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CI **FM** SC **FM** P1 L 31 # 26
 Ran, Adee Cisco systems
 Comment Type **E** Comment Status **A** bucket1
 802.3cv is published.
SuggestedRemedy
 Change "IEEE Std 802.3cv-20xx" to "IEEE Std 802.3cv-2021", here and on page 16.
 Response Response Status **C**
 ACCEPT.

CI **00** SC **0** P0 L 0 # 5
 Brown, Matt Huawei
 Comment Type **E** Comment Status **A** bucket1
 802.3ck will not be incorporated into the next amendment (802.3dc) so it will be amendment to that revision.
SuggestedRemedy
 Convert draft to be an amendment of new revision (802.3dc) rather than an amendment of 802.3-2018.
 Response Response Status **C**
 ACCEPT.

CI **00** SC **0** P0 L 0 # 20
 Brown, Matt Huawei
 Comment Type **E** Comment Status **A** bucket1
 According to the style manual subclause 16.4, table notes should be placed as follows: "A table note should be set immediately following the table to which it belongs, enclosed within the boxed table, above the bottom border of the table."
 Several table notes were added to several tables in recent drafts but not placed according to this guidance.
SuggestedRemedy
 Fix the table note at the following page/line: 169/24, 179/21, 251/46, 255/25, 283/28
 Response Response Status **C**
 ACCEPT.
 [Editor's note: CC: 120G, 162, 162B]

CI **80** SC **80.1.5** P80 L 45 # 2
 Brown, Matt Huawei
 Comment Type **T** Comment Status **A** PHY table (bucket1)
 In Table 80-4a, 100GAUI-1 C2C and C2M have been added to several PHY types, but the physical layer tables in the corresponding PMD clauses have not been updated.
SuggestedRemedy
 Amend the 100 Gb/s physical layer tables in clauses 138 and 140 to include 100GAUI-1 C2C and C2M sublayers.
 Response Response Status **C**
 ACCEPT.

CI **116** SC **116.1.4** P98 L 18 # 3
 Brown, Matt Huawei
 Comment Type **T** Comment Status **A** PHY table (bucket1)
 In Table 116-3, 200GAUI-2 C2C and C2M have been added to several 200 Gb/s PHY types, but the physical layer tables in the corresponding PMD clauses have not been updated.
SuggestedRemedy
 Amend the 200 Gb/s physical layer tables in clauses 121 and 122 to include 200GAUI-2 C2C and C2M sublayers.
 Response Response Status **C**
 ACCEPT.

CI **116** SC **116.1.4** P99 L 18 # 4
 Brown, Matt Huawei
 Comment Type **T** Comment Status **A** PHY table (bucket1)
 In Table 116-4, 400GAUI-4 C2C and C2M have been added to several 400 Gb/s PHY types, but the physical layer tables in the corresponding PMD clauses have not been updated.
SuggestedRemedy
 Amend the 400 Gb/s physical layer tables in clauses 122, 123, 124, 138, 150, and 151 to include 400GAUI-4 C2C and C2M sublayers.
 Response Response Status **C**
 ACCEPT.

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Cl 120 SC 120.5.1 P 107 L 54 # 16

Sun, Junqing Credo Semiconductor
 Comment Type TR Comment Status D withdrawn

SSPRQ usually causes confusion in the field to be used as receive pattern. A note in the spec will help to clarify.

SuggestedRemedy

Add "and SSPRQ" after "square wave" in the second paragraph of 120.5.1. This paragraph will be "Test patterns that are intended for transmitter testing, such as square wave for SSPRQ, may not be correctly recovered by an adjacent PMA."

Proposed Response Response Status Z

REJECT.
 This comment was WITHDRAWN by the commenter.
 [Editor's note: changed page/line from 108/46]

Cl 120 SC 120.5.11.2.a P 110 L 48 # 80

Dudek, Mike Marvell
 Comment Type E Comment Status A bucket1

120.5.7 should be a hot link

SuggestedRemedy

fix it

Response Response Status C

ACCEPT.

Cl 120G SC 120G.3.1 P 250 L 12 # 46

Ran, Adeo Cisco systems
 Comment Type TR Comment Status A AC CM noise

"AC common-mode RMS output voltage (max)" specification of 17.5 mV is not feasible for high-volume, multi-port products. The common-mode output may include a component correlated to the differential output, e.g. from mode conversion on the host channel. A module receiver is expected to be quite tolerant to a correlated common-mode signal.

As suggested in ran_3ck_adhoc_20210630, there are two reasonable alternatives:

- a) increase the allowed RMS voltage to 30 mV (as is allowed for the CR transmitter measured on an HCB - likely the same point - and where the common-mode concern is greater due to conversion in the cable assembly).
- b) Keep the 17.5 mV specification but only for the component uncorrelated to the differential signal; use the linear fitted pulse response method (which is already referred to in 120G.5.2) to calculate the linear fitted pulse response characteristics of the common-mode output, and define the AC common-mode noise as the RSS of sigma_n and sigma_v.

Note: This comment is only about the host output; module output is more controlled and modules can be designed to have low mode conversion so the correlated component is expected to be small. Modules should not be allowed to generate 30 mV RMS, so if option a is chosen, the module output specification should not be changed.

SuggestedRemedy

Preferably implement option a in the comment.

Response Response Status U

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

Comment 121 proposes to increase the value to 25 mV.

This comment proposes to either:

- (a) change the value to 30 mV
 - (b) change the parameter to relate to only the uncorrelated noise
- There is not sufficient evidence that the correlated noise is indeed tolerable by the receiver (e.g., conversion from CM to DM in receiver might be non-linear or CM might have much larger channel transit time than DM)

The resolution to comment #123 indicates there is not consensus to make the change proposed in option (b), above.

Following straw polls #3 and #4, there was consensus to close this comment changing the value to 25 mV.

Change the AC common-mode RMS output voltage (max) for module output and host

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output to 25 mV.

Straw poll #3, pick one (direction)
 Straw poll #4, Chicago rules (direction)
 To address comments #46 and #121, for the module output and host output AC CM noise (max) I would support:
 A: no change
 B: change to 25 mV
 C: change to 30 mV
 Straw poll #3
 A: 12 B: 13 C: 9
 Straw poll #4
 A: 15 B: 25 C: 21

Cl 120G SC 120G.3.1 P 250 L 12 # 121

Dawe, Piers Nvidia
 Comment Type TR Comment Status A AC CM noise
 As discussed, AC common-mode output voltage (max) 17.5 mV isn't reasonable at double the signalling rate of 120E with the same connectors and layout skew.

SuggestedRemedy
 Increase to 25 mV, both host and module output.

Response Response Status C
 ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

Resolve using the response to comment #46.

Cl 120G SC 120G.3.1 P 250 L 18 # 61

Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type TR Comment Status D HO EH/VEC

Data from Ghiasi page 7
https://www.ieee802.org/3/ck/public/adhoc/apr21_21/ghiasi_3ck_adhoc_01a_042121.pdf
 and Calvin page 4
https://www.ieee802.org/3/ck/public/adhoc/jun30_21/calvin_3ck_adhoc_01_063021.pdf
 indicate meeting current VEO/VEC at TP1a not feasible to meet

SuggestedRemedy
 Considering that on a system all 32 ports plus lanes must meet the TP1a, the best in practice channels should have margin to pass not fail. This is an area that we need more measurement but given what we know at this point VEC should be increased to 13 dB and VEO reduced to 8.5 mV

Proposed Response Response Status Z
 REJECT.

This comment was WITHDRAWN by the commenter.

Cl 120G SC 120G.3.1 P 250 L 25 # 58

Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type TR Comment Status A HO TT

Transition time host requesting short mode or long mode is for TP4

SuggestedRemedy
 Please revert to 10 ps in draft D2.0, please move this parameter to TP4 table 120G-3

Response Response Status C
 ACCEPT IN PRINCIPLE.

This comment relates to the host output transition time specified in Table 120G-1.

Separate values for host long and short modes were added per D2.1 comment #188.

The justification was that the host input and host output PCB insertion loss will likely be similar, which is reflected in the transition times chosen for the host input crosstalk calibration. This must also be explicitly allowed and constrained at the host output.

However, it would be helpful in Table 120G-1 to point to the subclause that defines long and short modes.

Add a footnote to the sub-rows for long and short modes in Table 120G-1 pointing to 120G.3.2.1.

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Cl **120G** SC **120G.3.1.5** P **252** L **15** # **8**

Brown, Matt Huawei

Comment Type **E** Comment Status **A** transition time (bucket1)

Reference to transition time methodology.

SuggestedRemedy

Change "transition time" to "transition time (see 120G.3.1.4)".

Repeat at:

page 254, line 13

page 258, lines 43/44

page 262, lines 10/11

Response Response Status **C**

ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Cl **120G** SC **120G.3.1.5** P **252** L **16** # **120**

Dawe, Piers Nvidia

Comment Type **TR** Comment Status **A** test system response

"without the use of a reference receiver" which occurs several times, is misleading; the BT4 filter, which is the reference receiver response in so many clauses, applies.

SuggestedRemedy

Change to "observed through the Bessel-Thomson response of 120G.3.1 in place of the reference receiver of 120G.5.2" or similar. Several places.

Response Response Status **C**

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

There could be some misinterpretation since the reference receiver as defined in 120G.5.2 includes the effect of the test equipment filter. Also, since the response is prescriptive, it should not be in parentheses.

On page 252, line 16...

Change: "calibrated at TP4 (without the use of a reference receiver)"

To: "calibrated at TP4 using a test system with a response as defined in 120G.3.1 rather than the reference receiver of 120G.5.2"

Apply similarly at page/line: 254/12, 258/43, and 262/10.

Implement with editorial license.

Cl **120G** SC **120G.3.2** P **253** L **1** # **48**

Ran, Adeo Cisco systems

Comment Type **E** Comment Status **A** bucket1

"Table 120G-3—Module output characteristics (at TP4)" - Parentheses are inconsistent with other similar tables (Host output in this annex, and Transmitter characteristics elsewhere).

SuggestedRemedy

Change title to "Module output characteristics at TP4"

Response Response Status **C**

ACCEPT.

Cl **120G** SC **120G.3.2** P **253** L **11** # **98**

Dawe, Piers Nvidia

Comment Type **TR** Comment Status **R** MO VEC/EH

If the eye height limit is the same at long near end as at long far end, there is huge margin at near end and the implementer is encouraged to optimise for far end or beyond, only limited by the NE VEC spec, while we want modules to be set up consistently, for the full range from near to far. EH is naturally larger at NE for a well set up output.

SuggestedRemedy

Increase the eye height, long mode near end, by 3 dB from 15 mV to 21 mV

Response Response Status **U**

REJECT.

This comment pertains to the module output eye height (min) for long mode, near end.

The comment does not provide sufficient evidence that the proposed change is necessary.

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Cl **120G** SC **120G.3.2** P **253** L **11** # **97**

Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **R** MO VEC/EH

The driver swing has to be aggressively reduced from 600 mV pk-pk to deliver only 15 mV at near end, short mode. 120E has 70 mV, and D1.4 had 24 mV, ghiasi_3ck_adhoc_01a_042121 shows 35 mV (before Vpkpk was reduced). Yet a host can usefully optimise for e.g. different crosstalk or noise if given a reasonable signal strength. A NIC has no high-loss ports so it can do this even if a switch won't. There is room to increase this weak signal without overloading the receiver. Also, making the limits more like reality encourages more consistent module setup across the industry.

SuggestedRemedy

Increase the eye height, short mode near end, by 1.1 dB from 15 mV to 17 mV

Response Response Status **U**

REJECT.

This comment pertains to the module output eye height (min) for short mode, near end.

The comment does not provide sufficient evidence that the proposed change is necessary.

Cl **120G** SC **120G.3.2** P **253** L **12** # **62**

Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **A** MO VEC/EH

TP4 VEC can be lowered from current 12 dB to 11 dB to allow additional penalty for real host channel and host ASIC

SuggestedRemedy

Reduce TP4 VEC=11 dB, see ghiasi_3ck_01_0721

Response Response Status **C**

ACCEPT IN PRINCIPLE.

This comment pertains to the module output VEC (max).

Slides 7 and 8 of the following presentation was reviewed by the task force:
https://www.ieee802.org/3/ck/public/21_07/ghiasi_3ck_01_0721.pdf

The slide shows that with the current g_dc constraints VEC fails for the long mode, near-end measurement. The comment suggests that g_dc max for TP4 far-end be increased from -3 dB to -2 dB. With this change to the g_DC limit there is no need to change VEC (max).

Cl **120G** SC **120G.3.2** P **253** L **13** # **59**

Ghiasi, Ali Ghiasi Quantum/Inphi
 Comment Type **TR** Comment Status **D** MO VEC/EH

TP4 long VEO at max loss drops to 12 mV

SuggestedRemedy

Reduce TP4 high loss VEO=12 mV, see ghiasi_3ck_01_0721

Proposed Response Response Status **Z**

REJECT.

This comment was WITHDRAWN by the commenter.

Cl **120G** SC **120G.3.2** P **253** L **20** # **49**

Ran, Adeo Cisco systems
 Comment Type **TR** Comment Status **A** MO DC CM voltage tolerance

footnote b says "Specification includes effects of ground offset voltage." - what does it mean?

It is unclear why the module needs a specification of DC common-mode voltage at all, given that its output is AC coupled (per 120G.1). Without AC coupling in the module, the limits given in this table are not reasonable.

SuggestedRemedy

Clarify what the quoted sentence mean, or delete it.

Consider removing the DC common mode voltage specification.

Response Response Status **C**

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

The comment is referring to module output "DC common-mode voltage" specifications which are intended to define a tolerance for the module output to host DC bias voltage. A DC common-mode voltage tolerance specification is required as the module output, whether it be a discrete capacitor or decoupling on the die, must tolerate the DC common-mode voltage applied by the host input. This is a necessary requirement and thus should not be deleted. However, this specification as written is difficult to interpret.

Implement slide 16 of brown_3ck_02b_0721 with editorial license.

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Cl **120G** SC **120G.3.2** P **253** L **22** # **50**

Ran, Adee Cisco systems
 Comment Type **ER** Comment Status **A** MO DC CM voltage tolerance

"DC common-mode voltage (max)" - assuming this specification is not removed, it should refer to footnote b, not footnote a.

SuggestedRemedy

change footnote reference from a to b.

Response Response Status **C**

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

Resolve using the response to comment #49.

Cl **120G** SC **120G.3.2.2.1** P **254** L **51** # **102**

Dawe, Piers Nvidia
 Comment Type **TR** Comment Status **R** MO SI host reference channel

The near end and far end should be placed far enough apart so that the module implementer has little choice what emphasis to use, so that all modules are set up similarly. As short is easier than long, this means that far minus near (mm or dB) for short should be at least as much as far minus near for long. As real host channels are not exactly like the theoretical reference host channel, there should be a healthy overlap of short and long to give the host room for its implementation. D2.0's 160 mm delivered on both these criteria, D2.1's 133 mm doesn't.

SuggestedRemedy

Change 133 to 150, change 80 to 90

Response Response Status **U**

REJECT.

The comment does not provide sufficient justification for the proposed changes.

There may be some benefit to balancing the length range between short and long modes. Further analysis is encouraged.

Cl **120G** SC **120G.3.3** P **255** L **34** # **51**

Ran, Adee Cisco systems
 Comment Type **TR** Comment Status **A** MO AC CM noise tolerance

The host should tolerate the AC common mode output allowed for the module output. Even if this is not included in the stressed input test, this expectation should be part of the host input specification.

SuggestedRemedy

Add a row to Table 120G-7 with parameter "AC common-mode input voltage tolerance (RMS)" and value based on Table 120G-3.

Response Response Status **C**

ACCEPT IN PRINCIPLE.

Comment #55 proposes a similar change to the host input.

Implement slide 19 of brown_3ck_02b_0721 with editorial license.

Strawpoll #8 (decision)

I support addressing comment #51 and #55 using slide 19 of brown_3ck_02b_0721.

Yes: 15

No: 12

Cl **120G** SC **120G.3.3.1** P **256** L **4** # **52**

Ran, Adee Cisco systems
 Comment Type **E** Comment Status **A** bucket1

It is preferable to refer to the value in table 120G-7 than to repeat it.

SuggestedRemedy

Change "for any signaling rate in the range 53.125 GBd ± 100 ppm" to "for any signaling rate in the range specified in Table 120G-7".

Response Response Status **C**

ACCEPT.

Cl **120G** SC **120G.3.3.4.1** P **257** L **31** # **89**

Wu, Mau-Lin MediaTek Inc.
 Comment Type **E** Comment Status **A** bucket1

"host reference channel" here means "reference host channel" in other places. It would be better to align with other places.

SuggestedRemedy

Change "host reference channel" to "reference host channel"

Response Response Status **C**

ACCEPT.

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CI 120G SC 120G.3.3.4.2 P 258 L 33 # 53

Ran, Adee Cisco systems

Comment Type T Comment Status A HI SI method

Unlike the jitter levels in step c, the initial signal levels in the calibration procedure are not defined. Using inappropriately low levels can result in bad jitter measurement in step c.

To achieve good jitter measurement, the initial output levels should be as high as possible without exceeding the differential peak to peak specification.

Also applies in module stressed input test, 120G.3.4.2.2.

SuggestedRemedy

Add guidance to step a to use initial signal level as high as possible such that the differential peak-to-peak input voltage tolerance given in Table 120G-9 is not exceeded.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Straw poll #9 (decision)

To address comment #53, I support implementing the suggested remedy.

Yes: 18

No:5

CI 120G SC 120G.3.3.4.2 P 258 L 39 # 72

Dudek, Mike Marvell

Comment Type E Comment Status A HI SI method

The final values of jitter used in the test are unlikely to match these values of Jrms and J4u because crosstalk is added in step e and random jitter is adjusted in step g. It would be helpful to the reader to indicate this.

SuggestedRemedy

Add to the end of bullet c. "Note that these are initial jitter values. They will be modified by the addition of crosstalk in step e and adjustment of random jitter in step g" Add this to the end of bullet c on page 262 as well.

Response Response Status C

ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

CI 120G SC 120G.3.3.4.2 P 259 L 16 # 66

Ghiasi, Ali Ghiasi Quantum/Inphi

Comment Type TR Comment Status D HI SI EH/VEC

Host stress input VEC is too high and does not account for real host channel and ASIC package and VEO can be as small as 12 mV

SuggestedRemedy

Reduce VEC=11-11.5 dB range and VEO to 12 mV, see ghiasi_3ck_01_0721

Proposed Response Response Status Z

REJECT.

This comment was WITHDRAWN by the commenter.

CI 120G SC 120G.3.3.4.2 P 259 L 20 # 90

Wu, Mau-Lin MediaTek Inc.

Comment Type TR Comment Status A bucket1

The 'Value' for 'Crosstalk differential peak-to-peak voltage' is 870, which is without unit. Unit of voltage shall be included here as other items.

SuggestedRemedy

Change '870' to '870 mV'

Response Response Status W

ACCEPT.

CI 120G SC 120G.3.4 P 260 L 9 # 55

Ran, Adee Cisco systems

Comment Type TR Comment Status A MI AC CM noise tolerance

The module should tolerate the AC common mode output allowed for the host output. Even if this is not included in the stressed input test, this expectation should be part of the module input specification.

SuggestedRemedy

Add a row to Table 120G-9 with parameter "AC common-mode input voltage tolerance (RMS)" and value based on Table 120G-1.

Response Response Status C

ACCEPT IN PRINCIPLE.

Comment #51 proposes a similar change to the host input.

Resolve using the response to comment #51.

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CI 120G SC 120G.3.4.1 P 260 L 30 # 56

Ran, Adee

Cisco systems

Comment Type E Comment Status A bucket1

It is preferable to refer to the value in table 120G-9 than to repeat it.

SuggestedRemedy

Change "for any signaling rate in the range 53.125 GBd ± 100 ppm" to "for any signaling rate in the range specified in Table 120G-9".

Response Response Status C

ACCEPT.

CI 120G SC 120G.3.4.2.2 P 262 L 18 # 68

Ghiasi, Ali

Ghiasi Quantum/Inphi

Comment Type TR Comment Status D MI EH/VEC

Data from Ghiasi page 7
https://www.ieee802.org/3/ck/public/adhoc/apr21_21/ghiasi_3ck_adhoc_01a_042121.pdf
 and Calvin page 4
https://www.ieee802.org/3/ck/public/adhoc/jun30_21/calvin_3ck_adhoc_01_063021.pdf
 indicate meeting current VEO/VEC at TP1a not feasible to meet

SuggestedRemedy

This is an area that we need more measurement but given what we know at this point VEC should be increased to 13 to 13.5 dB and VEO reduced to 8.5 mV to support Lim Channels, see ghiasi_3ck_01_0721

Proposed Response Response Status Z

REJECT.

This comment was WITHDRAWN by the commenter.

CI 120G SC 120G.5.2 P 265 L 12 # 105

Dawe, Piers

Nvidia

Comment Type TR Comment Status R RR gdc

When gDC2 is -2, we allow no more than $-(-12-2) = 14$ dB of peaking, yet when gDC2 is -3, we allow $-(-13-3) = 16$ dB, yet the channel loss should not be higher. This doesn't make sense.

SuggestedRemedy

For TP1a, change -12 -12 -13 to -12 -11 -10 or -12 -12 -11 (so the strongest CTLE peaking for the highest two gDC2 categories is the same).

Response Response Status U

REJECT.

The comment does not provide sufficient justification for the proposed changes.

CI 120G SC 120G.5.2 P 265 L 16 # 103

Dawe, Piers

Nvidia

Comment Type TR Comment Status R RR gdc

The limits for TP4 gDC, gDC2 should not be the same for short and long output modes.

SuggestedRemedy

Create separate limits for TP4 short and long output modes, so 4 sets for TP4+, in the style of TP1a.

Response Response Status U

REJECT.

This comment is a restatement of D2.0 comment #179, which was rejected on the basis of insufficient justification and detail. It adds request to provide 4 sets of values in the style used for TP1a but does not provide specific values. No further justification is provided.

The comment does not provide sufficient justification for the proposed changes nor does the suggested remedy provide sufficient detail to implement.

CI 120G SC 120G.5.2 P 265 L 25 # 104

Dawe, Piers

Nvidia

Comment Type TR Comment Status R RR gdc

As a lot of the channel for TP4 far-end is known exactly and the max loss to TP4 far end is less than to TP1a, the range of gDC, gDC2 combinations should be a subset of the TP1a ones. As for TP1a, I believe the strongest gDC and gDC2 should add to a constant.

SuggestedRemedy

For Continuous time filter, DC gain for TP4 far-end (gDC), change to a set of limits that depend on gDC2 in the same style as for TP1a, with the strongest gDC and gDC2 adding to a constant. The allowed values should be a subset of those for TP1a.

Response Response Status U

REJECT.

This comment is a restatement of D2.0 comment #178, which was rejected on the basis of insufficient justification and detail. No further justification or implementation detail is provided.

The comment does not provide sufficient justification for the proposed changes nor does the suggested remedy provide sufficient detail to implement.

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CI 120G SC 120G.5.2 P 265 L 51 # 10
 Brown, Matt Huawei
 Comment Type E Comment Status A bucket1
 Method should start at step "a)" not "h)"
 SuggestedRemedy
 Reformat list to start at "a)".
 Response Response Status C
 ACCEPT.

CI 120G SC 120G.5.2 P 265 L 51 # 38
 Ran, Adeo Cisco systems
 Comment Type ER Comment Status A bucket1
 The list in this subclause starts at h) instead of a).
 SuggestedRemedy
 Change the list format to start at a).
 Response Response Status W
 ACCEPT.

CI 120G SC 120G.5.2 P 266 L 23 # 106
 Dawe, Piers Nvidia
 Comment Type TR Comment Status A EO method
 This draft has a primitive rectangular eye mask spec with mask height = max(EHmin, EA/VECmax) and mask width = 0.1 UI, although it is described as a histogram. Measuring a diamond eye with a rectangular mask is an inefficient, inaccurate way of measuring signal quality and provides weak and uncertain protection against too much jitter. Its effective width is less than its actual because of the 1e-5 probability criterion and the inefficient shape.
 De-weighting the sides of the histogram/mask would make this worse, equivalent to increasing the target BER by 10x or so. A higher VEC / smaller EH limit with the rectangular mask would allow more jittered and more varied signals, particularly for very short host channels (see Mike Dudek's work) that can have faster edges than higher loss ones. The target BER is not going to change.
 We need an eye mask that's more eye shaped, so that a higher proportion of the samples are near the boundary and contribute to the measurement.

SuggestedRemedy
 Change from a 4-cornered mask with corners at $t = ts \pm 0.05$, $V = y \pm H/2$ to a 10-cornered mask with corners at $t = ts \pm 0.05$, $ts \pm 1/16$, $ts \pm 3/32$, $V = y \pm H/2$, $k \pm H \cdot 0.4$, y is near VCmid, VCupp or VClow (vertically floating, as in D2.1).
 H is $\max(EHmin, \text{Eye Amplitude} \cdot 10^{-(VECmax/20)})$. Eye Amplitude is AVupp, AVmid or AVlow, as in D2.1.
 This simple scalable method can remain as the EH and VEC limits are revised. Scopes have been measuring with 10-sided masks for many years, it's not more difficult than a rectangular mask and gives better results.

Response Response Status U
 ACCEPT IN PRINCIPLE.

This comment is a restatement of D2.0 comment #127, which was rejected on the basis of insufficient justification and insufficient analysis to show equivalent or better interoperability.

Straw polls 5, 6, and 7 indicate there is no consensus to make the proposed change. However, the resolution to comment #39 addresses the concern expressed in this comment.

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CI 120G SC 120G.5.2 P 266 L 25 # 39

Ran, Adeo Cisco systems
 Comment Type TR Comment Status A EO method

As has been reported in calvin_3ck_adhoc_01_063021, the authors have been "unable to reliably close the calibration loop on TP1a at 12.5dB VEC with precision lab equipment" for insertion loss of 16.4 dB. This suggests that the VEC specification may be unfeasible.

Allowing a higher (worse) VEC for transmitters (host/module outputs) might pass bad receivers with very closed eyes, which will put more burden on receivers (even if the signal in stressed input test does not change, receivers will have to work with transmitters that have the same VEC due to other reasons, e.g. a "rectangular eye" closed by high noise that can't be equalized, rather than ISI).

Instead of lowering the VEC bar for transmitters, we should look at the definition of VEC and make it more suitable to the expected eye shape of good transmitters after processing with the reference receiver (this shape is not rectangular), taking into account the expected behavior of real receivers.

The calculation of VEC and EH from a CDF accumulated over $t_s \pm 0.05$ UI gives the same weight to all phases. This makes sense if the receiver's phase is distributed uniformly in this window; it supposedly makes sense if we don't know where the receiver will sample within this region and account for sampling error. But the eye is not independent of the receiver - it is shaped by the receiver's equalization, and in the reference receiver we assume a certain behavior.

A receiver is expected to optimize its equalization (CTLE+DFE or equivalent) at the sampling point t_s - this is part of the measurement procedure (currently steps k and l) - which would result in the maximum vertical opening being at t_s . We should assume the average sampling phase is then t_s ; any difference between the optimized phase and the average phase is an implementation penalty that should be covered by the minimum EH.

A real receiver's CDR does not have a uniform phase distribution around its mean; the probability of sampling at either -0.05 UI or $+0.05$ UI from t_s is smaller than the probability of sampling closer to t_s . The rare events where the sample is taken far from t_s contribute less to the average BER, so they should be weighted down in the calculation of the CDFs. Having equal weights as in the current method is overly pessimistic in both EH and VEC.

It is therefore proposed to apply a weighting function to the sampled data based on the phase.

Suggested Remedy

A detailed proposal will be provided in a presentation.

Response Response Status C

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot.

Hence it is not within the scope of the recirculation ballot.

The following presentation analyzed the effect of the currently specified measurement method. A similar analysis is required to make any changes.
https://www.ieee802.org/3/ck/public/20_10/healey_3ck_01a_1020.pdf

The following presentation was reviewed by the task force:
https://www.ieee802.org/3/ck/public/21_07/ran_3ck_01a_0721.pdf

Per straw polls 5, 6, and 7 there was consensus to implement the proposal in ran_01a (slide 9) with σ_r set to 0.02 UI.

Implement the method in ran_01a (slide 9) with σ_r set to 0.02 UI.

Straw poll #5 (chicago rules) direction

Straw poll #6 (pick one) direction

For the eye opening method in 120G.5.2 I would support:

A: a weighted method similar to comment #39 and ran_01a

B: a multi-sided eye mask similar to comment #106

C: no change

D: need more information

#5: A: 25 B: 15 C: 13 D: 11

#6: A: 15 B: 8 C: 11 D: 5

Straw poll #7 (decision)

I support resolving comment #39 using the proposal in ran_01a (slide 9) except with standard deviation (σ_r) of 0.02 UI.

Yes: 21

No: 11

CI 161 SC 161.5.2.8 P 134 L 3 # 18

Brown, Matt Huawei

Comment Type E Comment Status A bucket1

To address the editor's note a simple change to 161.5.2.9 can address the main concern of D2.1 Comment #163. The terms "FEC encode" and "Reed-Solomon" encoded should be reconciled. All other references in Clause 161 to encoding are preceded by "Reed-Solomon" not "FEC". The same holds for decoder except for one instance.

Reed-Solomon encoder 3x
 Reed-Solomon encoding 1x
 Reed-Solomon encoded 2x
 Reed-Solomon encode 2x
 FEC encoded 1x
 Reed-Solomon decode 1x
 Reed-Solomon decoding 1x
 Reed-Solomon decoder 9x
 decoder 1x

SuggestedRemedy

In 161.5.2.9, change "FEC encoded" to "Reed-Solomon" encoded.
 In 161.5.3.3 (page 136, line 31), change "decoder" to "Reed-Solomon decoder"

Response Response Status C

ACCEPT IN PRINCIPLE.

Resolve the first part of the suggested remedy using the response to comment #27.
 In 161.5.3.3 (page 136, line 31), change "decoder" to "Reed-Solomon decoder"

CI 161 SC 161.5.2.9 P 134 L 3 # 27

Ran, Adeo Cisco systems

Comment Type T Comment Status A bucket1

The text can be made more precise to avoid possible confusion of "FEC encoded" vs. "Reed-Solomon encoded" and to clarify where the codewords come from and what is being distributed.

SuggestedRemedy

Change "Once the data has been FEC encoded, two FEC codewords" to "Once the data has been encoded per 161.5.2.8, two resulting codewords"

On line 16, change "Once the data has been Reed-Solomon encoded and interleaved, it shall be distributed" to "tx_out<1087:0> shall be distributed".

Response Response Status C

ACCEPT IN PRINCIPLE.

Change "Once the data has been FEC encoded, two FEC codewords" to "Once the data has been Reed-Solomon encoded, two resulting FEC codewords"

On line 16, change "Once the data has been Reed-Solomon encoded and interleaved, it shall be distributed" to "tx_out<1087:0> shall be distributed".

CI 162 SC 162.1 P 149 L 15 # 82

Wu, Mau-Lin MediaTek Inc.

Comment Type E Comment Status A bucket1

The hyperlink of "Figure 162-1" is not correct. It is linked to Table 162-1.

SuggestedRemedy

Correct the hyperlink of "Figure 162-1".

Response Response Status C

ACCEPT.

CI 162 SC 162.9.3 P 162 L 12 # 83

Wu, Mau-Lin MediaTek Inc.

Comment Type E Comment Status A bucket1

There is no "hyperlink" to 162A.2.

SuggestedRemedy

The hyperlink of 162A.2 shall be added in the sentence "The transmitter characteristics at TPO are provided informatively in 162A.2."

Response Response Status C

ACCEPT.

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Cl 162 SC 162.9.3 P 163 L 5 # 28

Ran, Adee Cisco systems
 Comment Type TR Comment Status A bucket1

In Table 162-10 the first parameter is "Signaling rate, each (nominal)" - but the value is 53.125 ± 50 ppm so this label is incorrect (nominal is 53.125).

This label is inconsistent: in Table 163-5 it is just "Signaling rate", in Table 120F-1 and Table 120G-1 it is "Signaling rate, each lane (range)".

The "(range)" seems correct. The words "each lane" are unnecessary - all parameters in these tables are per-lane.

Make the label consistent across the similar tables.

SuggestedRemedy

Change the label to "Signaling rate (range)" in all 4 tables.

Response Response Status W

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

Change the label to "Signaling rate, each lane (range)" for all 4 tables.
 [Editor's note: CC: 120F, 120G, 162, 162]

Cl 162 SC 162.9.3 P 163 L 10 # 123

Mellitz, Richard Samtec
 Comment Type TR Comment Status R AC CM noise

Table 162-10 specifies AC common-mode RMS voltage, vcmi (max) note b just changes to a PRBS13Q with method described in 93.8.1.3. The problem is that coherent CM signal are included in differential measurements like SNDR, Jitter, and Linear fit pulse peak ratio. That means it is the coherent part if AC CM is double counted.

SuggestedRemedy

Add note to line 10 (vcmi) indicating that the CM mode measurement is only for the non-coherent CM part of the measurement.

This applies to Tables 163-5, 120F-1, 120G-1, and 120G-3

Response Response Status U

REJECT.

[Editor's note: Changed clause/subclause from 163/163.9.3.]

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

The following presentation was reviewed by the task force:
https://www.ieee802.org/3/ck/public/21_07/mellitz_3ck_01a_0721.pdf.
 Resolve in conjunction with comment #46.

Based on straw poll #2, there is not sufficient consensus to implement the proposed changes.

Straw poll #1 (direction)
 I would support the AC CM voltage test methodology in Comment #123 and the related presentation mellitz_3ck_01_0721.
 Yes: 18
 No: 6
 Need more information: 13
 Abstain: 3

Straw poll #2 (decision)
 For the resolution of comment #123, I support adopting the AC CM voltage test methodology in Comment #123 and the related presentation mellitz_3ck_01a_0721.
 Yes: 15
 No: 16

[Editor's note: CC: 163, 120F, 120G]

302.3ck D2.1 100/200/400 Gb/s Electrical Interfaces Task Force 1st Working Group recirculation ballot co

CI 162 SC 162.9.3 P 163 L 15 # 99

Dawe, Piers Nvidia
 Comment Type E Comment Status A bucket1

Now that we have established a consistent way of naming these return losses, let's make it easier for the reader to find them.

SuggestedRemedy

Please add "RLcc", "RLdc" and so on in the table rows as we do for ERL, VEC, vf and others, throughout the draft. Also in running text such as 162.9.3.6. Similarly Rpeak.

Response Response Status C

ACCEPT.

CI 162 SC 162.9.3.4 P 168 L 1 # 31

Ran, Adeo Cisco systems
 Comment Type ER Comment Status A bucket1

120D.3.1.2 is not the correct reference for the pattern symbols and thresholds.

SuggestedRemedy

Change 120D.3.1.2 to Table 120D-4.

Response Response Status W

ACCEPT.

CI 162 SC 162.9.3.4 P 168 L 22 # 24

Hidaka, Yasuo Credo Semiconductor, Inc.
 Comment Type E Comment Status A bucket1

164 on the row F10 and the column of index of last symbol is a typo.

SuggestedRemedy

Change 164 with 264.

Response Response Status C

ACCEPT.

CI 162 SC 162.9.4 P 170 L 39 # 32

Ran, Adeo Cisco systems
 Comment Type ER Comment Status A signaling rate (bucket1)

The receiver specifications tables the signaling rate parameter has inconsistent name across tables. In Table 162-14 it is "Signaling rate", in Table 163-8 "Receiver signaling rate", in Table 120F-4, Table 120G-7, and Table 120G-9 "Signaling rate, each lane (range)".

The word "(range)" seems correct. The words "each lane" are unnecessary - all parameters in these tables are per-lane. Similarly "Receiver" is unnecessary.

Make the label consistent across the similar tables.

SuggestedRemedy

Change the label to "Signaling rate (range)" in all 4 tables.

Response Response Status W

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

Change in all tables to be consistent with Table 120G-9:
 "Signaling rate, each lane (range)"
 [Editor's note: CC: 120F, 120G, 162, 163]

CI 162 SC 162.9.4.1 P 171 L 4 # 33

Ran, Adeo Cisco systems
 Comment Type T Comment Status A UI value (bucket1)

"This translates to a nominal unit interval of 18.82353 ps" - even with 5 digits after the decimal, this is not the nominal unit interval but an approximation.

In fact, 4 digits (0.1 fs resolution) result in about 1 ppm error, which is sufficient for any practical purpose.

SuggestedRemedy

Change "18.82353" to "approximately 18.8235".

Response Response Status C

ACCEPT.

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Cl 162 SC 162.9.4.2 P 171 L 12 # 84

Wu, Mau-Lin MediaTek Inc.

Comment Type TR Comment Status A bucket1

The peak-to-peak differential output voltage is defined in Table 162-10 footnote b, instead of "footnote a".

SuggestedRemedy

Change "Table 162-10 footnote a" to "Table 162-10 footnote b".

Response Response Status W

ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

However, the proposed change is an improvement to the draft.

Implement the suggested remedy.

Cl 162 SC 162.9.4.3.3 P 172 L 25 # 6

Brown, Matt Huawei

Comment Type E Comment Status A transition time (bucket1)

Transition time is referred to here as "20% to 80% transition time". It is defined explicitly in 120E.3.1.5. Transition time is usually referred to elsewhere in draft as just "transition time". Align terminology.

SuggestedRemedy

Change "20% to 80% transition time" to "transition time"

Response Response Status C

ACCEPT.

Cl 162 SC 162.9.4.3.3 P 173 L 25 # 112

Dawe, Piers Nvidia

Comment Type TR Comment Status A bucket1

fhp is not defined.

SuggestedRemedy

Define fhp

Response Response Status W

ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Cl 162 SC 162.9.4.3.4 P 174 L 8 # 114

Dawe, Piers Nvidia

Comment Type TR Comment Status A bucket1

These equations for spectral density mask are too obscure.

SuggestedRemedy

Add a graph

Response Response Status W

ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Cl 162 SC 162.9.4.4.2 P 175 L 18 # 85

Wu, Mau-Lin MediaTek Inc.

Comment Type E Comment Status A bucket1

The reference here is missed in D2.1. It's (see 162.9.4.3.4 in D2.0). No comments were accepted to change this in D2.0.

SuggestedRemedy

Change "(see)" to "(see 162.9.4.3.4)"

Response Response Status C

ACCEPT IN PRINCIPLE.

Reference to 162.9.4.3.4 is not helpful since that subclause does not address added sinusoidal jitter. Given that the previous subclause 162.9.4.4.1 describes the test setup including sinusoidal jitter this reference can be deleted.

Delete "(see)".

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Cl 162 SC 162.11.7 P 183 L 39 # 95

Dawe, Piers Nvidia
 Comment Type TR Comment Status R COM bbgmax

The normalized DFE coefficient minimum limit bbgmax for taps 3 to 12 is -0.03. It doesn't make sense that taps 13 to 40 could be worse, -0.05. If I have understood the data correctly, the example channels we have don't need this. (Remember, these are reference receiver limits not hard cable or channel limits anyway; a cable or channel can go beyond a tap limit if it makes up the COM another way, e.g. with acceptable crosstalk.)

SuggestedRemedy

Change bbgmax 0.05 to bbgmax 0.05, bbgmax -0.03. Also in 163.

Response Response Status U

REJECT.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.1 and D2.0 or the unsatisfied negative comments from the initial ballot. Hence it is not within the scope of the recirculation ballot.

The following presentation showed that some backplane channels had floating tap coefficient values of <-0.03.
https://www.ieee802.org/3/ck/public/19_09/heck_3ck_01_0919.pdf
 The comment does not provide an assessment of the impact to those channels.
 [Editor's note: CC: 162, 163]

Cl 162 SC 162.11.7.1 P 184 L 7 # 81

Dudek, Mike Marvell
 Comment Type E Comment Status A bucket1

93A.1.2.3, Equation 93A-13, 93A-14 and Table 162-19 should be hot links or green text.

SuggestedRemedy

fix them

Response Response Status C

ACCEPT.

Cl 162 SC 162.11.7.1 P 184 L 8 # 86

Wu, Mau-Lin MediaTek Inc.
 Comment Type E Comment Status A bucket1

There is no "hyperlink" to Table 162-19.

SuggestedRemedy

Add hyperlink to Table 162-19

Response Response Status C

ACCEPT.

TYPE: TR/technical required ER/editorial required GR/general required T/technical E/editorial G/general
 COMMENT STATUS: D/dispatched A/accepted R/rejected RESPONSE STATUS: O/open W/written C/closed U/unsatisfied Z/withdrawn
 SORT ORDER: Clause, Subclause, page, line

Cl 162A SC 162A.5 P 277 L 30 # 11

Brown, Matt Huawei
 Comment Type E Comment Status A terminology (bucket1)

The acronym "IL" is often used to represent "insertion loss" in text, but is never formally introduced.

SuggestedRemedy

Either introduce it properly, e.g., "insertion loss (IL)" or expand it everywhere.

Response Response Status C

ACCEPT IN PRINCIPLE.

Introduce the acronym properly, e.g., "insertion loss (IL) with editorial license.

Cl 162B SC 162B.1.2.1 P 280 L 41 # 12

Brown, Matt Huawei
 Comment Type E Comment Status A bucket1

lcatf and f should be italic.

SuggestedRemedy

Format as italic.

Response Response Status C

ACCEPT.

Cl 163 SC 163.9.2 P 200 L 5 # 19

Brown, Matt Huawei
 Comment Type T Comment Status A table note (bucket1)

Table 163-5 is a normative table, but footnote c relating to transmitter waveform is a recommendation.

SuggestedRemedy

Convert footnote c to a table note (see style manual 16.4) or delete footnote c.

Response Response Status C

ACCEPT IN PRINCIPLE.

This can also be fixed by placing the recommendation in regular text.
 The comment equally applies to footnote c in Table 162-10.
 Remove footnote c from Table 163-5 and Table 162-10 and add a new sentence to the end of the first paragraph in 162.9.3.1.4 as follows:
 "It is recommended that the same step size is used for all coefficients."

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Cl 163 SC 163.9.3.1 P 202 L 37 # 34
 Ran, Adeo Cisco systems
 Comment Type E Comment Status A signaling rate (bucket1)
 It is preferable to refer to the value in table 163-8 than to repeat it. (The NOTE can stay as it is).
 SuggestedRemedy
 Change "for any signaling rate in the range 53.125 GBd ± 100 ppm" to "for any signaling rate in the range specified in Table 163-8".
 Response Response Status C
 ACCEPT.

Cl 163 SC 163.9.3.5 P 204 L 51 # 35
 Ran, Adeo Cisco systems
 Comment Type E Comment Status A RIT TX off
 "with the transmitter equalizer turned off" - preferably be consistent with most other places in this draft which use the wording "set to preset 1 (no equalization)".
 Also is 162.9.4.3.3 with a variation on the wording - preferably change that one too.
 SuggestedRemedy
 Use the term "preset 1 (no equalization)" in all places.
 Response Response Status C
 ACCEPT IN PRINCIPLE.
 [Editor's note: CC: 163, 162]
 In 162.9.4.3.3, 162.9.4.3.5, and 163.9.3.5, and elsewhere if appropriate, change the text to the following:
 "with transmitter equalization off by setting coefficients to preset 1 values (see 162.9.3.1.3)"
 Implement with editorial license.

Cl 163 SC 163.9.3.5 P 205 L 30 # 44
 Ran, Adeo Cisco systems
 Comment Type E Comment Status A bucket1
 "Q3d" is formatted with inconsistent roman/italic font.
 SuggestedRemedy
 For consistency with clause 162, use italics for all occurrences of Q3d.
 Response Response Status C
 ACCEPT.

Cl 163 SC 163.9.3.5 P 205 L 31 # 45
 Ran, Adeo Cisco systems
 Comment Type TR Comment Status A bucket1
 In NOTE 1, "Q(Q3)" should be "Q(Q3d)".
 SuggestedRemedy
 Change per comment.
 Response Response Status W
 ACCEPT.

Cl 163 SC 163.9.3.5 P 205 L 31 # 25
 Hidaka, Yasuo Credo Semiconductor, Inc.
 Comment Type E Comment Status A bucket1
 Symbol Q3 remains in NOTE 1.
 SuggestedRemedy
 Change Q(Q3) with Q(Q3d).
 Response Response Status C
 ACCEPT.

Cl 163 SC 163.10 P 206 L 38 # 87
 Wu, Mau-Lin MediaTek Inc.
 Comment Type TR Comment Status A bucket1
 Maximum AC-coupling 3 dB corner frequency shall be 50 kHz, instead of 50 Hz, based on 163.10.7
 SuggestedRemedy
 Change the "Unit" in Table 163-10 from "Hz" to "kHz"
 Response Response Status W
 ACCEPT.

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Cl 163 SC 163.10 P 206 L 40 # 88

Wu, Mau-Lin MediaTek Inc.

Comment Type TR Comment Status A bucket1

The note "a" here is specific for Cable assembly and shall be removed, due to this is KR Clause

SuggestedRemedy

Remove note a

Response Response Status W

ACCEPT IN PRINCIPLE.

When this table was created in D2.1 the referenced footnote was accidentally included. There was no comment to include the provision in this footnote. Delete table footnote a.

Cl 163A SC 163A.3.1.3 P 308 L 25 # 22

Hidaka, Yasuo Credo Semiconductor, Inc.

Comment Type T Comment Status D withdrawn

f_r is also a parameter specified by the clause that invokes this method but missing in the list.

SuggestedRemedy

Change "A_t and T_b" with "A_t, T_b and f_r" in page 308 line 25. Apply the same change to page 307 line 13.

Proposed Response Response Status Z

REJECT.

This comment was WITHDRAWN by the commenter.

Cl 163A SC 163A.3.1.3 P 308 L 43 # 1

Brown, Matt Huawei

Comment Type E Comment Status A bucket1

extra closing parenthesis "Tr(ref))"

SuggestedRemedy

remove extra closing parenthesis

Response Response Status C

ACCEPT.