# Reference Architecture Proposals and Channel Data 

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## Outline

- 4 COM architectures

Data for each architecture vs a collection of channels
$\square$ Next steps

## 4 Signal Architecture Approaches

1. Zero Forced DFE
2. Quantized Forced DFE
3. One DFE tap and a number of (Rx)FFE taps
4. One DFE tap and a number of ( Rx )FFE taps with gain at cursor

## COM is based on the pulse response (Annex 93A)

Thru (ISI) channel response is $h^{(0)}(t)$ i.e. the pulse response

The pulse response $h^{(k)}(t)$ is derived from the voltage transfer function $H^{(k)}(f)$ (see 93A.1.4) using Equation (93A-24).

$$
\begin{equation*}
h^{(k)}(t)=\int_{-\infty}^{\infty} X(f) H^{(t)}(f) \exp (j 2 \pi f t) d t \tag{93~A-24}
\end{equation*}
$$

The following uses pulse response plots to describe COM equalization

## 

The FOM is calculated for each permitted combination of $c(-1), c(1)$, and $g_{\mathrm{DC}}$ values per Table $93 \mathrm{~A}-1$. The combination of values that maximizes the FOM, including the corresponding value of $t_{s}$ is used for the calculation of the interference and noise amplitude in 93A.I.7 and the calculation of COM in 93A.I.
$\square$ All legal Tx FFE and CTF (continuous time function) settings are considered

- Called a full grid search
- Caveat: Very often CTF settings dominate over the Tx FFE post cursor.
$\square$ Exception: Samples corresponding to DFE cursor of is $h^{(0)}(t)$ greater than certain values ( $\mathrm{b}_{\text {max }}$ ) are converted in to ISI noise

Example where $1^{\text {st }}$ DFE tap reach limit creating ISI noise


## Quantized DFE

$\square$ Same as Zero force except:

- Samples corresponding to a DFE cursor $h^{(0)}\left(t_{n}\right)$ greater than the DFE quantization step size are also converted into ISI noise



## One DFE tap + (Rx)FFE

$\square$ Same full grid as for zero forced DFE except

- 1 tap of DFE w/ an Rx FFE of a specified number and resolution of pre-cursors and post-cursors are determined from a vector forced optimization.
- The cursor for the vector forcing is $h^{(0)}\left(t_{s}\right)$ where $t_{s}$ is the sample point and
- The first post cursor is set the maximum allowed setting ( $\mathrm{b}_{\max }$ )
- $\mathrm{C}=\left(\left(\mathrm{HH}^{\prime} \star \mathrm{HH}\right)^{\wedge}-1 \star \mathrm{H}^{\prime}\right)^{\prime} \star \mathrm{FV}^{\prime}$;
- C are the Rx FFE taps HH is derived from $h^{(0)}(t)$
- FV is the forcing vector, $\mathrm{FV}=[\ldots 0,0$, As, bmax (1)*As, $0,0,0,0 \ldots]$
- FOM is computed from each CTF and Tx FFE setting with
- $h_{\text {fferx }}(f)$ is computed from the $C$ found as in eq 93A-32

$$
\begin{equation*}
H_{j f c}(f)=\sum_{i=-1}^{1} c(i) \exp \left(-j 2 \pi(i+1)\left(f / f_{b}\right)\right) \tag{93~A-21}
\end{equation*}
$$

$\square \operatorname{FFE}(3,32)$ used here for now

- 3 precursors and 32 post cursors

IEEE $802.3100 \mathrm{~Gb} / \mathrm{s}, \mathbf{2 0 0} \mathrm{Gb} / \mathrm{s}$, and $400 \mathrm{~Gb} / \mathrm{s}$ Electrical Interfaces Task Force

## One DFE tap $+(R x)$ FFE w/ Cursor Gain

$\square$ Same as one DFE tap and a number of Rx FFE taps (pre and post cursor) except:

- The cursor for the vector forcing $\left(h^{(0)}\left(t_{s}\right)\right.$ where $t_{s}$ is the sample point) has some gain
- $\mathrm{C}=\left(\left(\mathrm{HH}{ }^{\prime *} \mathrm{HH}\right)^{\wedge}-1 * \mathrm{HH}^{\prime}\right)^{\prime}{ }^{*} \mathrm{FV}^{\prime}$;
- C are the Rx FFE taps HH is derived from $h^{(0)}(t)$
- FV is the forcing vector, $\mathrm{FV}=\left[\ldots 0,0, A s * 10^{\text {gatn }} \frac{20}{20}, \mathrm{~b}_{\max }(1) *_{\mathrm{A} s}, 0,0,0,0 \ldots\right]$
- 3 dB gain seems to work best

| Table 93A-1 parameters |  |  |  |
| :---: | :---: | :---: | :---: |
| Parameter | Setting | Units | Information |
| f_b | 53.125 | GBd |  |
| f_min | 0.05 | GHz |  |
| Delta_f | 0.01 | GHz |  |
| C_d | [1.3e-4 1.3e-4] | nF | [TX RX] |
| 2_p select | [2] |  | [test cases to run] |
| z_p (TX) | [12 30] | mm | [test cases] |
| z_p (NEXT) | [12 30] | mm | [test cases] |
| 2_p (FEXT) | [12 30] | mm | [test cases] |
| $z_{\sim} \quad \mathrm{p}(\mathrm{RX})$ | [12 30] | mm | [test cases] |
| C_p | [1.1e-4 1.1e-4] | nF | [TX RX] |
| R_0 | 50 | Ohm |  |
| R_d | [ 5050 ] | Ohm | [TX RX] or selected |
| f_r | 0.75 | *fb |  |
| c(0) | 0.6 |  | min |
| $\mathrm{c}(-1)$ | [-0.28:0.025:0] |  | [min:step:max] |
| c(-2) | [0:0.05:0.1] |  | [min:step:max] |
| $\mathrm{c}(-3)$ | [-0.1:0.025:0] |  | [min:step:max] |
| c(-4) | 0 |  | [min:step:max] |
| c(1) | [-0.05:025:0] |  | [min:step:max] |
| g_DC | [-20:1:10] | dB | [min:step:max] |
| f_z | 21.25 | GHz |  |
| f_p 1 | 21.25 | GHz |  |
| f_p2 | 53.125 | GHz |  |
| A_V | 0.41 | V | tdr selected |
| A_fe | 0.41 | v | tdr selected |
| A_ne | 0.6 | v | tdr selected |
| L | 4 |  |  |
| M | 32 |  |  |
| N_b | 32 | UI |  |
| N_b_step | 0 |  | normailized |
| b_max(1) | 0.7 |  |  |
| b_max(2..N_b) | 0.2 |  |  |
| sigma_RJ | 0.01 | UI |  |
| A_DD | 0.02 | UI |  |
| eta_0 | 8.20E-09 | V^2/GH2 |  |
| SNR_TX | 32.5 | dB | tdr selected |
| R_LM | 0.95 |  |  |
| DER_0 | 1.00E-04 |  |  |
| Operational control |  |  |  |
| COM Pass threshold | 3 | dB |  |
| Include PCB | 0 | Value | 0, 1, 2 |
|  |  |  |  |
| g_DC_HP | [-6:1:0] |  | [min:step:max] |
| f_HP_PZ | 0.6640625 | GHz |  |



Set to zero

## COM config sheet for ZF or Q DFE



For reference

IEEE 802.3100 Gb/s, 200 Gb/s, and 400 Gb/s Electrical Interfaces Task Force

| Table 93A-1 parameters |  |  |  |
| :---: | :---: | :---: | :---: |
| Parameter | Setting | Units | Information |
| f_b | 53.125 | GBd |  |
| f_min | 0.05 | GHz |  |
| Delta_f | 0.01 | GHz |  |
| C_d | [1.3e-4 1.3e-4] | nF | [TX RX] |
| z_p select | [2] |  | [test cases to run] |
| z_p (TX) | [12 30] | mm | [test cases] |
| z_p (NEXT) | [12 30] | mm | [test cases] |
| 2_p (FEXT) | [1230] | mm | [test cases] |
| $z_{\text {_ }}(\mathrm{P}$ ( P$)$ | [12 30] | mm | [test cases] |
| C_p | [1.1e-4 1.1e-4] | nF | [TX RX] |
| R_0 | 50 | Ohm |  |
| R_d | [ 5050 ] | Ohm | [TX RX] or selected |
| f_r | 0.75 | *fb |  |
| c(0) | 0.6 |  | min |
| c(-1) | [-0.28:0.025:0] |  | [min:step:max] |
| $\mathrm{c}(-2)$ | [0:0.05:0.1] |  | [min:step:max] |
| c(-3) | 0 |  | [min:step:max] |
| c(-4) | 0 |  | [min:step:max] |
| c (1) | [-0.05:.025:0] |  | [min:step:max] |
| g_DC | [-20:1:10] | dB | [min:step:max] |
| f_z | 21.25 | GHz |  |
| f_p1 | 21.25 | GHz |  |
| f_p2 | 53.125 | GHz |  |
| A_v | 0.41 | V | tdr selected |
| A_fe | 0.41 | v | tdr selected |
| A_ne | 0.6 | v | tdr selected |
| L | 4 |  |  |
| M | 32 |  |  |
| N_b | 1 | UI |  |
| b_max(1) | 0.7 |  |  |
| b_max(2..N_b) | 0.2 |  |  |
| sigma_RJ | 0.01 | UI |  |
| A_DD | 0.02 | UI |  |
| eta_0 | 8.20E-09 | V^2/GHz |  |
| SNR_TX | 32.5 | dB | tdr selected |
| R_LM | 0.95 |  |  |
| DER_0 | 1.00E-04 |  |  |
| Operational control |  |  |  |
| COM Pass threshold | 3 | dB |  |
| Include PCB | 0 | Value | 0, 1, 2 |
|  |  |  |  |
| g_DC_HP | [-6:1:0] |  | [min:step:max] |
| f_HP_PZ | 0.6640625 | GHz |  |




| Table 92-12 parameters |  |  |
| :---: | :---: | :---: |
| Parameter | Setting |  |
| board_tl_gamma0_a1_a2 | $[04.114 \mathrm{e}-42.547 \mathrm{e}-4]$ |  |
| board_tl_tau | $6.191 \mathrm{E}-03$ | $\mathrm{~ns} / \mathrm{mm}$ |
| board_Z_c | 110 | Chm |
| Z_bp (TX) | 151 | mm |
| Z_bp (NEXT) | 72 | mm |
| z_bp (FEXT) | 72 | mm |
| Z_bp (RX) | 151 | mm |

## COM config sheet for FFE and w/wo gain

## Reference: ZF DFE




Channels:

- Cabled backplane (2)
- Cabled fabric switch (12)

Used channels with $\mathrm{COM} \geq 2.3 \mathrm{~dB}$
Analysis used 32 taps total (DFE+FFE or DFE-only)

- Is the ZF DFE too optimistic
- Does the implication of the ZF DFE require too much power



## Data Summary



- Quantized DFE seems like just derating COM of the ZF DFE
- FFE with gain seems to get closer to ZF DFE for high loss



## COM Correlations to DFE-based COM

More variability for the FFE based COM




Quantized DFE $=-0.4393+0.9172272^{*}$ DFE $\triangle$ Summary of Fit

| RSquare |  | 0.994505 |  |
| :---: | :---: | :---: | :---: |
| RSquare |  | 0.994047 |  |
| Root Me | Square Error | 0.051023 |  |
| Mean of | Response | 2.51465 |  |
| Observat | ons (or Sum Wgts) | 14 |  |
| $\checkmark$ Lack Of Fit |  |  |  |
| $\triangle$ Analysis of Variance |  |  |  |
| Source | DF $\begin{array}{r}\text { Sum of } \\ \text { Squares }\end{array}$ | Mean Square | F Rati |
| Model | 5.6535462 | 5.65355 | 2171.62 |
| Error | 120.0312405 | 0.00260 | Prob > |
| C. Total | $13 \quad 5.6847867$ |  | <. 0001 |
| $\triangle$ Parameter Estimates |  |  |  |
| Term | Estimate Std Er | ror t Ratio | Prob> $\mid$ \| $\mid$ |
| Intercept | -0.4393 0.0648 | -6.78 | <.0001* |
| DFE | 0.91722720 .01 | 46.6 | <.0001* |



- Linear Fit
- Bivariate Normal Ellipse $\mathrm{P}=0.950$


## $\triangle$ Linear Fit

\section*{$\triangle$ Summary of Fit <br> | RSquare | 0.94702 |
| :--- | ---: |
| RSquare Adj | 0.94261 |
| Root Mean Square Error | 0.24503 |
| Mean of Response | 2.16739 |
| Observations (or Sum Wgts) | 1 | Observations (or Sum Wgts) 2.16739 <br> Lack Of Fit <br> |  | Sum of |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Source | DF | Squares | Mean Square | FRatio |  |
| Model | 1 | 12.881333 | 12.8813 | 214.5404 |  |
| Error | 12 | 0.720498 | 0.0600 | Prob $>$ F |  |
| C. Total | 13 | 13.601831 |  | $<.0001^{*}$ |  |}

## $\triangle$ Parameter Estimates

$\begin{array}{lrrrr}\text { Term } & \text { Estimate } & \text { Std Error } & \boldsymbol{t} \text { Ratio } & \text { Prob }>|t| \\ \text { Intercept } & -2.291455 & 0.311381 & -7.36 & \end{array}$ $\begin{array}{lllll}\text { Intercept } & -2.291455 & 0.311381 & -7.36<.0001^{*} \\ \text { DFE } & 1.3845124 & 0.094524 & 14.65<0001^{*}\end{array}$

-Linear Fit

- Bivariate Normal Ellipse $\mathrm{P}=0.950$


## $\triangle$ Linear Fit

FFE 3dB Gain $=-2.710912+1.567303^{*}$ DFE
$\Delta$ Summary of Fit

| mary of Fit |  |  |
| :---: | :---: | :---: |
| RSquare | 0.881475 |  |
| RSquare Adj | 0.871597 |  |
| Root Mean Square Error | 0.430078 |  |
| Mean of Response | 2.336621 |  |
| Observations (or Sum Wgts) | 14 |  |
| $\triangleright$ Lack Of Fit |  |  |
| $\triangle$ Analysis of Variance |  |  |
| Source DF Sum of | Mean Square | F Rat |
| $\begin{array}{llll}\text { Model } & 1616.507187\end{array}$ | 16.5072 | 89.244 |
| Error $12 \quad 2.219600$ | 0.1850 | Prob |
| $\begin{array}{lll}\text { Total } & 13 & 18.72678\end{array}$ |  | <. 0 |


| $\Delta$ Parameter Estimates |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |
| Term | Estimate | Std Error | t Ratio | Prob $>\|t\|$ |
| Intercept | -2.710912 | 0.546529 | -4.96 | $0.0003^{*}$ |

$X$ and $Y$
axis are $d B$ of COM

## Summary \& Next Steps

$\square$ Reference EQ architecture choices impact on COM results
$\square$ More variability in results with DFE+FFE-based reference EQ
I Is a quantized DFE good enough?

- It seems like it is the same as raising the COM threshold
$\square$ Follow-on work
- Assess the sensitivity to \# of taps in the Rx Equalizer
- Look at algorithm to better optimize gain in FFE; goal being to reduce uncertainty in results
Follow-work for channels: Address PCB manufacturing to further reduce the channel ISI.


## Backup

## COM vs Channel IL




## Consolidated Data



## Consolidated Data \#2



## Quantized DFE




Delta calculated relative to ZF-DFE.



## DFE + FFE






## DFE + FFE w/ 3dB Cursor Gain



## Correlation to COM with DFE



