e.g. TP0 and TP0v).

*SuggestedRemedy*

Add 93A.5.2 and change the text following Equation (93A-62), adding after the quoted sentence:

", unless its value is specified by the clause that invokes this method"

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 219 L 10 # 114

Ran, Adeo Cisco

Comment Type TR Comment Status X

The common mode voltage limits for C2C transmitter should have been changed to 1.0 V max and 0.2 V min, as in the KR transmitter (Table 163-5).

This change has been requested in comment #58 against D1.1, which was resolved with AIP, but for some reason the resolution was implemented only in clause 163 and not here.

(the response to that comment was:  
ACCEPT IN PRINCIPLE.

The following presentation was reviewed by the task force:

[http://www.ieee802.org/3/ck/public/20\\_03/ran\\_3ck\\_01a\\_0320.pdf](http://www.ieee802.org/3/ck/public/20_03/ran_3ck_01a_0320.pdf)

Implement the changes proposed on slides 4 and 5 in the referenced presentation, except set the cutoff frequency to 50 kHz and maximum common mode voltage of 1V. Implement with editorial license.")

*SuggestedRemedy*

Change the common mode limits to 1 V and 0.2 V, as in Table 163-5.

Proposed Response Response Status O

CI 120F SC 120F.3.2.5 P 225 L 22 # 115

Ran, Adeo Cisco

Comment Type E Comment Status X

Table 120F-6 has a "reference" column that has identical values for all rows (136.8.11.7.1). This reference is repeated in the text following the table, so it is redundant. Note that the similar Table 120F-3 does not have this column.

If the reference column is omitted, the "management access" column can be widened to prevent breaking its title, as in Table 120F-3.

*SuggestedRemedy*

delete the "reference" column and adjust the width of remaining columns.

Proposed Response Response Status O

CI 120F SC 120F.5.4.1 P 232 L 39 # 116

Ran, Adeo Cisco

Comment Type TR Comment Status X

Item TC13 feature is "Transmitter precoder request" with no comment, and its status is M. However, the referenced 120F.1 says "Precoding may be enabled and disabled using the precoder request mechanism specified in 135F.3.2.1." (P218 L28), and this mechanism is explicitly optional. So requesting through this mechanism can't be mandatory.

It may be preferable to add the transmitter precoder request as a major (optional) feature, as done in annex 135F (802.3cd).

*SuggestedRemedy*

Change TC13 status from "M" to "O". Consider moving it to 120F.5.3.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 120F SC 120F.5.4.1 P 232 L 40 # 117

Ran, Adeo Cisco

Comment Type TR Comment Status X

Item TC14 is optional and points to 120F.3.1.2, which points to 120F.3.1.4, which is pointed to by item TC15 (mandatory). These two items are one and the same.

The transmitter control interface is mandatory; only its usage is described with the word "may", but it is not an optional feature. So TC15 is the correct one.

*SuggestedRemedy*

Remove item TC14.

Proposed Response Response Status O

Cl 120G SC 120G.3.1 P 237 L 13 # 118

Ran, Adeo Cisco

Comment Type T Comment Status D

Host output "AC common-mode output voltage (max, RMS)" is specified in Table 120G-1 as 17.5 mV.

This value is tighter than what is allowed for CR transmitter measured at the same point (30 mV) and also tighter than the specification for KR/C2C.

Analysis of the effect of 17.5 mV vs. 30 mV has not been provided. Devices with higher AC CM output have been demonstrated to operate with real receivers at acceptable BER on a variety of channels.

Unless evidence is provided that 30 mV is unacceptable with real receivers, the limit should be aligned with the CR specification.

Applies similarly to Module output characteristics in Table 120G-3.

*SuggestedRemedy*

Change the value for AC common-mode output voltage (max, RMS) from 17.5 to 30, in Table 120G-1 and Table 120G-3.

Proposed Response Response Status O

[Editor's note: Line number changed from blank to 13.]

Cl 120G SC 120G.3.3.3.1 P 244 L 53 # 119

Ran, Adeo Cisco

Comment Type TR Comment Status X

In the host input stressed eye calibration procedure, "The stressed signal is generated by adding sinusoidal jitter, random jitter, and bounded uncorrelated jitter to a clean pattern".

This signal does not necessarily represent a real module output, in which the EH and VEC can also be affected by additive noise (which is quite different from jitter in its effect on a receiver). Stressing the host with a high level of bounded uncorrelated jitter (which is not fully specified, and may create different stress for different DUTs) does not test its ability to operate with a noisy module.

Adjusting the VEC using additive noise, as done in the CR/KR/C2C tolerance tests, should at least be allowed instead of using "bounded uncorrelated jitter"; it may be preferable in some setups. For the time being, it is suggested as an alternative.

*SuggestedRemedy*

Add a wideband noise source to the diagram in Figure 120G-9, between the pattern generator and the HCB.

Add a description of the noise source to the text, with reference to 93C.1 (where noise source specification is defined) and setting f\_NSD1 to 1 GHz, as in 163.9.3.4.

Add that calibrating the noise source level is an alternative method to adding BUJ for calibrating the EH and VEC.

Editorial license is suggested, but if necessary for accepting the comment I can provide candidate text before comment resolution.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.3.3.1 P 245 L 41 # 120

Ran, Adeo Cisco

Comment Type E Comment Status X

In the host stressed input test procedure there is a "block" paragraph of 18 lines, which contains some 13 sentences, dealing with the bounded uncorrelated jitter (purpose, definition), calibration of jitter (BUJ and random), and crosstalk signal requirements and calibrations, with great detail and no clear list of requirements. This is painful to read (many times).

The paragraph should be broken to shorter paragraphs and possibly a list of requirements, to make it more legible, and separate requirements from informative explanations.

*SuggestedRemedy*

Rephrase and reformat as necessary.

If required, I can create a detailed proposal, but I trust the editors to be able to improve this paragraph by inspection.

Proposed Response Response Status O

CI 120G SC 120G.3.3.3.1 P 245 L 42 # 121

Ran, Adeo Cisco

Comment Type TR Comment Status X

The host stressed eye does not include any common-mode noise, even though a module output is allowed to have some common-mode AC content.

In a real system, the common-mode AC content of the module can be converted to differential noise at the host's receiver, via the S21DC of the host input channel, which is not specified at all. This will not be detected in the host test without common-mode content, and may not be addressed in host channel design - but it can cause compliant hosts to fail with real modules.

The common mode noise stress should be a sinusoid at any frequency up to the Nyquist frequency, and should be calibrated at TP4 to have the RMS value allowed for the module output in Table 120G-3.

*SuggestedRemedy*

In another comment I am suggesting to add a wideband noise source to the diagram in Figure 120G-9, between the pattern generator and the HCB.

If the other comment is accepted, an addition for this comment would be to make the noise source also have a common mode component. otherwise, add a common mode noise source in the same location instead.

Add the necessary text for calibrating the common mode output at TP4.

Editorial license is suggested, but if necessary for accepting the comment I can provide candidate text before comment resolution.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 247 L 49 # 122

Ran, Adeo Cisco

Comment Type T Comment Status X

The instructions for calibrating the module stressed input are unclear and unstructured, and there are missing parts, such as when and how VEC is optimized.

It would be better to write it as procedure separated to steps, as done for example in 120G.5.2, and in other receiver test procedures such as 110.8.4.2.1 through 110.8.4.2.5, or annex 93C.

*SuggestedRemedy*

A proposal for restructuring will be provided in a presentation.

Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 248 L 1 # 123

Ran, Adeo Cisco

Comment Type TR Comment Status X

In the module input stressed eye calibration procedure, "The stressed signal is generated by adding sinusoidal jitter, random jitter, and bounded uncorrelated jitter to a clean pattern, followed by frequency-dependent attenuation".

This signal does not necessarily represent a real host output, in which the EH and VEC can also be affected by additive noise (which is quite different from jitter in its effect on a receiver). Stressing the module with a high level of bounded uncorrelated jitter (which is not fully specified, and may create different stress for different DUTs) does not test its ability to operate with a noisy host.

Note that in a host transmitter it is often easier to control clock jitter than to reduce additive noise coupling from multiple sources in an ASIC.

Adjusting the VEC using additive noise, as done in the CR/KR/C2C tolerance tests, should at least be allowed instead of using "bounded uncorrelated jitter"; it may be preferable in some setups. For the time being, it is suggested as an alternative.

*SuggestedRemedy*

Add a wideband noise source to the diagram in Figure 120G-10, between the pattern generator and the frequency-dependent attenuator.

Add a description of the noise source to the text, with reference to 93C.1 (where noise source specification is defined) and setting f\_NSD1 to 1 GHz, as in 163.9.3.4.

Add that calibrating the noise source level is an alternative method to adding BUJ for calibrating the EH and VEC.

Editorial license is suggested, but if necessary for accepting the comment I can provide candidate text before comment resolution.

Proposed Response Response Status

CI 120G SC 120G.3.4.1.1 P 248 L 1 # 124

Ran, Adeo Cisco

Comment Type TR Comment Status X

The module stressed eye does not include any common-mode noise, even though a host output is allowed to have some common-mode AC content.

In a real system, the common-mode AC content of the host can degrade the module's (electrical) receiver performance, via the module's allowed termination mismatch or by circuit sensitivity. This will not be detected in the module test without common-mode content, and may not be addressed in design - but it can cause compliant modules to fail with real hosts.

For uncorrelated common mode noise, a sinusoidal source should be used. However, for the host output it is likely that common-mode content is generated by conversion from a differential signal and is therefore correlated to it. In this test, it is suggested that p/n skew is the preferred way to create the allowed common-mode RMS level.

*SuggestedRemedy*

In another comment I am suggesting to add a wideband noise source to the diagram in Figure 120G-10, between the pattern generator and the frequency-dependent attenuator.

For adding correlated common-mode noise, a skew between the p and n components of the frequency-dependent attenuator should be added and calibrated to create the allowed common-mode RMS level. Alternatively, a sinusoidal common-mode signal can be added, at any frequency up to the Nyquist frequency.

Add the necessary text for calibrating the common mode output at TP1a.

Editorial license is suggested, but if necessary for accepting the comment I can provide candidate text before comment resolution.

Proposed Response Response Status



EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.4.1.1 P 248 L 44 # 125

Ran, Adee Cisco

Comment Type TR Comment Status X

"For the high loss case, pre-emphasis capability is likely to be required in the pattern generator to meet the TP1a eye height and vertical eye closure specifications."

It is not specified what kind of pre-emphasis the pattern generator should include. In presentations to the task force, there were some assumptions about a CR host transmitter (3 precursors and 1 postcursor); it is reasonable to assume similar capabilities for a C2M host output.

Also, it should be explicitly permissible to use pre-emphasis for both high-loss and low-loss cases.

*SuggestedRemedy*

Delete "For the high-loss case,"

Add after this sentence: "The pattern generator is expected to be able to apply pre-emphasis equivalent to the Transmit equalizer functional model specified in 162.9.3.1. Pre-emphasis may be set separately for the high-loss and low-loss cases".

Proposed Response Response Status

CI 120G SC 120G.3.4.1.1 P 249 L 10 # 126

Ran, Adee Cisco

Comment Type TR Comment Status X

Here it is specified that "Random jitter and the pattern generator output levels are adjusted (...) to result in the eye height for all three eyes given in Table 120G-11"

But:

The random jitter level has already been adjusted in a prior step (P248 L15) "such that the output of the pattern generator approximates the output jitter profile given by maximum JRMS and maximum J4u".

Random jitter cannot satisfy both conditions. Adding higher jitter than J4u/JRMS specifications is an overstress (since host output should not have such higher jitter). Unlike low EH, high jitter cannot be compensated by simple Rx circuitry.

Eye height should be adjustable by pattern generator output level (after VEC has been obtained by other means; this is the subject of another comment) but not using random jitter.

*SuggestedRemedy*

Delete "Random jitter and".

Proposed Response Response Status

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 120G SC 120G.5.2 P 252 L 32 # 127

Ran, Adeo Cisco

Comment Type T Comment Status X

The reference receiver parameters fz, fp1, fp2, and gDC create CTLE transfer functions that are not necessarily passive (up to 0 dB across the spectrum) for all combinations.

This is different from the reference receiver used in the previous C2M specification (Annex 120E). Although 120E uses different equation and parameters, the resulting CTLE combinations always have combinations of the parameters Z1 and G that create 0 dB gain at the peaking frequency.

(The reference receiver CTLE in 120E is essentially similar to the one used in the COM method in all CR/KR specifications, in that the peaking is created by varying the zero while keeping the poles constant, with the zero being equal to fp1 for zero peaking; 120E has an addition of a flat gain G to create 0 dB maximum gain; this gain has no effect on COM, but does affect the eye height).

There was no indication or claim that the CTLE in this annex has better performance or better matches real designs than a CTLE similar to Annex 120E (with different peaking frequency). In fact, with the addition of a DFE to the reference receiver, a CTLE similar to the one in Annex 120F (C2C) may be more adequate, as the equalization at Nyquist frequency can utilize the DFE.

It is suggested to modify the reference receiver transfer functions to be similar to those of 120E. This requires a minor change in the definition of the CTLE in Annex 93A (COM).

*SuggestedRemedy*

Bring 93A.1.4.3 (Receiver equalizer) into the draft, and change Equation 93A-22 to include an additional factor G. Add a description of G below the equation:

"where G is a gain factor, whose value depends of the variable norm\_ctle as follows:

- If norm\_ctle is 1, G is set based on g\_DC, f\_z, g\_DC2, f\_LF, f\_p1, and fp2, such that the maximum of H\_ctf(f) across f is equal to 1.
- If norm\_ctle is 0 or is not provided by the clause that invokes this method, G is set to 1."

In Table 120G-12, change the values of f\_z and f\_p1 to f\_b/2.5, change the value of f\_p2 to f\_b, and add the parameter norm\_ctle with value 1.

A presentation with the effect of the proposed change will be provided.

Proposed Response Response Status O

Cl 136 SC 136.8.11.7.2 P 117 L 37 # 128

Law, David HPE

Comment Type T Comment Status X

The action 'start\_holdoff\_timer' in the QUIET state should read 'start holdoff\_timer', that is the underscore between start and holdoff\_timer should be a space. See timer conventions in 14.2.3.2 and 'start holdoff\_timer' in TIMEOUT state.

*SuggestedRemedy*

Change 'start\_holdoff\_timer' to read 'start holdoff\_timer'.

Proposed Response Response Status O

Cl 162 SC 162.9.3.1.1 P 155 L 44 # 129

Ben Artsi, Liav Marvell Technology

Comment Type TR Comment Status X

Defining a corner frequency for a clock recovery unit (CRU) can be ambiguous due to possible actual implementations of CRU implementations

*SuggestedRemedy*

Change the definition of a CRU unit with a definition of the effect expected from the CRU. The effect expected is a high frequency filter applied on the jitter of the measured signal. A reference for the wording can be found in 93.8 "The effect of a single-pole high-pass filter with a 3 dB frequency of XMHz is applied to the jitter"

Proposed Response Response Status O

Cl 162 SC 162.9.3.4 P 158 L 38 # 130

Ben Artsi, Liav Marvell Technology

Comment Type TR Comment Status X

Defining a corner frequency for a clock recovery unit (CRU) can be ambiguous due to possible actual implementations of CRU implementations

*SuggestedRemedy*

Change the definition of a CRU unit with a definition of the effect expected from the CRU. The effect expected is a high frequency filter applied on the jitter of the measured signal. A reference for the wording can be found in 93.8 "The effect of a single-pole high-pass filter with a 3 dB frequency of XMHz is applied to the jitter"

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.4.1.1 P 247 L 50 # 131

Ben Artsi, Liav Marvell Technology

Comment Type TR Comment Status X

Defining a corner frequency for a clock recovery unit (CRU) can be ambiguous due to possible actual implementations of CRU implementations

SuggestedRemedy

Change the definition of a CRU unit with a definition of the effect expected from the CRU. The effect expected is a high frequency filter applied on the jitter of the measured signal. A reference for the wording can be found in 93.8 "The effect of a single-pole high-pass filter with a 3 dB frequency of XMHz is applied to the jitter"

Proposed Response Response Status O

CI 162 SC 162.9.3.1.1 P 155 L 44 # 132

Ben Artsi, Liav Marvell Technology

Comment Type TR Comment Status X

Defining a corner frequency for a clock recovery unit (CRU) can be ambiguous due to possible actual implementations of CRU implementations

SuggestedRemedy

Change the definition of a CRU unit with a definition of the effect expected from the CRU. The effect expected is a high frequency filter applied on the jitter of the measured signal. A reference for the wording can be found in 93.8 "The effect of a single-pole high-pass filter with a 3 dB frequency of XMHz is applied to the jitter"

Proposed Response Response Status O

CI 162 SC 162.9.3.4 P 158 L 34 # 133

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type TR Comment Status X

A detail definition of twelve edges in PRBS9Q is recommended to improve reproducibility of even-odd jitter measurement.

This is re-submission of my comment #110 to draft D1.4.

SuggestedRemedy

Add a new table "PRBS9Q pattern symbols used for even-odd jitter measurements" similar to Table 120D-4, but replacing the values as follows:

Label: Description : Gray coded PAM4 symbol : first : TR begins : TR ends : last

REF	: Reference	: 33333	: 1	: -	: -	: 5
R03	: 0 to 3 rise	: 1000 331	: 260	: 263	: 264	: 266
F30	: 3 to 0 fall	: 233333 001	: 511	: 5	: 6	: 8
R12	: 1 to 2 rise	: 3111 23	: 265	: 268	: 269	: 270
F21	: 2 to 1 fall	: 1222 10	: 466	: 469	: 470	: 471
R01	: 0 to 1 rise	: 2000 13	: 195	: 198	: 199	: 200
F10	: 1 to 0 fall	: 21111 0003	: 256	: 260	: 261	: 264
R23	: 2 to 3 rise	: 3222 330	: 210	: 213	: 214	: 216
F32	: 3 to 2 fall	: 0333 20	: 401	: 404	: 405	: 406
R02	: 0 to 2 rise	: 2000 23	: 275	: 278	: 279	: 280
F20	: 2 to 0 fall	: 12222 001	: 321	: 325	: 326	: 328
R13	: 1 to 3 rise	: 0111 331	: 166	: 169	: 170	: 172
F31	: 3 to 1 fall	: 0333 10	: 107	: 110	: 111	: 112

Add an exception to use the new table instead of Table 120D-4, when PRBS9Q is used as the test pattern for even-odd jitter measurement.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 163 SC 163.9.3.4 P 192 L 34 # 134

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type TR Comment Status X

Equation (163-2) and (163-3) are not accurate, because the dual-dirac jitter distribution estimated by these equations does not match well with the original distribution even if the original distribution is pure dual-dirac distribution as presented at ad hoc meeting (see hidaka\_3ck\_adhoc\_01\_041421). For instance, J3u of the estimated dual-dirac jitter distribution is always significantly smaller than the measured J3u. I propose to change these equations.

Since the proposed equations never break, we do not need Note 2.

I propose similar changes to clause 162.9.4.3.3.

*SuggestedRemedy*

Replace Equation (163-2) and (163-3) with the following set of equations:

$$D3d = (Q3d^2 + 1) * (J\_RMS^2) - (J3u / 2)^2$$

If  $D3d \geq 0$ ,

$$A\_DD = (J3u / 2 + Q3d * \sqrt{D3d}) / (Q3d^2 + 1)$$

$$\sigma_{RJ} = (J3u / 2 - A\_DD) / Q3d$$

If  $D3d < 0$ ,

$$Qx = \sqrt{(J3u / 2 / J\_RMS)^2 - 1}$$

$$A\_DD = (J3u / 2) / (Qx^2 + 1)$$

$$\sigma_{RJ} = \sqrt{(J\_RMS^2) - (A\_DD^2)}$$

where  
Q3d = 3.0902

Change Note 1 as follows:

Note 1 -- Q3d is an approximated solution of  $Q(Q3d) = 1 \times 10^{(-3)}$ , where the Q function is defined in Equation (95-1).

Remove Note 2.

Apply the same changes to Equation (162-7), Equation (162-8), Note 1, and Note 2 in clause 162.9.4.3.3.

Change the references to Equation (162-7) and (162-8) in Note 2 of Table 162-15 in clause 162.9.4.4.2 with the updated equations.

Proposed Response Response Status

CI 120F SC 120F.3.2.3 P 224 L 2 # 135

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type TR Comment Status X

Equation (120D-10) and (120D-11) referred from 120F.3.2.3 step e are not accurate, because the dual-dirac jitter distribution estimated by these equations does not match well with the original distribution even if the original distribution is pure dual-dirac distribution. For instance, J4u of the estimated dual-dirac jitter distribution is always significantly smaller than the measured J4u. I propose to change these equations.

*SuggestedRemedy*

Add the following equations after step j, and change references to Equation (120D-10) and (120D-11) in step e with the new equations:

$$D4d = (Q4d^2 + 1) * (J\_RMS^2) - (J4u / 2)^2$$

If  $D4d \geq 0$ ,

$$A\_DD = (J4u / 2 + Q4d * \sqrt{D4d}) / (Q4d^2 + 1)$$

$$\sigma_{RJ} = (J4u / 2 - A\_DD) / Q4d$$

If  $D4d < 0$ ,

$$Qx = \sqrt{(J4u / 2 / J\_RMS)^2 - 1}$$

$$A\_DD = (J4u / 2) / (Qx^2 + 1)$$

$$\sigma_{RJ} = \sqrt{(J\_RMS^2) - (A\_DD^2)}$$

where  
Q4d = 3.7190

Add the following Note after the equation:

Note 1 -- Q4d is an approximated solution of  $Q(Q4d) = 1 \times 10^{(-4)}$ , where the Q function is defined in Equation (95-1).

Proposed Response Response Status

CI 162 SC 162.9.3.1 P 155 L 31 # 136

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type T Comment Status X

The number of initial conditions was increased from three to five.

*SuggestedRemedy*

Change "three initial conditions" to "five initial conditions".

Proposed Response Response Status

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 162 SC 162.9.4.1 P161 L4 # 137

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type T Comment Status X

The signalling-rate tolerance of transmitter was changed from 100ppm to 50ppm according to comment #42 on D1.3. However, the signaling-rate tolerance of receiver remained 100ppm. It is not clear whether it was an overlooked error or it remained 100ppm on purpose for compatibility with prior implementations with up to +/- 100ppm.

*SuggestedRemedy*

Add the following statement:

Note that the tolerance of signaling rate of transmitter is +/- 50ppm. The tolerance of signaling rate of receiver is +/- 100ppm for compatibility with prior transmitter implementations with up to +/- 100ppm tolerance.

Proposed Response Response Status O

Cl 163 SC 163.9.3.4 P192 L9 # 138

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type TR Comment Status X

The equation " $T_r = 1.09 * T_{rm} - 4.32 \text{ ps}$ " remains unchanged since it was adopted for clause 111 in IEEE P802.3by project to account for TP0 - TP0a effect. (See [https://www.ieee802.org/3/by/public/Jan16/ran\\_3by\\_01b\\_0116.pdf](https://www.ieee802.org/3/by/public/Jan16/ran_3by_01b_0116.pdf), slide 13.)

Correction of transition time by this equation is not valid any more, because the symbol rate has been doubled and the test point has been changed from TP0a to TP0v.

We should calibrate  $T_r$  at the signal source so that the reference transition time at TP0v including the effect of the reference package model and the test fixture matches to the measured transition time at TP0v.

When a BERT is used as TX, it is not necessary to calibrate the transition time at the signal source to match the measured transition time at TP0v, because it is easy to measure the transition time at the signal source (i.e. the BERT output) directly without the test fixture. Using the measured transition time directly at BERT output without calibration is more accurate and error free in comparison to calibrating the transition time at the signal source to match the measured transition time after the test fixture at TP0v.

Note that in the former specs, the correction of transition time must be used even if a BERT is used as TX, because the transition time must be measured at TP0a after the test fixture, not directly at the BERT output.

Note that this equation is not used in CR spec, because the transition time of the BERT output is directly measured without test fixture. This equation is also not used in OIF CEI spec, because the test point is equivalent to TP0, not TP0a in OIF CEI spec.

There is the same issue in 120F.3.2.3 step d.

*SuggestedRemedy*

Change step e as follows:

In the calculation of COM, if the transmitter is a device with known S-parameters and transition time  $T_r$ , these parameters should be used instead of the transmitter package model in 93A.1.2. If the transmitter is a calibrated instrument-grade transmitter, the transmitter device package model  $S^{(tp)}$  is omitted from Equation (93A-3), TP0 to TP0a trace or replica trace in Figure 93C-2 through Figure 93C-4 is omitted, and  $T_r$  in Equation (93A-46) is same as the measured 20% to 80% transition time  $T_{rm}$  of the signal source using the test setup in Figure 93C-3 without TP0 to TP0a trace. If the transmitter is not a device with known S-parameters and transition time nor a calibrated instrument-grade transmitter,  $T_r$  in Equation (93A-46) is calibrated so that the reference 20% to 80% transition time  $T_r^{(ref)}$  calculated according to 163A.3.1.X matches to the measured 20% to 80% transition time  $T_{rm}$  of the signal at TP0v using the test setup in Figure 93C-3 including TP0 to TP0v trace. The measured 20% to 80% transition time  $T_{rm}$  is measured with the transmitter equalizer turned off and using the method in 120E.3.1.5.

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Apply the same change as above to 120F.3.2.3 step d.

Add a new sub clause in 163A.3.1.X to calculate the reference 20% to 80% transition time  $Tr^{(ref)}$  using the following equation:

$$Tr^{(ref)} = T_{80} - T_{20} \quad (163A-X)$$

$$u(t) = \text{integral of } h(\tau)/T_b \text{ from } -\infty \text{ to } t \quad (163A-Y)$$

$T_{80}$  is a solution of  $u(t) = 0.8 * v^{(ref)}$  in terms of  $t$ .  
 $T_{20}$  is a solution of  $u(t) = 0.2 * v^{(ref)}$  in terms of  $t$ .

where  
 $Tr^{(ref)}$  is the reference 20% to 80% transition time.  
 $u(t)$  is the output step response.  
 $T_{80}$  is the time to reach 80% of the reference steady-state voltage.  
 $T_{20}$  is the time to reach 20% of the reference steady-state voltage.  
 $T_b$  is the unit interval in ps.  
 $v^{(ref)}$  is the reference steady-state voltage calculated by Equation (163A-3).

Obtain the output pulse response,  $h(t)$ , using Equation (93A-23) and Equation (93A-24) with  $H^{(0)}(f)$  from Equation (163A-2), where  $A_t$  and  $T_b$  are specified by the clause that invokes this method.  
 Obtain the output step response,  $u(t)$ , by integrating  $h(t)/T_b$  from minus infinite to  $t$  using Equation (163A-Y).  
 From the output step response, find the time to reach 20% and 80% of the reference steady-state voltage  $v^{(ref)}$  as  $T_{20}$  and  $T_{80}$ , respectively.  
 From  $T_{20}$  and  $T_{80}$ , calculate the reference 20% to 80% transition time  $Tr^{(ref)}$  using Equation (163A-X).

Proposed Response      Response Status

Cl 162      SC 162.9.4.3.3      P 162      L 26      # 139

Hidaka, Yasuo      Credo Semiconductor, Inc.

Comment Type    T      Comment Status    D

In 120E.3.1.5, transition time is measured with 33GHz BT4 filter.

*SuggestedRemedy*

Change "T\_r is measured using the method in 120E.3.1.5 with the transmit equalizer turned off (i.e., coefficients set to the preset 1 values, see 162.9.3.1.3)." to "T\_r is measured using the method in 120E.3.1.5 with the transmit equalizer turned off (i.e., coefficients set to the preset 1 values, see 162.9.3.1.3) with an exception that the waveform is observed through a fourth-order Bessel-Thomson low-pass response with a 3 dB bandwidth of 40 GHz.."

Proposed Response      Response Status

[Editor's note: changed subclause from 162.9.4.3 to 162.9.4.3.3.]

Cl 120G      SC 120G.3.4.1.1      P 248      L 17      # 140

Hidaka, Yasuo      Credo Semiconductor, Inc.

Comment Type    T      Comment Status    X

It says "The ERL of the test system as measured at TP1 meets the specification given in 120G.3.1.2."  
 120G.3.1.2 measures the host output ERL at TP1a rather than TP1.  
 Hence, the ERL of the test system is measured at TP1a, not at TP1.

*SuggestedRemedy*

Change  
 "The ERL of the test system as measured at TP1 meets the specification given in 120G.3.1.2."

to

"The return loss of the test system at TP1 meets the ERL specification given in 120G.3.1.2 when measured at TP1a."

Proposed Response      Response Status

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.9.3.4 P 158 L 34 # 141

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type TR Comment Status X

A detail definition of PRBS9Q with the entire sequence is recommended to avoid implementation errors.

This is re-submission of my comment #109 to draft D1.4.

SuggestedRemedy

Define PRBS9Q as a new clause in clause 120.5.11.2 using clause 120.5.11.2.1 as a template.

In the new clause, modify the second paragraph of the template (120.5.11.2.1) as follows:

When the PRBS9Q test pattern enabled, it replaces the signal on the output lane(s) for which it is enabled. The PRBS9Q test pattern is a repeating 511-symbol sequence formed by Gray coding pairs of bits from two repetitions of the PRBS9 pattern into PAM4 symbols as described in 120.5.7. The PRBS pattern generator produces the same result as the implementation shown in Figure XX-X, which implements the generator polynomial shown in Equation (YY-Y). Since the PRBS9 pattern is an odd number of bits in length, bits which are mapped as the first bit of a PAM4 symbol during one repetition of the PRBS9 sequence are mapped as the second bit of a PAM4 symbol during the next repetition of the PRBS9 sequence, and bits which are mapped as the second bit of a PAM4 symbol are mapped as the first bit of the following symbol in the next repetition of the PRBS9 sequence. For example, if the PRBS9 generator used to create the PRBS9Q sequence is initialized to a seed value of 111111111 (with the leftmost bit in S0 and the rightmost in S8), the PRBS9Q sequence is the following Gray coded PAM4 symbols, transmitted left to right:

```
0012322303231310010331213302202231320111030230213332303130303000
1003020031203332002123313231011003321022213103113222031333131300
0201311013311222101130233203202201221210013321323200113322333330
0110332203232300120233102211211010301312003221320210023220022223
0022122011202030031102321012312202130333101201321112010201010000
3010130102311113013221021203033011133122320310321223102110202000
1302033021032223303201211311312302232330021132121300321122111100
033111231121200023121031233233303100202301123213133012123012222.
```

Draw Figure XX-X "PRBS9 pattern generator" similar to Figure 94-6 but according to polynomial  $1 + x^5 + x^9$ .

Define Equation (YY-Y) as  $G(x) = 1 + x^5 + x^9$  or make a reference to the polynomial in Table 68-6.

Make a reference to the new clause from 162.9.3.4.

Proposed Response Response Status O

CI 162B SC 162B.1.3.1 P 269 L 36 # 142

Champion, Bruce TE Connectivity

Comment Type TR Comment Status X

FOM\_ILD is set at 0.13 dB and is too stringent for the various form factors and MTF manufacturing variation

SuggestedRemedy

It is recommended to update this value to 0.18 dB

Proposed Response Response Status O

CI 162 SC 162.3 P 143 L 43 # 143

Kochuparambil, Beth Cisco

Comment Type E Comment Status X

The PMD does not reside ON the MDI.

SuggestedRemedy

Change "on" to "for"

Resulting text would read "The PMD converts these streams of symbols into appropriate signals for the MDI."

Proposed Response Response Status O

CI 162 SC 162.8.11 P 151 L 24 # 144

Kochuparambil, Beth Cisco

Comment Type E Comment Status X

Current text: "The terminal count of max\_wait\_timer as specified in 136.8.11.7.3 is 12s." Given a value is specified within the clause/statement makes the phrase "specified in 136[. . .]" incorrect.

SuggestedRemedy

Change "specified" to "defined" or "described"  
This is a semi-pervasive issue.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 162 SC 162.9.3.1.1 P 155 L 47 # 145

Kochuparambil, Beth

Cisco

Comment Type E Comment Status D

"M should be an integer not less than 32"  
May be easier for the reader to avoid the double negative.

*SuggestedRemedy*

Change "not less than"  
to "greater than or equal to"

Proposed Response Response Status O

[Editor's note: Change page from 154 to 155.]

Cl 162 SC 162.9.3.1.3 P 157 L 6 # 146

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

Initial is capitalized mid sentence, however is lower case in Table 162-11's title.

*SuggestedRemedy*

Make "Initial" lower case

Proposed Response Response Status O

Cl 162 SC 162.9.3.5 P 158 L 46 # 147

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

Sentence is poor english

*SuggestedRemedy*

Change "Parameters that do not appear in Table 162-12 take values from Table 162-18."  
to " Take parameter values that do not appear in Table 162-12 from Table 162-18."

Do the same for  
162.9.4.5, pg 164, ln 40 and 162.11.3, pg 167, ln 26  
163.9.2.1.2, 163.9.2.2, 163.9.3.2  
163.10.3  
120F.3.1.1, 120F.3.2.1, 120F.4.3  
162B.1.3.2

Proposed Response Response Status O

Cl 162 SC 162.9.3.6 P 159 L 18 # 148

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

Description may or may not be helpful for those reading the standard. I do, however, note that previous clauses (examples are 92.10.6 and 110.10.6) do NOT describe why we limit CM return loss, but instead just define the limit. Perhaps this description of the re-reflections concept is helpful to readers, it was somewhat confusing until reading it multiple times.

*SuggestedRemedy*

Remove the first paragraph of this section. "Common-mode signals can be returned [ . . . ]  
To reduce this effect, a minimum common-mode to common-mode return loss is specified."

Proposed Response Response Status O

Cl 162 SC 162.11.3 P 167 L 49 # 149

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

The location of the Tfx not is not consistent with other clauses (namely 162.9.4.5 & 162.9.3.5)

*SuggestedRemedy*

Move this note to line 28 (after the description of where to find the parameters)

Proposed Response Response Status O



EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.11.7 P 169 L 44 # 150

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

We've lost a bit of the description of doing COM with 2 package test cases. Someone reading this section in isolation may be confused.

93.9.1 States "The Channel Operating Margin (COM) is computed using the procedure in 93A.1 with the Test 1 and Test 2 values in Table 93-8. Test 1 and Test 2 differ in the value of the device package model transmission line length zp.

*SuggestedRemedy*

Use editorial licence to modify paragraph to say something like, "COM shall be computed twice, Test 1 and Test 2, which differ in the value of the device package model transmission line length zp." Similarly, modify the COM table from "Rx Test 2" and "TX Test 2" to "Test 2, RX" and "Test 2, TX"

Replicate in COM description and tables for 163 & 120F

Proposed Response Response Status O

CI 163 SC 163.9.3.4 P 191 L 48 # 151

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

There are 2 different "Test 1 and Test 2" in the interference tolerance test. In the interference tolerance test description and in step h for COM.

*SuggestedRemedy*

Change the interference tolerance test cases to "Setup 1" and "Setup 2" in both the procedure and the table.

Do similar for 120F.

Proposed Response Response Status O

CI 163 SC 163.10 P 193 L 43 # 152

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

Introduction to channel characteristics mention IL and ERL, but not COM.

*SuggestedRemedy*

Add "and COM 163.10.1" to the end of this paragraph.

Resulting sentence would read: "Channels shall meet the ERL requirements in 162.10.3 and COM requirements in 163.10.1."

Proposed Response Response Status O

CI 120F SC 120F.4 P 225 L 48 # 153

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

There is no overview paragraph in the channel characteristics

*SuggestedRemedy*

Insert a similar paragraph to 163.10 with appropriate modifications. "Channels are recommended to meet... Channels shall meet..."

Proposed Response Response Status O

CI 162 SC 162.1 P 140 L 13 # 154

Kochuparambil, Beth

Cisco

Comment Type E Comment Status X

Annex 162D is the only description that restates the PMD. CR1, CR2, and CR4 seem to already be implied.

*SuggestedRemedy*

Remove "100GBASE-CR1, 200GBASE-CR2, and 400GBASE-CR4" which would leave "Annex 162D describes host and cable assembly types."

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 162 SC 162.1 P 140 L 31 # 155  
 Kochuparambil, Beth Cisco  
 Comment Type E Comment Status X  
 I may just be confused, but seems odd that both RS-FEC and RS-FEC-Int are required, but the Inverse RS-FEC is optional, however required to convert between the other 2 required interfaces.  
 SuggestedRemedy  
 Make Inverse RS-FEC required  
 Proposed Response Response Status O

Cl 162 SC 162.1 P 142 L 41 # 156  
 Kochuparambil, Beth Cisco  
 Comment Type E Comment Status X  
 MAC = MEDIA ACCESS CONTROL is listed twice in the key.  
 SuggestedRemedy  
 Remove 1 of the MAC definitions  
 Proposed Response Response Status O

Cl 30 SC 30.5.1.1.16 P 35 L 48 # 157  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type T Comment Status X  
 "RS-FEC-Int enabled RS-FEC-Int enabled" - gives absolutely NO useful information in the description. Please at least expand a little or give a cross reference to give the reader a clue. (other places where this abbreviation are used, such as 45.2.1.110.ab, generally do give more information)  
 SuggestedRemedy  
 Change the description "RS-FEC-Int enabled" to "Clause 161 Codeword-interleaved Reed-Solomon Forward Error Correction enabled".  
 Proposed Response Response Status O

Cl 45 SC 45.2.1.110 P 43 L 13 # 158  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type E Comment Status X  
 Description text indicating Clause 91 and Clause 161 should be cross references (2 instances of each)  
 SuggestedRemedy  
 Change "Clause 91" and "Clause 161" text in descriptions to active cross references.  
 Proposed Response Response Status O

Cl 1 SC 1.5 P 34 L 18 # 159  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type E Comment Status D  
 "FEC AM lock" While the abbreviation "AM" has been used for "Alignment Marker" in many multi-lane PHYs, it somehow was never entered in the abbreviations list (at least not that I can find, having checked 802.3-2018, where it is used, and 802.3cd). Because it has other common meanings, and this one is specific to IEEE Std 802.3, it should be in the list... (simple things like FEC are). I plan to submit maintenance on this just to make it clear - but since it is an issue in this draft, you can fix it here...  
 SuggestedRemedy  
 Add "AM Alignment Marker" to the list of abbreviations in 1.5 (page 34 of draft)  
 Proposed Response Response Status O  
 [Editor's note: Changed clause, subclause, page, line from {45,0,44,22} to {1,1.5,34,18}.]

Cl 91 SC 91.6.2f P 86 L 5 # 160  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type E Comment Status X  
 "For PHYs supporting RS-FEC-Int operation" should have a reference, especially because it would send the reader searching this clause (RS-FEC) for RS-FEC-Int, and not find it.  
 SuggestedRemedy  
 change "RS-FEC-Int operation" to "RS-FEC-Int operation (see Clause 161)" similar to other references, where Clause 161 is a cross-ref.  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 91 SC 91.7.3 P 87 L 38 # 161  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type T Comment Status X  
 \*FINT indicates RS-FEC-Int and should reference clause 161 as the relevant clause for the capability  
 SuggestedRemedy  
 Add cross-ref to clause 161 under subclause  
 Proposed Response Response Status O

CI 161 SC 161.5.2.6 P 122 L 52 # 162  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type TR Comment Status X  
 "The alignment markers shall be mapped to am\_txmapped<1284:0> in a manner that yields the same result as the following process." Where the process begins and ends isn't really clear in the text since the text just runs in paragraphs of descriptive text intermingled with the text and multiple sets of either pseudocode or alphabetic steps. I THINK it ends at P 123 line 38, but that was only after first thinking it ended at other places a few times. This section is technically quite important and needs to be crystal clear, hence my comment is technical, as it is currently not clear to those outside the group.  
 Descriptive, non-process text should be set out, and the process itself should be either all in steps or all in pseudocode, and set out by its own section. (in my remedy I have used the existing text and put it all in text).  
 Being a little confused by the text, take caution, as I may have gotten it wrong in my proposed remedy.  
 SuggestedRemedy  
 Change "same result as the following process" to "same result as the process in 161.5.2.6.1." Insert new section "161.5.2.6.1 Alignment Marker Mapping Process" following line 54, with content from page 123 lines 1 through 10, and add step e) using text from page 123 lines 18 through 21, and step f) using the text at lines 23 ("The variable am\_txmapped...") through line 33. Add step g) with text at page 123 lines 34 through 38.  
 Move descriptive (and non-process requirement) text at page 123 lines 12-17 and page 123 lines 39 -page 124 line 46 (end of the existing section) ahead of the new section with just the process.  
 Proposed Response Response Status O

CI 161 SC 161.5.2.9 P 125 L 8 # 163  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type E Comment Status X  
 "has been FEC encoded, two FEC codewords... each FEC lane... Once the data has been Reed-Solomon encoded and interleaved... FEC lanes... highest FEC lane." - use consistent nomenclature. You go from FEC, to Reed-Solomon, and as much as I love to remember Gus Solomon by name, it suggests there may be 2 different things youre talking about here.  
 I didn't name it in my remedy, but the editor may wish to review instances of FEC where RS-FEC is meant to be clear - the same thing shows up in 161.5.3.1, 161.5.3.2, and 161.5.3.3. (note RS-FEC is an abbreviation in 802.3-2018 for Reed-Solomon Forward Error Correction)  
 SuggestedRemedy  
 Suggest replace instances on lines 8 through 22 of "FEC" with "RS-FEC", and "Reed-Solomon encoded" on line 21 with "RS-FEC encoded".  
 Additionally suggest editor review usage of "FEC" for possible replacement with RS-FEC elsewhere in clause 161 (I note this doesn't look globally feasible)  
 Proposed Response Response Status O

CI 161 SC 161.5.3.3 P 127 L 31 # 164  
 Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,  
 Comment Type T Comment Status X  
 "The probability that the decoder fails to indicate a codeword with t+1 errors as uncorrected is not expected to exceed 10<sup>-16</sup>." This statement is not technically correct without reference to an underlying raw symbol error rate. The probability of a failed decode can be anything if the raw symbol error rate is left unpinned. Since this subclause stands alone and could be reused with different PHYs in different scenarios, it isn't appropriate to pin the raw SER. Additionally, the descriptive sentence is unnecessary.  
 SuggestedRemedy  
 Delete the last two sentences of the 2nd paragraph of 161.5.3.3 ("The probability...").  
 Proposed Response Response Status O

Cl 1 SC 1.1.3.2 P 31 L 18 # 165

Zimmerman, George CME Consulting/ADI, APL Gp, Cisco, CommScope,

Comment Type E Comment Status X

"For each of chip-to-chip and chip-to-module interfaces" awkward wording, subject/verb agreement - also leaves open whether the definition is different if other than chip-to-chip or chip-to-module interfaces are used here - which does not seem to be the case. Seems it would be cleaner and clearer just to say "for each interface" and the extra words are unnecessary. This same problem exists 6 places on page 31 lines 18, 35, and 50; page 33, lines 5 and 33, and page 34 line 5

*SuggestedRemedy*

Change "For each of chip-to-chip and chip-to-module interfaces" to "For each interface" in all 6 instances (page 31 lines 18, 35, 50; page 33 lines 5 & 33; and page 34 line 5)

Proposed Response Response Status O

Cl 162 SC 162.9.3 P 154 L 21 # 166

Dawe, Piers Nvidia

Comment Type TR Comment Status X

The draft loss budget wastes over 3 dB in nearly every case. The recommended maximum insertion loss allocation for the host traces plus BGA footprint and host connector footprint, of 6.875 dB, compares very poorly with C2M's host insertion loss up to 11.9 dB, making passive copper expensive and unattractive for a switch, while a full range of NICs can be made within only 3.75 dB. Server-switch links will get made with an asymmetric loss budget, so it would be better for the standard to regularise what will happen anyway. By the way, many server-switch links will be asymmetric anyway (different form factors at server and switch ends), and that's already allowed in this draft. This change would also benefit CR switch-switch links because the shortest ports would get credit for their low loss.

*SuggestedRemedy*

As we have done for C2M, create two kinds of CR ports. Host loss allocations of 3.75 dB and 10 dB. Short can connect to short or long with same cable as today; long to long is not supported. Add entries in Clause 73 Auto-Negotiation to advertise short and long to the other end.

In Table 162-10, provide separate limits for Linear fit pulse peak (min).

In Table 162-14, provide separate rows for Test channel insertion loss: for testing the short host input the values for Test 2 are 10-6.875 = 3.125 dB higher (26.75 dB and 27.75 dB), while for the long host input the values for Test 2 are 6.875-3.75 = 3.125 dB lower (20.5 dB and 21.5 dB). No change needed for Test 1.

In 162A.4, provide two equations for each of IL\_PCBmax and for ILHostMax and show them in Fig 162A-1 and 2. In 162A.5, provide two Value columns in Table 162A-1. Adjust figures 162A-3 and 4.

For discussion: should a "long" cable,  $19.75+2*(6.875-3.75) = 19.75+6.25 = 26$  dB max (maybe 3 m) be defined? A CR link could have no more than one of the three host, cable, and host being "long".

We could choose other names than "short" and "long" for the ports, possibly "short" and "medium" (as a C2M host can be "longer"), or A and B, somewhat like USB.

In 162.11.7.1.1, zp, representing the extra loss a host has above an MCB, could be made asymmetric but I believe that would not bring an improvement in accuracy.

There could be a third kind of CR port with 6.875 dB but this would not be useful for server-switch links, would be useful for only a subset of switch-switch links, for which passive copper is a subset anyway, so it doesn't seem worthwhile.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.9.3 P 154 L 21 # 167

Dawe, Piers Nvidia  
 Comment Type E Comment Status X  
 Clumsy "x v" way of defining linear fit pulse peak (min)

SuggestedRemedy

Use "Linear fit pulse peak ratio" as in 163 and 163A.3.2.1. Note the unit in the table changes to V/V.

Proposed Response Response Status O

CI 162 SC 162.9.4.6 P 164 L 46 # 168

Dawe, Piers Nvidia  
 Comment Type E Comment Status X  
 Most such RL equations are graphed out to help the user see what is meant.

SuggestedRemedy

Please illustrate this receiver differential to common-mode return loss too. This would be best done in in Figure 162-4, presently "Transmitter common mode to differential return loss" so that the reader can compare the two.

Proposed Response Response Status O

CI 162 SC 162.9.3.6 P 159 L 30 # 169

Dawe, Piers Nvidia  
 Comment Type TR Comment Status D

1. This paragraph claims that the minimum common-mode to common-mode return loss is specified to reduce reflections of signals that were generated originally as differential and end up as differential. This is not the case: it is included to contain a gross build-up of CM voltage on the line caused by repeated reflections, that is otherwise unbounded. If it had been intended to address mixed-mode issues it would be a tighter spec, but that's not viable for front-panel connectors. Other specs such as Rx Differential to common-mode return loss and Tx Common-mode to differential mode return loss (both 12 dB at Nyquist, total 24) and Differential to common-mode cable assembly conversion loss (10 dB each way) are there to address the mixed-mode issues, and this spec at only 2 dB won't make much difference to them.
2. This is a standard, not an attempt at a textbook. We don't give any justifications for most other specs; there is no reason that this one should be different.

SuggestedRemedy

Delete the paragraph

Proposed Response Response Status O

[Editor's note: Changed page from 157 to 159.]

CI 163 SC 163.10.2 P 195 L 49 # 170

Dawe, Piers Nvidia  
 Comment Type T Comment Status X

51.8 dB at 40 GHz, at least 23.3 dB beyond the loss at Nyquist and further filtered by the transmitter and receiver, is unlikely to affect performance and may exclude some acceptable channels which are good to 30 GHz then less good at 40.

SuggestedRemedy

Replace the straight part of the limit with one that curves down (with an  $f^2$  term), with a reduced  $f_{max}$ .

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.2 P 240 L 9 # 171

Dawe, Piers Nvidia  
 Comment Type TR Comment Status X

For a reasonably clean module (or test equipment in a host stressed eye test), the driver swing has to be aggressively reduced to deliver only 15 mV at near end, short mode. 120E has 70 mV, and the previous draft had 24 mV. Yet a host designer knows whether the host wants the short or long setting, and can usefully optimise for e.g. different crosstalk or noise or BER if given a reasonable signal strength. There is room to increase this weak signal without overloading the receiver.

*SuggestedRemedy*

Increase the eye height, short mode, from 15 mV to 18 mV

Proposed Response Response Status O

CI 162 SC 162.9.4.6 P 164 L 46 # 172

Dawe, Piers Nvidia  
 Comment Type E Comment Status X

In C2M-like specs the Rx Differential to common-mode return loss and Tx Common-mode to differential mode return loss differ by 3 dB at low frequency, for a good reason, but in this clause they are the same. Also, the Differential to common-mode cable assembly conversion loss is more lenient than these specs.

*SuggestedRemedy*

Review the relation between these three limits and adjust if necessary.

Proposed Response Response Status O

CI 162 SC 162.9.4.6 P 165 L 2 # 173

Dawe, Piers Nvidia  
 Comment Type E Comment Status X

Italic >=

*SuggestedRemedy*

Non-italic >= Also 162-10, 162-11, 162-11, possibly others.

Proposed Response Response Status O

CI 120G SC 120G.3.1.2 P 238 L 41 # 174

Dawe, Piers Nvidia  
 Comment Type TR Comment Status X

This fixed time value of time-gated propagation delay Tfx is unworkable because the HCB is defined by its loss not its transit time. While HCBs for connectors with few lanes such as SFP+ may be constructed from PCB, those for connectors with many lanes such as QSFP-DD are challenged by fanout and therefore may use a cabled construction with the same loss and a much greater delay than a PCB. The discontinuity at cable-PCB interface should be windowed out just like the coax connector, but would reasonably be much more than 0.2/2 ns (or ~20 mm?) from the coax connector. The HCB transit time is known well enough, just as its loss is, so we can use that in the windowing. Notice that in 163 and 120F, "The value of Tfx is twice the delay from TP5v to TP5", so it's known there.

*SuggestedRemedy*

Change 0.2 ns to twice 0.8 times the delay between the test fixture test connector and the near side of the test fixture host-facing connector on the HCB. Make a similar change in 162.9.3.5 (HCB for CR). Although there may be less pressure to use a cabled technique for MCBs, for consistency, make similar changes in 120G.3.2.3 and 162.11.3 (MCB).

Proposed Response Response Status O

CI 120G SC 120G.3.2.1 P 240 L 27 # 175

Dawe, Piers Nvidia  
 Comment Type T Comment Status X

The module output doesn't have to "support" two modes (e.g. receive, co-operate, enable, or similar), it has to actually do them. They are abilities of the module.

*SuggestedRemedy*

Change "The module output shall support two modes: short and long." to "There are two module output modes: short and long."

Proposed Response Response Status O

CI 162 SC 162.1 P 141 L 23 # 176

Dawe, Piers Nvidia  
 Comment Type E Comment Status X

Tables 162-2 and 162-3 are essentially the same, and it benefits the reader to see that.

*SuggestedRemedy*

Combine into one table with columns for clause/annex no., description for 200G, description for 400G, and required/optional status. Similarly for tables 163-2 and 3.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.11.6 P 169 L 27 # 177

Dawe, Piers Nvidia

Comment Type TR Comment Status X

Relaxing the already very loose CM RL spec from 2 dB to 1.8 dB at all frequencies isn't justified. This spec becomes useless at the frequency when the MCB loss is 0.9 dB!

SuggestedRemedy

Restore it to 2 dB or use a frequency-dependent mask e.g.  $1.8 + 0.01f$

Proposed Response Response Status

CI 120G SC 120G.5.2 P 252 L 25 # 178

Dawe, Piers Nvidia

Comment Type TR Comment Status X

As a lot of the channel for TP4 far-end is known exactly, one would expect that a known subset of gDC, gDC2 combinations would be the only candidates to try. As for TP1a, I believe the strongest gDC and gDC2 should add to a constant.

SuggestedRemedy

For Continuous time filter, DC gain for TP4 far-end (gDC), change to a set of limits that depend on gDC2 in the same style as for TP1a, with the strongest gDC and gDC2 adding to a constant. The allowed values should be a subset of those for TP1a.

Proposed Response Response Status

CI 120G SC 120G.5.2 P 252 L 12 # 179

Dawe, Piers Nvidia

Comment Type TR Comment Status X

By allowing stronger gDC with stronger gDC2, we can have up to 12 dB of peaking for gDC2 = -1 but up to 16 dB for gDC2 = -3 - yet we don't expect the maximum channel loss to vary like that.

SuggestedRemedy

For TP1a, change the second -12 to -11, and -13 to -10 (so the strongest "CTLE peaking" is 13).

Proposed Response Response Status

CI 120G SC 120G.5.2 P 253 L 23 # 180

Dawe, Piers Nvidia

Comment Type TR Comment Status X

This draft has a primitive rectangular eye mask (H = either EHmin or EA/VECmax), although it is described as a histogram. It's an inefficient/inaccurate way of measuring a signal quality vertically and provides weak and uncertain protection against too much jitter. This is worse with the higher VEC limit in the latest draft that allows worse and more varied signals, and is a particular concern for very short host channels (see Mike Dudek's work) that can have faster edges than higher loss ones.

SuggestedRemedy

Change from a 4-cornered mask with corners at  $t = ts \pm 0.05$ ,  $V = k \pm H/2$  to a 10-cornered mask with corners at  $t = ts \pm 0.05$ ,  $ts \pm 1/16$ ,  $ts \pm 3/32$ ,  $V = k \pm H/2$ ,  $k \pm H \cdot 0.4$ , k. k is VCmid, VCupp or VClow.

In case it's not clear, H is either EHmin or Eye Amplitude \*  $10^{-(VECmax/20)}$ .

This simple scalable method can remain as the EH and VEC limits are revised. Scopes have been measuring with 10-sided masks for many years, it's not more difficult than a rectangular mask.

Proposed Response Response Status

CI 120G SC 120G.3.1.1 P 237 L 36 # 181

Dawe, Piers Nvidia

Comment Type E Comment Status X

In other specs such as CEI-56G-VSR-PAM4 and CEI-56G-VSR-PAM4, the output differential to common-mode return loss is 3 dB better than the input common-mode to differential mode return loss at low frequency, for a good reason, but in this annex they are the same.

SuggestedRemedy

Unless we find a reason not to, offset the specs in the usual way.

Proposed Response Response Status

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162A SC 162A.4 P 260 L 40 # 182

Dawe, Piers Nvidia

Comment Type T Comment Status X

This section, for CR, says "the recommended minimum insertion loss allocation for the transmitter or receiver differential controlled impedance PCBs is 2.3 dB at 26.56 GHz". This is the same as the 2.3 dB MCB PCB IL (but why?), and (ignoring connector via loss) 1/3 of the maximum host trace loss (6.875 dB). 92A.4 and 136A.4 use a ratio of 0.086/0.5 or 1/5.8 which allows more flexibility in host layout than 1/3 does. 120G has Host insertion loss up to 11.9 dB, and I didn't find a minimum host loss, although very low loss could be more of a concern in C2M than CR.

*SuggestedRemedy*

Reduce the recommended minimum insertion loss allocation for the CR transmitter or receiver differential controlled impedance PCBs to whatever is justified. If the reasonable limit is a strong function of host package reflection, state whether the recommendation is for a "nominal worst" package, or what. Add a recommended minimum insertion loss for C2M host traces as appropriate.

Proposed Response Response Status O

CI 120G SC 120G.5.2 P 252 L 16 # 183

Dawe, Piers Nvidia

Comment Type TR Comment Status X

The limits for TP4 gDC, gDC2 should not be the same for short and long output modes.

*SuggestedRemedy*

Create separate limits for TP4 short and long output modes.

Proposed Response Response Status O

CI 162 SC 162.9.3.5 P 159 L 13 # 184

Dudek, Mike Marvell

Comment Type TR Comment Status X

Investigations of the effect of the Time-gated propagation delay on practical HCB's has shown that the input RF connector is affecting the ERL unless the 200 ps is increased to approx 300ps. 300ps is still adequately short to not affect the measurement of the device under test. i.e. The value used for Tfx does not sufficiently mitigate the effects of reflections from the test connector. See dudek\_3ck\_adhoc\_01a\_041421

*SuggestedRemedy*

Change the value from 0.2ns to 0.3ns. Also on page 167 line 44.

Proposed Response Response Status O

CI 120G SC 120G.3.1.2 P 238 L 41 # 185

Dudek, Mike Marvell

Comment Type TR Comment Status X

Investigations of the effect of the Time-gated propagation delay on practical HCB's has shown that the input RF connector is affecting the ERL unless the 200 ps is increased to approx 300ps. 300ps is still adequately short to not affect the measurement of the device under test. i.e. The value used for Tfx does not sufficiently mitigate the effects of reflections from the test connector. See dudek\_3ck\_adhoc\_01a\_041421

*SuggestedRemedy*

Change the value from 0.2ns to 0.3ns also on page 242 line 41

Proposed Response Response Status O

CI 163 SC 163.10 P 193 L 43 # 186

Dudek, Mike Marvell

Comment Type E Comment Status X

Why is the Channel ERL listed here with a duplicate "shall" to 163.10.3 but COM (or the other normative channel requirements aren't listed.

*SuggestedRemedy*

Either delete the two sentences here or change the second sentence to "Channels shall meet the requirements in 163.10.1 and 163.10.3 to 163.10.7."

Proposed Response Response Status O



EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 120G SC 120G.3.2 P 240 L 8 # 187

Dudek, Mike Marvell

Comment Type TR Comment Status X

The 900mV output amplitude allowed for the module is larger than necessary for a short channel and makes it more difficult for the host receiver to avoid being overloaded.

SuggestedRemedy

Provide two rows for Differential peak-to-peak output voltage (max) one for "long mode" and one for "short mode". Leave the "long mode" at 900mV. Make the "short mode" 600mV

Proposed Response Response Status O

CI 120G SC 120G.3.2.2 P 241 L 13 # 188

Dudek, Mike Marvell

Comment Type T Comment Status X

It is unlikely that a host that is asking for a "long mode" will have a fast risetime, and therefore the crosstalk will be less, helping the module achieve better VEC and VEO

SuggestedRemedy

Change to "transition time of 10ps with short mode and 15ps with long mode". Also in table 120G-1 Change the existing row to be for "when requesting short mode" and add another row with value 15ps for "transition time (min 20% to 80%) when requesting long mode." and on page 245 line 53 change to "and transition time of 10ps with short mode and 15ps with long mode as measured at TP1a"

Proposed Response Response Status O

CI 163 SC 163.9.2 P 187 L 45 # 189

Dudek, Mike Marvell

Comment Type TR Comment Status X

The allowed value of dERL of -3dB allows complinat transmitters with substantially worse reflections than the reference transmitter used in COM. I expect to have a presentation showing this.

SuggestedRemedy

Change dERLmin to -1dB also for C2C in Table 120F-1

Proposed Response Response Status O

CI 162C SC 162C.1 P 277 L 54 # 190

Dudek, Mike Marvell

Comment Type T Comment Status X

For interoperability it would be good to specify which signals are assigned in a partially utilized connector.

SuggestedRemedy

Add a sentence. "When a connector is not fully utilized the lower PMD numbers should be used"

Proposed Response Response Status O

CI 116 SC 116.1.4 P 92 L 54 # 191

Dudek, Mike Marvell

Comment Type T Comment Status X

The Optical PMD's are not listed using the new chip to chip and chip to module AUI's

SuggestedRemedy

bring the tables for the 200G and 400G from clause 116 into the document and add the new AUI interfaces to the tables.

Proposed Response Response Status O

CI 162 SC 162.7 P 147 L 34 # 192

Dudek, Mike Marvell

Comment Type E Comment Status X

Improve English

SuggestedRemedy

change "provide" to "provided"

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.7 P 146 L 28 # 193  
 Dudek, Mike Marvell  
 Comment Type E Comment Status X  
 Draft should be consistent format for the PMD control and status registers.  
 SuggestedRemedy  
 Delete the "to" to match table 162-5.  
 Proposed Response Response Status O

CI 162 SC 162.9.4.3.3 P 162 L 18 # 196  
 Dudek, Mike Marvell  
 Comment Type T Comment Status X  
 There are no modifications to COM parameters in Table 162-14.  
 SuggestedRemedy  
 Delete this bullet. (Note that if this is done then step f on page 162 line 20 will become step e).  
 Proposed Response Response Status O

CI 162 SC 162.9.3.1 P 155 L 31 # 194  
 Dudek, Mike Marvell  
 Comment Type T Comment Status X  
 There are now five preset conditions  
 SuggestedRemedy  
 Change "three" to "five"  
 Proposed Response Response Status O

CI 162 SC 162.9.4.3.3 P 162 L 36 # 197  
 Dudek, Mike Marvell  
 Comment Type TR Comment Status X  
 SNDR should be measured as appropriate for this clause not as for C2C at 25G.  
 SuggestedRemedy  
 Change "SNDR is measured at the Tx test reference using the procedure in 120D.3.1.6, with the exception that the linear fit in 120D.3.1.3 is performed with a pulse length (Np) of 15 UI." to "SNDR is measured at the Tx test reference using the procedure in 162.9.3.3"  
 Proposed Response Response Status O

CI 162 SC 162.9.4.3.2 P 162 L 4 # 195  
 Dudek, Mike Marvell  
 Comment Type T Comment Status X  
 An extra exception is needed for the test channel loss.  
 SuggestedRemedy  
 Change to "The test channel is the same as the one defined in 110.8.4.2.2, except that the cable assembly meets the requirements of 162.11, the test channel loss meets the requirements of table 162-14 and the cable assembly test fixture meets the requirements of 162B.1.2."  
 Proposed Response Response Status O

CI 162 SC 162.9.4.3.3 P 162 L 42 # 198  
 Dudek, Mike Marvell  
 Comment Type E Comment Status X  
 93A.1.2.1 and 93A.1.2.4 have been brought into this amendment.  
 SuggestedRemedy  
 Make these references standard hot links.  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.9.4.6 P 165 L 9 # 199

Dudek, Mike Marvell

Comment Type E Comment Status X

It would be helpful to have a graph showing this equation.

SuggestedRemedy

Either add a separate graph or reference figure 162-4 and change the figure title to Transmitter common mode to differential return loss and Receiver differential to common mode return loss.

Proposed Response Response Status O

CI 162 SC 162.11.3 P 167 L 25 # 200

Dudek, Mike Marvell

Comment Type E Comment Status X

93A.5 should be a hot link

SuggestedRemedy

fix it.

Proposed Response Response Status O

CI 162 SC 162.11.5 P 168 L 41 # 201

Dudek, Mike Marvell

Comment Type TR Comment Status X

The differential to common mode conversion loss specification is very relaxed particularly at higher frequencies. As an example at 25GHz this specification is only approx 6dB more than the insertion loss. There is no specification for the common mode to common mode return loss of the Rx so all this common mode energy can be reflected back to the cable where through common mode to differential conversion it then becomes a differential signal interferer. Assuming this common mode to differential mode has approximately the same value as the differential to common mode conversion of approx 12.5dB this unwanted interferer is only 18.5dB below the wanted signal and will severely degrade the BER.

SuggestedRemedy

Add 10dB to this equation

Proposed Response Response Status O

CI 162 SC 162.11.7 P 169 L 39 # 202

Dudek, Mike Marvell

Comment Type E Comment Status X

93A.1 is in this amendment. It should be a hot link

SuggestedRemedy

fix it.

Proposed Response Response Status O

CI 162 SC 162.11.7.1 P 171 L 42 # 203

Dudek, Mike Marvell

Comment Type T Comment Status X

There is ambiguity as to whether the transmitter and receiver PCB signal paths include the capacitors or not. Here the description implies that they don't but on page 172 (e.g. equation 162-14) they do.

SuggestedRemedy

Change "The transmitter and receiver PCB signal paths are calculated using the method defined in 93A.1.2.3. The scattering parameters for a PCB transmission line are defined by Equation (93A-13), Equation (93A-14) and the parameter values given in Table 162-19." to "The scattering parameters for a PCB transmission line are calculated using the method defined in 93A.1.2.3 using Equation (93A-13), Equation (93A-14) and the parameter values given in Table 162-19."

Proposed Response Response Status O

CI 162 SC 162.11.7.2 P 174 L 1 # 204

Dudek, Mike Marvell

Comment Type E Comment Status X

It is confusing to state the aggressors are in column two through four because there are separate columns for next and next.

SuggestedRemedy

Change to "the crosstalk paths are from the aggressors listed horizontally to the victims listed vertically.

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

Cl 163 SC 163.10.1 P 195 L 21 # 205

Healey, Adam Broadcom Inc.

Comment Type TR Comment Status X

The bmax limit is very generous (0.2) for taps up to Nb. Channels considered by the Task Force do not justify such a high limit. The limit should be tightened to reduce the chance that unexpected channels will meet the minimum COM threshold but contain large reflections that are difficult to handle.

*SuggestedRemedy*

Change the bmax limit for n = 7 to Nb to be 0.1. Make a similar change to Table 162-16.

Proposed Response Response Status O

Cl 120G SC 120G.3.2 P 240 L 8 # 206

Healey, Adam Broadcom Inc.

Comment Type TR Comment Status X

The maximum differential peak-to-peak output voltage for the "short" module output mode should be reduced. A lower output amplitude for "short" mode would reduce the input dynamic range that the host receiver needs to support. This was part of the original proposal for multiple module output modes. However, the feature has not yet been included in the standard.

*SuggestedRemedy*

Change the maximum differential peak-to-peak output voltage to 600 mV for the "short" module output mode.

Proposed Response Response Status O

Cl 162 SC 162.9.4.3.4 P 163 L 23 # 207

Healey, Adam Broadcom Inc.

Comment Type TR Comment Status X

The spectrum of the broadband noise that is added at the pattern generator output is undefined. Since noise injected at the pattern generator output is filtered by the channel, "broadband" noise will be low-pass filtered at the input to the receiver under test. This is a different stress from the "broadband" noise (with bounded spectral density) injected at the receiver for the Clause 163 interference tolerance test. It could also be argued that the low-pass filtered noise is less "realistic" and test results may not represent receiver performance under normal operating conditions.

*SuggestedRemedy*

Bound the spectrum of the broadband noise in a manner similar to what is done in 93C.1. The spectrum should be bounded to be more high-pass in nature so that band-pass noise is presented to the receiver (similar to Clause 163 stress).

Proposed Response Response Status O

Cl 120G SC 120G.3.3.3.1 P 246 L 13 # 208

Healey, Adam Broadcom Inc.

Comment Type TR Comment Status X

The stressed input signal calibration procedure states that "random jitter and the pattern generator output levels are adjusted (without exceeding the differential peak-to-peak input voltage tolerance specification as shown in Table 120G-7) to result in the eye height for all three eyes given in Table 120G-8 with the setting of the CTLE that minimizes the vertical eye closure." The term "output levels" is ambiguous. It could be interpreted to be "pattern generator output amplitude" or "individual PAM-4 signal levels". This needs to be clarified.

*SuggestedRemedy*

Change:

"Random jitter and the pattern generator output levels are adjusted (without exceeding the differential peak-to-peak input voltage tolerance specification as shown in Table 120G-7) to result in the eye height for all three eyes given in Table 120G-8 with the setting of the CTLE that minimizes the vertical eye closure."

To:

"Random jitter and the pattern generator differential peak-to-peak output voltage are adjusted so that the height of the smallest eye matches the value in Table 120G-8. The differential peak-to-peak input voltage tolerance given in Table 120G-7 is not exceeded."

Make a similar change to 120G.3.4.1.1 (page 249, line 10).

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.9.4.3.3 P 163 L 6 # 209

Healey, Adam Broadcom Inc.

Comment Type TR Comment Status X

For values of J3u/Jrms where the condition stated in NOTE 1 is satisfied, The Q3 value should be derived from  $10^{(-3)}$  and not  $10^{(-3)}/2$ . The A\_DD and sigma\_RJ derived for the given value of Q3 will correspond to a dual-Dirac distribution with a smaller value of J3u than what is measured from the pattern generator. The calibrated interference amplitude (based on COM) will in turn be somewhat higher resulting in a level of overstress. This issue has been pointed out in [https://www.ieee802.org/3/ck/public/adhoc/apr14\\_21/hidaka\\_3ck\\_adhoc\\_01\\_041421.pdf](https://www.ieee802.org/3/ck/public/adhoc/apr14_21/hidaka_3ck_adhoc_01_041421.pdf).

SuggestedRemedy

Change the value of Q3 to 3.0902. Change NOTE 1 to begin "Q3 is an approximated solution of  $Q(Q3) = 10^{(-3)}$ , where...". Make a similar change to 163.9.3.4 (page 192, line 14). In 120F.3.2.3 (page 224, line 2), note that Q4 (an approximated solution of  $Q(Q4) = 10^{(-4)}$ ) is 3.719 as an exception to the use of Equation (120D-10) and Equation (120D-11).

Proposed Response Response Status O

CI 162B SC 162B.1.3.6 P 273 L 30 # 210

Kocsis, Sam Amphenol

Comment Type TR Comment Status X

NEXT\_loss(f) range specified is 50MHz-40.000MHz. I believe this is just a typo given the discussion on this topic. This could be deemed editorial, but there is technical impact to the change.

SuggestedRemedy

Change to 40.000 GHz

Proposed Response Response Status O

CI 162B SC 162B.1.3.6 P 273 L 42 # 211

Kocsis, Sam Amphenol

Comment Type TR Comment Status X

Table 162B-2 rise and fall time specified as 7.5ps (1 instance). The group determined during D1p4 comment resolution that 8.5ps was a more practical value for the rise and fall time for FOM\_ILD calculations. Its logical that the same rise time should be applied to ICN calculations.

SuggestedRemedy

Change to 8.5ps to match the FOM\_ILD definitions in 162B.1.3.1

Proposed Response Response Status O

CI 162B SC 162B.1.3.6 P 274 L 2 # 212

Kocsis, Sam Amphenol

Comment Type TR Comment Status X

NEXT\_loss(f) range specified is 50MHz-40.000MHz. I believe this is just a typo given the discussion on this topic. This could be deemed editorial, but there is technical impact to the change.

SuggestedRemedy

Change to 40.000 GHz

Proposed Response Response Status O

CI 162B SC 162B.1.3.6 P 274 L 18 # 213

Kocsis, Sam Amphenol

Comment Type TR Comment Status X

Table 162B-4 rise and fall time specified as 7.5ps (2 instances). The group determined during D1p4 comment resolution that 8.5ps was a more practical value for the rise and fall time for FOM\_ILD calculations. Its logical that the same rise time should be applied to ICN calculations.

SuggestedRemedy

Change to 8.5ps to match the FOM\_ILD definitions in 162B.1.3.1

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 45 SC 45.2.1.126a P 53 L # 214

He, Xiang Huawei

Comment Type T Comment Status X

32-bit counter may be too short for some of the codeword error bins. A brief calculation below shows the saturation time for the lower bins for 400 Gb/s rate, if the overall BER is  $2E-4$  (random).

Bin#	Minutes to saturate
1	2.5
2	4.6
3	12.7
4	46.9
5	217
...	

If considering burst errors, bin 2 and 3 will saturate even faster.  
Bins saturated too early may not be able to provide useful information.

*SuggestedRemedy*

Increase the size of counters for bin 1~3, if not for all, to 48 bits.

Proposed Response Response Status O

CI 120F SC 120F.3.1 P 219 L 22 # 215

He, Xiang Huawei

Comment Type E Comment Status X

A dot is added to the abbreviated word "abs" in this table but not in the others.

*SuggestedRemedy*

Change "abs." to "abs" or add the dot for all other occurrences.

Proposed Response Response Status O

CI 162D SC 162D.1 P 289 L 14 # 216

DiMinico, Christopher MC Communications

Comment Type ER Comment Status D

There are six MDI connector "receptacles" distinguished uniquely by name, referring to them by "type" is unnecessary.

*SuggestedRemedy*

P289; Line 14 delete "types of" in the sentence "There are six types of MDI connectors "receptacles" specified for hosts."  
P289; Line 32 change sentence to "This enables multiple cable assembly types with different combinations of the plug connectors at each end."  
P290; Line 4 in Table 162D-2 delete "type" two places "Receptacle/Plug type"  
P290; Line 32 in Table 162D-3 delete "type" two places "Receptacle/Plug type"  
P291; Line 20 in Table 162D-4 delete "type" two places "Receptacle/Plug type"

Proposed Response Response Status W

CI 162B SC 162B.1.3.1 P 269 L 1 # 217

Haser, Alex Molex

Comment Type T Comment Status X

IL\_MTFref(26.56 GHz) does not match the 6.60 dB specified in 162B.1 (page 266 line 20).

*SuggestedRemedy*

Update Equation 162B-5; change coefficient out front from 0.9505 to 0.942 to get correct 6.60 dB value at 26.56 GHz

Proposed Response Response Status O

CI 162B SC 162B.1.3.1 P 269 L 36 # 218

Haser, Alex Molex

Comment Type T Comment Status X

FOM\_ILD limit is too strict for measured data

*SuggestedRemedy*

Relax FOM\_ILD to 0.18 dB (see slide 11 of kocsis\_3ck\_adhoc\_01\_011321.pdf)

Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 162 SC 162.14.4.3 P 178 L 43 # 219  
 Wu, Mau-Lin MediaTek Inc.  
 Comment Type ER Comment Status X  
 The 'Feature' of 'TC5' is not correct.  
 SuggestedRemedy  
 Change "Differential mode to common-mode output return loss" to "Common-mode to differential output return loss" for the 'Feature' of 'TC5'.  
 Proposed Response Response Status O

CI 163 SC 163.1 P 181 L 9 # 220  
 Wu, Mau-Lin MediaTek Inc.  
 Comment Type E Comment Status X  
 There are no descriptions for Annex 163B in the paragraph.  
 SuggestedRemedy  
 Add the following sentence at the end of the 1st paragraph of 163.1 Overview.  
 "Annex 163B provides informative information of an example test fixture meeting the requirements for TP0v"  
 Proposed Response Response Status O

CI 120G SC 120G.1 P 235 L 36 # 221  
 Wu, Mau-Lin MediaTek Inc.  
 Comment Type E Comment Status X  
 The sentence below refers to CEI-112G-VSR-PAM4 defined in OIF-CEI-05.0 [B55a].  
 "The C2M interface is defined using a specification and test methodology that is similar to that used for CEI-112G-VSR-PAM4 defined in OIF-CEI-05.0 [B55a]."  
 However, OIF-CEI-05.0 doesn't exist yet.  
 SuggestedRemedy  
 Propose to remove this sentence  
 Proposed Response Response Status O

CI 120G SC 120G.3.1.5 P 239 L 10 # 222  
 Wu, Mau-Lin MediaTek Inc.  
 Comment Type TR Comment Status X  
 Vertical eye opening is not used as a specification in 120G, vertical eye closure is used instead. Therefore, the following sentence is not appropriate.  
 "Eye height and Vertical eye opening are measured according to the method described in 102G.5.2."  
 SuggestedRemedy  
 Change "vertical eye opening" to "vertical eye closure".  
 Proposed Response Response Status O

CI 120G SC 120G.3.2.1 P 240 L 37 # 223  
 Wu, Mau-Lin MediaTek Inc.  
 Comment Type TR Comment Status X  
 In Table 120G-4, Module output mode mapping, there are 100GAUI-1-S C2M, 100GAUI-1-L C2M, and etc. defined for "Host electrical interface". However, no definitions of those "Host electrical interface" were found in the whole specification. Based on that, the information provided by this Table may be confusing for the readers.  
 SuggestedRemedy  
 We shall either add the definitions of 100GAUI-1-S & 100GAUI-1-L C2M or remove Table 120G-4.  
 Proposed Response Response Status O

CI 120G SC 120G.3.4.1.1 P 249 L 8 # 224  
 Wu, Mau-Lin MediaTek Inc.  
 Comment Type TR Comment Status X  
 The frequency-dependent attenuation added from output of the pattern generator to TP1a is 18.2 dB, which is 16 dB channel loss with 2.2 dB for host transmitter package loss. However, 2.2 dB is too small a value for host transmitter package loss with 31 mm package trace length.  
 SuggestedRemedy  
 By leveraging what adopted in OIF CEI-112G-VSR-PAM4, propose to adopt the 19.5 dB value to replace 18.2 dB, where 3.5 dB representing host transmitter package loss is reasonable.  
 Proposed Response Response Status O

EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI 163B SC 163B.2 P 297 L 25 # 225

Wu, Mau-Lin MediaTek Inc.

Comment Type ER Comment Status X

Equation (163-1) is the wrong reference. It shall be "Equation (163B-1)".

SuggestedRemedy

Change "Equation (163-1)" to "Equation (163B-1)" in the following sentence.  
 "The insertion loss of the example test fixture is approximated by Equation (163-1) which is illustrated in Figure 163B-1."

Proposed Response Response Status O

CI FM SC 0 P 3 L 2 # 226

Wu, Mau-Lin MediaTek Inc.

Comment Type ER Comment Status D

Annex 163A through Annex 163B are lost here.

SuggestedRemedy

Change the sentence to  
 "This amendment to IEEE Std 802.3-2018 adds Clause 161 through Clause 163, Annex 120F, Annex 120G, Annex 162A through Annex 162D, and Annex 163A through Annex 163B."

Proposed Response Response Status O

[Editor's note: Changed clause from 00 to FM.]

CI FM SC 0 P 14 L 29 # 227

Wu, Mau-Lin MediaTek Inc.

Comment Type ER Comment Status D

Annex 163A through Annex 163B are lost here.

SuggestedRemedy

Change the sentence to  
 "This amendment to IEEE Std 802.3-2018 adds Clause 161 through Clause 163, Annex 120F, Annex 120G, Annex 162A through Annex 162D, and Annex 163A through Annex 163B."

Proposed Response Response Status O

[Editor's note: Changed clause from 00 to FM.]

CI 162 SC 162.9.4.3.3 P 162 L 36 # 228

Wu, Mau-Lin MediaTek Inc.

Comment Type TR Comment Status X

For the calculation of SNDR measured at the Tx test reference, the linear fit in 120D.3.1.3 is performed with a pulse length (N<sub>p</sub>) of 15 UI. The pulse length (N<sub>p</sub>) shall be long enough to cover all 'linear response', such as reflection due to package length. In this case, the calculated SNDR includes nonlinearity only, instead of the far-away 'linear' reflection. The 15 UI spec here is the same as 50GBASE-CR, which is not reasonable for 100GBASE-CR1. We shall need a larger value of N<sub>p</sub> here.  
 In 'li\_3ck\_01\_1020', the authors proposed to consider TX + RX EQ capability to decide N<sub>p</sub> value. In that contribution, N<sub>p</sub> = 29 was proposed for Clause 163. I found no clues why we have different N<sub>p</sub> value for Clause 162, since their TX + RX EQ capability are similar.

SuggestedRemedy

By considering the pulse length to at least cover reflection due to package trace length, whose maximum value is 31 mm. By considering the dielectrics constant, D<sub>k</sub>, as in the range of 3.5 ~ 4.0, the location of reflection due to 31 mm trace length is around 22 ~ 24 taps after main cursor. Therefore, adopt N<sub>p</sub> = 29 as Clause 163 seems reasonable.  
 Proposed to N<sub>p</sub> value from 15 to 29.

Proposed Response Response Status O

CI FM SC FM P 1 L 10 # 229

Grow, Robert RMG Consulting

Comment Type E Comment Status X

From the amendment list starting at line 28, it appears the TF is planning to be included in the current revision project.

SuggestedRemedy

Add assigned amendment number 16.

Proposed Response Response Status O

CI FM SC FM P 4 L 8 # 230

Grow, Robert RMG Consulting

Comment Type E Comment Status X

IEEE style has changed (2020 IEEE Standards Style Manual, 11.1).

SuggestedRemedy

Delete 2nd paragraph of the Editor's Note.

Proposed Response Response Status O



EE P802.3ck D2.0 100/200/400 Gb/s Electrical Interfaces Task Force Initial Working Group ballot comment

CI **FM** SC **FM** P **8** L **21** # **231**  
 Grow, Robert RMG Consulting  
 Comment Type **E** Comment Status **X**  
 The ballot group is now known.  
 SuggestedRemedy  
 Add WG members list at start of P802.3ck WG ballot.  
 Proposed Response Response Status **O**

CI **FM** SC **FM** P **11** L **4** # **232**  
 Grow, Robert RMG Consulting  
 Comment Type **E** Comment Status **X**  
 Amendment title missing.  
 SuggestedRemedy  
 Replace "Amendment title (copy from PAR)" with the title.  
 Proposed Response Response Status **O**

CI **120G** SC **120G.3.3.3** P **244** L **46** # **233**  
 Dawe, Piers Nvidia  
 Comment Type **E** Comment Status **X**  
 It would be better to put the crosstalk parameters in the stressed input parameters tables rather than scattered through the text.  
 SuggestedRemedy  
 Move the peak-to-peak voltage and transition time numbers from the text of 120G.3.3.3.1 and 120G.3.4.1.1 to Table 120G-8 and 120G-11  
 Proposed Response Response Status **O**

CI **120G** SC **120G.1** P **235** L **38** # **234**  
 Dawe, Piers Nvidia  
 Comment Type **TR** Comment Status **X**  
 Up to now, the optical PMD channels have not needed a very strong DFE, and the C2M loss (10 dB for C2M CAUI-4, 10.2 for 200GAUI-4 C2M, 16 for 400GAUI-4) is low enough that CR and KR PMDs don't need a very strong DFE when used as C2M. Therefore, we never have precoding on C2M at 50G/lane - simple. At 100G/lane, links such as active copper cables will benefit from a very strong DFE in the receiver in the cable end that's receiving from a higher loss in the cable. 802.3 enables such active cables via the C2M specs; up until now there was nothing more to say, so they don't get a mention in 802.3. Adding precoding after the signal has been serialised is best avoided, so it should be added in the host, so for the first time, there is something that 802.3 should do specifically about active cables.  
 SuggestedRemedy  
 Allow optional precoding abilities in 100G/lane C2M transmitters and receivers in the host. Add MDIO registers to advertise these abilities and to enable them.  
 Proposed Response Response Status **O**

CI **162** SC **162.11.7** P **171** L **31** # **235**  
 Dawe, Piers Nvidia  
 Comment Type **TR** Comment Status **X**  
 The spec allows a channel to have its COM calculated with 9 taps in the range 13 to 24 clipped at +/-0.05 - which means that the channel's pulse response could be a little worse than +/-0.05 for all these 9 taps. That's a very bad cable! and not likely to get made. We don't need to provide all the receiver power and complexity to cope with it.  
 SuggestedRemedy  
 Use another DFE root-sum-of-squares limit for positions 13-24. Similarly in 163, but as 163 specifies the complete channel while 162 uses clean synthetic host traces, the limit might differ.  
 Proposed Response Response Status **O**

Cl 162 SC 162.9.3.4 P 158 L 34 # 236

Li, Mike Intel

Comment Type TR Comment Status X

PRBS9Q pattern definition is incomplete, and PRBS9Q symbol transition definition for EOJ measurement is missing.

*SuggestedRemedy*

1.) change "PRBS9Q is defined in a similar way to PRBS13Q (see 120.5.11.2.1) except that the polynomial in Table 68-6 is used instead of the polynomial in Equation 94-3." to "PRBS9Q is defined in 162.9.3.4.1, a similar way to PRBS13Q (see 120.5.11.2.1), except that the polynomial in Table 68-6 is used instead of the polynomial in Equation 94-3."; 2.) Add a new sentence of "The symbol transition definition for jitter measurement and even-odd jitter calculation with PRBS9Q is provided in 162.9.3.4.1; 3.) Create a new section 162.9.3.4.1 entitled "EOJ measurement with PRBS9Q", with contents from slides 5, 6 of li\_3ck\_01\_0521

Proposed Response Response Status O

Cl 162C SC 162C.2.4 P 283 L 41 # 237

Zhang, Bo Inphi

Comment Type T Comment Status X

QSFP+ is meant for 4x10G 40G pluggable connector transceivers. I believe this section is meant for QSFP families such as QSFP28, QSFP56, QSFP-DD etc.

*SuggestedRemedy*

Suggest replace QSFP+ with QSFP families. Also please provide similar references to the 'QSFP+' such as those in section 1.3 normative references footnotes.

Proposed Response Response Status O

Cl 162 SC 162.1 P 140 L 7 # 238

Zhang, Bo Inphi

Comment Type E Comment Status X

When -CRx interfaces are first introduced in the overview section of clause 162. It's not clear the definition is properly referenced.

*SuggestedRemedy*

Suggest provide linkage of the definition of -CRx with -CRx interfaces when they are first introduced.

Proposed Response Response Status O