
Comment Agenda

162 cable assembly

162A-D Annexes

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Comment Agenda

| Topic – 162 CA | Comments |
|--|---|
| CA IL | 181 |
| CA ERL and Tr | [68], 44, champion_3ck_01_0720.pdf |
| CA DC RL | 71*, 181, 148, 74, haser_3ck_adhoc_02_061720.pdf |
| CA CD IL | 148*, 181 |
| CA CC RL | 73*, 181, 76, haser_3ck_adhoc_02_061720.pdf |
| CA COM Tr | 149 |
| CA COM SNRTX | 37*, 70, 77, 152, 11162 |
| Topic-162A | Comments |
| ILMaxHost(<i>f</i>) TBD, ILCamin(<i>f</i>) TBD | 182 |
| Topic -162C | Comments |
| MDI Connector contact map | #1, lusted_3ck_01_0720.pdf |

Comment Agenda

| Topic -162B | Comments |
|--------------------|-----------------|
| RL | 180*,86,87 |
| CMIL | 180*,88,89 |

| Topic -162B | Comments |
|--------------------|-----------------------------------|
| Frequency Range | 91*,79,80,81,84,85,87,89,90 |
| FOM _{ILD} | 83 value, 84 frequency range, 180 |
| ICN | 92,93,94,95,96 |

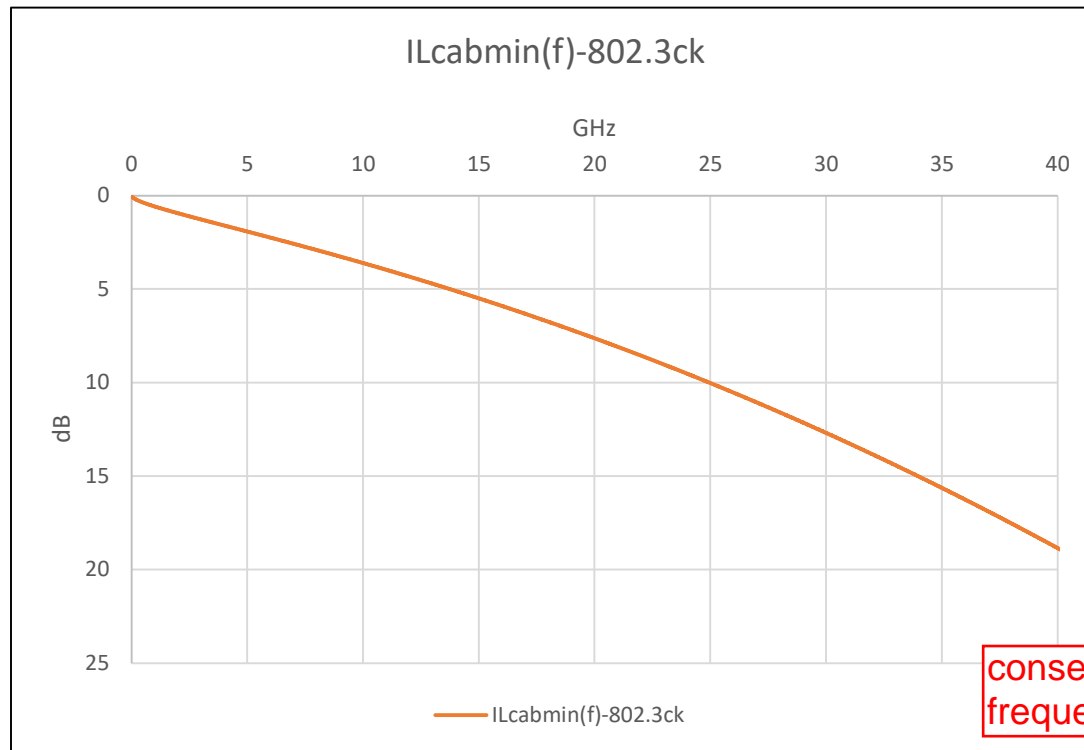
| Topic – MDI | Comments |
|---|-------------------------------|
| MDI connectors require normative references | 232*,233,234,251,252, 253,254 |

CA IL minimum - #181

162.11.2 Cable assembly insertion loss

The measured insertion loss of a cable assembly shall be greater than or equal to the minimum cable assembly insertion loss given in TBD and illustrated in TBD.

The measured insertion loss at 26.56 GHz of a cable assembly shall be less than or equal to 19.75 dB.



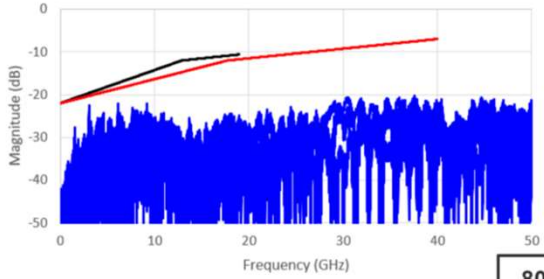
consensus around equation and frequency limits

$$IL_{cabmin}(f) = 0.418 \cdot \sqrt{f} + 0.177 \cdot f + 0.0059 \cdot f^2 \quad f \text{ from TBD GHz to 40 GHz}$$

$$IL_{cabmin}(f) = 11 \text{ dB} = 0.418 \cdot \sqrt{26.56} + 0.177 \cdot (26.56) + 0.0059 \cdot 26.56^2$$

CA DC RL – 71*, 181, 147, 74,

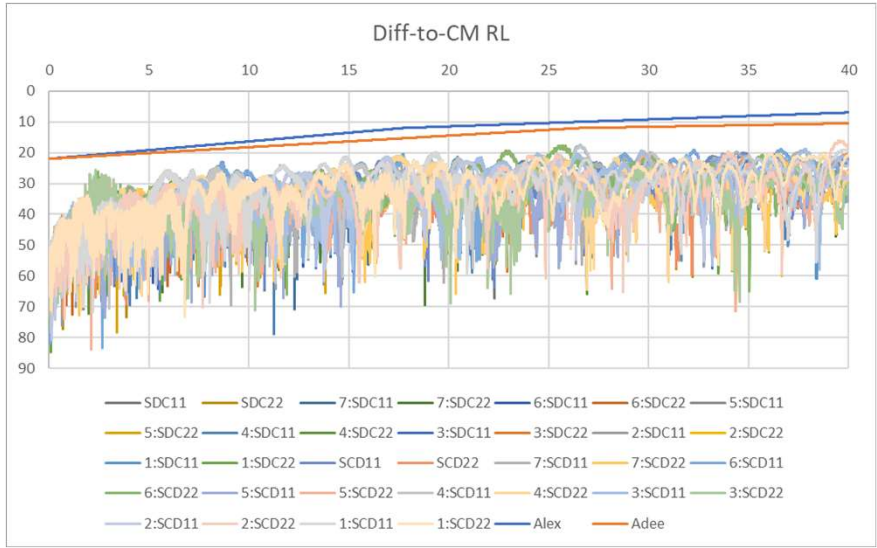
Differential to Common-Mode Return Loss:



Key:
BLUE = POC Data
BLACK = 802.3cd
RED = 802.3ck proposal

802.3ck proposal:
 $\left(22 - \frac{15}{26.56}f\right) \text{ dB} \quad 0.05 \text{ GHz} \leq f < 17.7 \text{ GHz}$
 $\left(16 - \frac{6}{26.56}f\right) \text{ dB} \quad 17.7 \text{ GHz} \leq f \leq 40 \text{ GHz}$

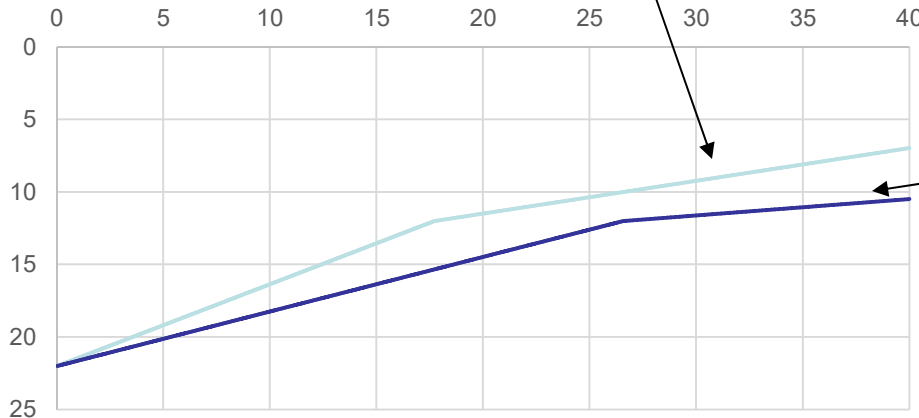
#71 haser_3ck_adhoc_02_061720.pdf



tracy_3ck_01a_0719.pdf

100 Gbps Copper Cable Measurement and S-Parameter File
 8 Channel Cable Measurement

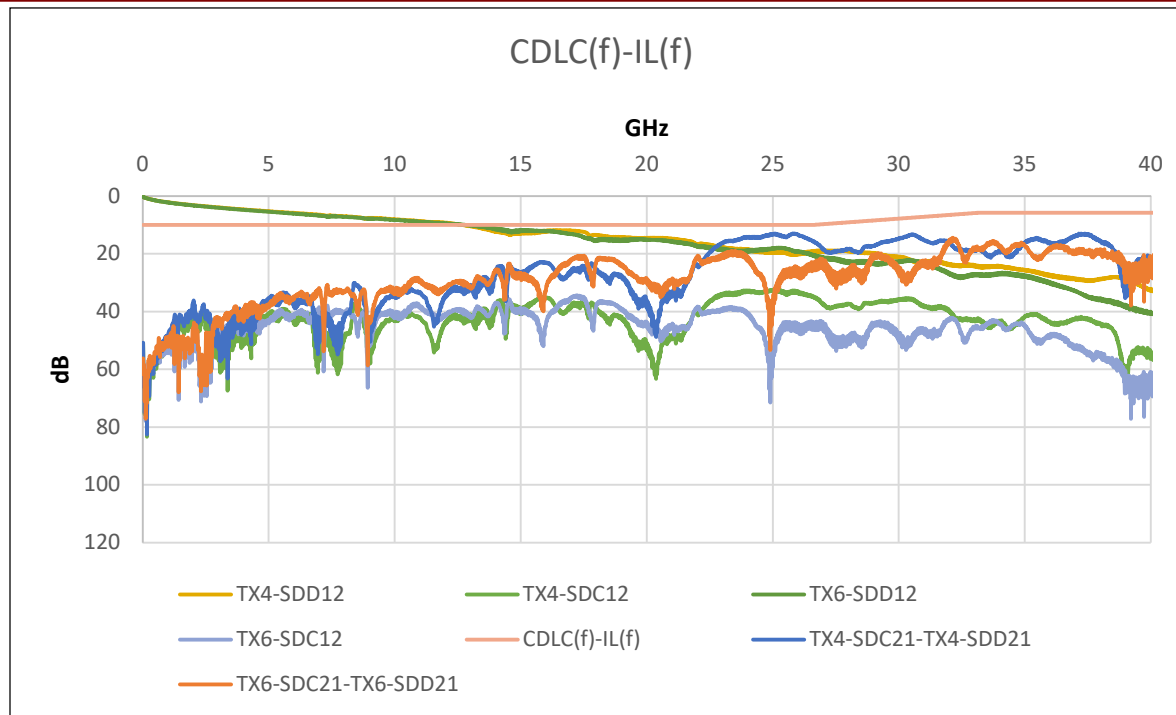
common to differential mode RL proposals



Alex # 71 Adee - #147

#147 ---CDRL(f) ≥
 $22 - 10 * f / f_N, 0.01 \leq f \leq f_N$
 $15 - 3 * f / f_N, f_N < f < 40$
 Where
 $f_N = 26.5625$ is the Nyquist frequency in GHz
 f is the frequency in GHz

CA CDCL – 148*, 74



tracy_3ck_01a_0719.pdf

100 Gbps Copper Cable
Measurement and S-Parameter
File 8 channel cable measurement

162.11.5 Cable assembly differential to common-mode conversion loss Conversion between differential and common-mode signals can result in degradation of the signal at the receiver, and in introduction of differential noise into the receiver. To limit these effects, the differential to common-mode mode conversion loss, relative to the insertion loss, has to be limited. f

The difference between the cable assembly differential to common-mode conversion loss

and the cable

assembly insertion loss shall meet Equation (162-new).

$$CDCL(f) - IL(f) \geq$$

$$10, 0.01 \leq f \leq f_N$$

$$27-17*f/f_N, f_N < f \leq 1.25*f_N$$

$$5.75, 1.25*f_N < f < 40$$

Where

$f_N=26.5625$ is the Nyquist frequency in GHz

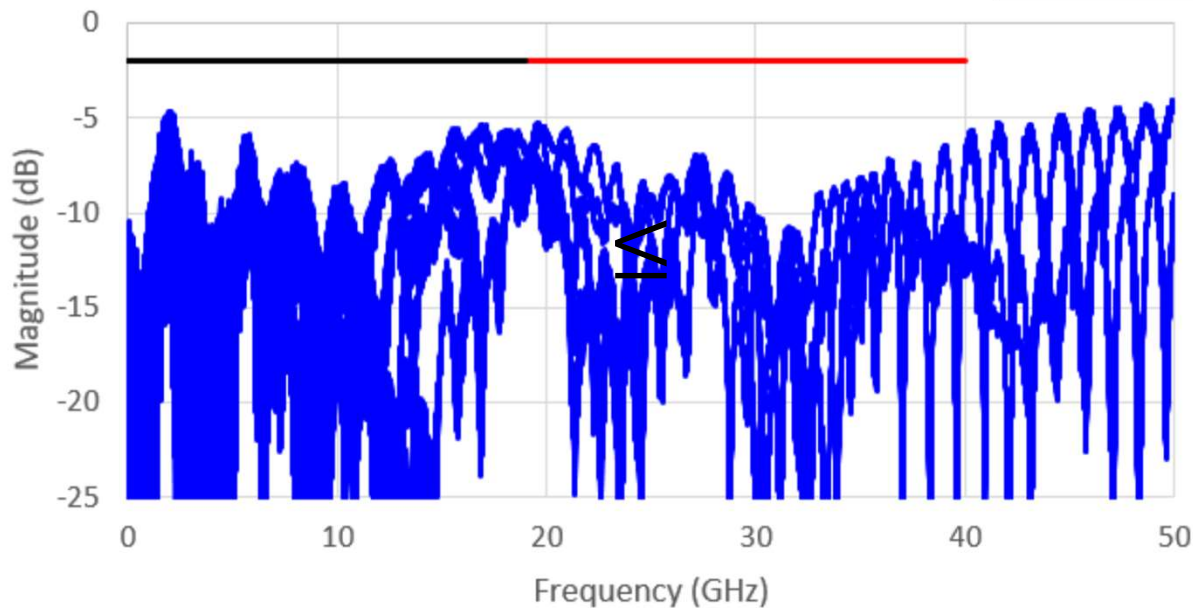
f is the frequency in GHz

CDCL(f) is the common-mode to differential inversion loss in dB at frequency

CA CC RL – 73*,181,76

Common-Mode to Common-Mode Return Loss:

Key:
BLUE = POC Data
BLACK* = 802.3cd
RED = 802.3ck proposal



802.3ck proposal: 2 dB $0.05 \text{ GHz} \leq f < 40 \text{ GHz}$

molex

haser_3ck_adhoc_02_061720.pdf

CA COM: SNRTx - #37

Cl 162 SC 162.11.7 P 160 L 42 # 77
 Haser, Alex Molex
 Comment Type TR Comment Status D CA COM
 Fill in TBD for SNR_Tx

SuggestedRemedy:
 Set SNR_Tx to 32.52 dB. All lanes of cables must pass COM; need a higher SNR_Tx value to do so given shared data (see champion_3ck_adhoc_01_031120)
 Proposed Response Response Status W
 PROPOSED ACCEPT
 The referenced presentation is here:
http://www.ieee802.org/3/ck/public/adhoc/mar11_20/champion_3ck_adhoc_01_031120.pdf
 Resolve using response to comment #37.

Cl 162 SC 162.11.7 P 160 L 43 # 152
 Ran, Adeel Intel
 Comment Type T Comment Status D CA COM

SNR_TX of the CR PHY needs to be somewhat lower than the corresponding CK PHY COM value (33 dB), to account for crosstalk that is introduced by practical host board routing. The mathematical host board model that is used in COM does not introduce any crosstalk.
 Proposed value is 32.5 dB.
 SuggestedRemedy:
 Change TBD to 32.5 dB.
 Proposed Response Response Status W
 PROPOSED ACCEPT.
 Resolve using response to comment #37.

Cl 162 SC 162.11.7 P 160 L 43 # 37
 Ben Artsi, Liav Marvell Technology
 Comment Type T Comment Status D CA COM
 Transmitter signal-to-noise ratio is TBD

SuggestedRemedy
 In benartsi_3ck_D1a_0919 it was shown that an optimized break-out section cross-talk degrades SNR by at least 0.5dB.
 This degradation is not represented in the "include PCB" section and should be accounted for in setting a proper value of SNR_Tx in section 162. In Table 163-10 SNR_Tx is specified to be 33dB and very likely same devices will be used for both sections. For comparison, in section 163 the break-out area crosstalk is included in the interconnect supplied to COM.
 According to all of the above, set 162 section's SNR_Tx COM value to be 32.5dB (to account for host board break-out section crosstalk which is not included in the "include PCB" specification). This value correlates to 163 section's SNR_Tx of 33dB and allows traces and connector crosstalk degradation of an additional 1dB up to TP2 resulting in the 31.5dB already specified in table 162-9 (SNDR = 31.5dB)

Proposed Response Response Status W
 PROPOSED ACCEPT
 The referenced presentation is here:
http://www.ieee802.org/3/ck/public/19_09/benartsi_3ck_D1a_0919.pdf
 Comments #37, #70, #77, #152 all propose the same remedy.

Cl 162 SC 162.11.7 P 160 L 42 # 70
 Champion, Bruce TE Connectivity
 Comment Type T Comment Status D CA COM
 SNR_Tx listed at TBD

SuggestedRemedy:
 Change TBD to 32.5 as described in champion_3ck_adhoc_01_031120.pdf. See presentation
 Proposed Response Response Status W
 PROPOSED ACCEPT
 The referenced ad hoc presentation is here:
http://www.ieee802.org/3/ck/public/adhoc/mar11_20/champion_3ck_adhoc_01_031120.pdf
 Pending review of the following new presentation:
http://www.ieee802.org/3/ck/public/20_07/champion_3ck_02_0720.pdf
 Resolve using response to comment #37.

Cl 162 SC 162.11.7 P 160 L 42 # 11162
 Palkert, Tom Molex
 Comment Type T Comment Status D CA COM
 [Comment resubmitted from Draft 1.1. 162.11.7, P160, L42]

Need value for SNRTx
 SuggestedRemedy:
 Make SNRTx = 33dB (See supporting presentation)
 Proposed Response Response Status W
 PROPOSED ACCEPT IN PRINCIPLE
 Resolve using the response to comment #37.

| C# | Proposal | Proposed Response |
|-------|----------|---|
| 37 | 32.5 dB | Accept |
| 70 | | |
| 77 | | |
| 152 | | |
| 11162 | 33 dB | AIP. Resolve using response to comment #37. |

CA COM Tr - #149

CI 162 SC 162.11.7 P 159 L 20 # 149
Ran, Adee Intel
Comment Type T Comment Status D ERL

(cross-clause)

Addressing the value of T_r used in COM, which is currently TBD.

Tr is not measurable, but it implicitly affects the transmitter specification peak/V_f which is measurable, and is also TBD in 162, 163 and 120F.

The proposed value for Tr (as used in COM, prior to the device package model) is 7.5 ps. This values matches results of feasible transmitter devices and will enable reasonable values of peak/V_f.

Note that the value 6.16 ps has been used in prior analysis, but has never been adopted. This latter value is overly aggressive and does not enable feasible design of transmitters. The proposed value has only a mild effect on COM results in comparison.

A presentation supporting this value and possible values for peak/V_f at Tp0 or TP0a (possibly informative) will be provided.

SuggestedRemedy

Change TBD to 7.5 ps in 162.11.7, in 163.10, and in 120F.4.1.

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

A related presentation was not submitted.
Resolve using the response to comment 45.

Comment Agenda - #182

| Topic-162A | Comments |
|----------------------------------|----------|
| ILMaxHost(f) TBD, ILCamin(f) TBD | 182 |

162A.4 Transmitter and receiver differential printed circuit board trace loss

The recommended maximum and minimum printed circuit board trace insertion losses are specified in **TBD** and **TBD**, respectively.

Note that the recommended maximum insertion loss allocation for the transmitter or receiver differential controlled impedance printed circuit boards with allowances for ball grid array (BGA) footprint and host connector footprints is 6.875 dB at 26.56 GHz and the recommended minimum insertion loss allocation for the transmitter or receiver differential controlled impedance printed circuit boards is 2.3 dB at 26.56 GHz. The recommended maximum insertion loss allocation for the transmitter or receiver differential controlled impedance printed circuit boards is consistent with the insertion loss from TP0 to TP2 or TP3 to TP5 given in **TBD** and an assumed mated connector loss of 1.6 dB.

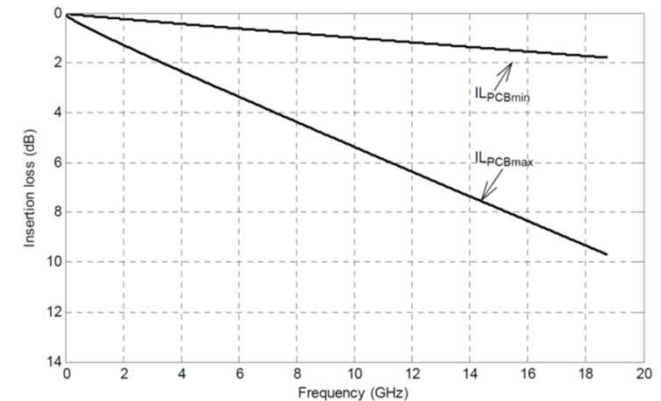


Figure 92A-1—Insertion Loss Tx or Rx PCB max and min

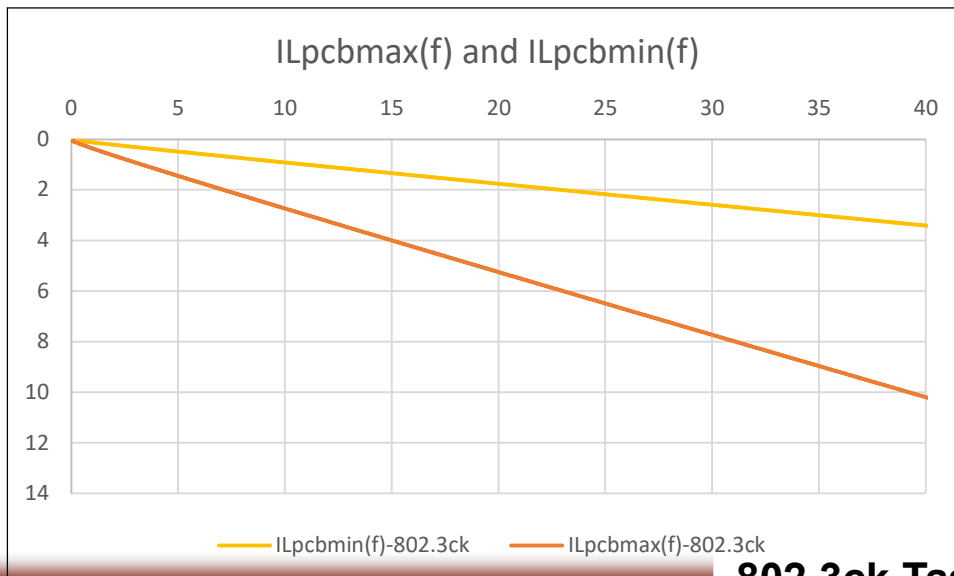
$$IL_{pcbmax}(f_{ghz}) = 0.0176 + 0.1082 * \text{SQRT}(f_{ghz}) + 0.2372 * f_{ghz}$$

$$IL_{pcbmax}(26.56) = 6.875 = 0.0176 + 0.1082 * \text{SQRT}(26.56) + 0.2372 * 26.56$$

$$IL_{pcbmin}(f) = 0.0059 + 0.0361 * \text{SQRT}(f_{ghz}) + 0.0794 * f_{ghz}$$

$$IL_{pcbmin}(26.56) = 2.30 = 0.0059 + 0.0361 * \text{SQRT}(26.56) + 0.0794 * 26.56$$

Editorial license update Annex reference to 162.11.2 ILCamin



Comment Agenda - #1

| Topic -162C | Comments |
|---------------------------|----------------------------|
| MDI Connector contact map | #1, lusted_3ck_01_0720.pdf |

| Pin# | Symbol | Description |
|------|--------|-------------------------------|
| 1 | GND | Ground |
| 2 | SL1p | Transmitter Data Non-Inverted |
| 3 | SL1n | Transmitter Data Inverted |
| 4 | GND | Ground |
| 5 | SL3p | Transmitter Data Non-Inverted |
| 6 | SL3n | Transmitter Data Inverted |
| 7 | GND | Ground |
| 8 | SL5p | Transmitter Data Non-Inverted |
| 9 | SL5n | Transmitter Data Inverted |
| 10 | GND | Ground |
| 11 | SL7p | Transmitter Data Non-Inverted |
| 12 | SL7n | Transmitter Data Inverted |
| 13 | GND | Ground |
| 18 | GND | Ground |
| 19 | DL6n | Receiver Data Inverted |
| 20 | DL6p | Receiver Data Non-Inverted |
| 21 | GND | Ground |
| 22 | DL4n | Receiver Data Inverted |
| 23 | DL4p | Receiver Data Non-Inverted |
| 24 | GND | Ground |
| 25 | DL2n | Receiver Data Inverted |
| 26 | DL2p | Receiver Data Non-Inverted |
| 27 | GND | Ground |
| 28 | DL0n | Receiver Data Inverted |
| 29 | DL0p | Receiver Data Non-Inverted |
| 30 | GND | Ground |
| 31 | GND | Ground |
| 32 | DL1p | Receiver Data Non-Inverted |

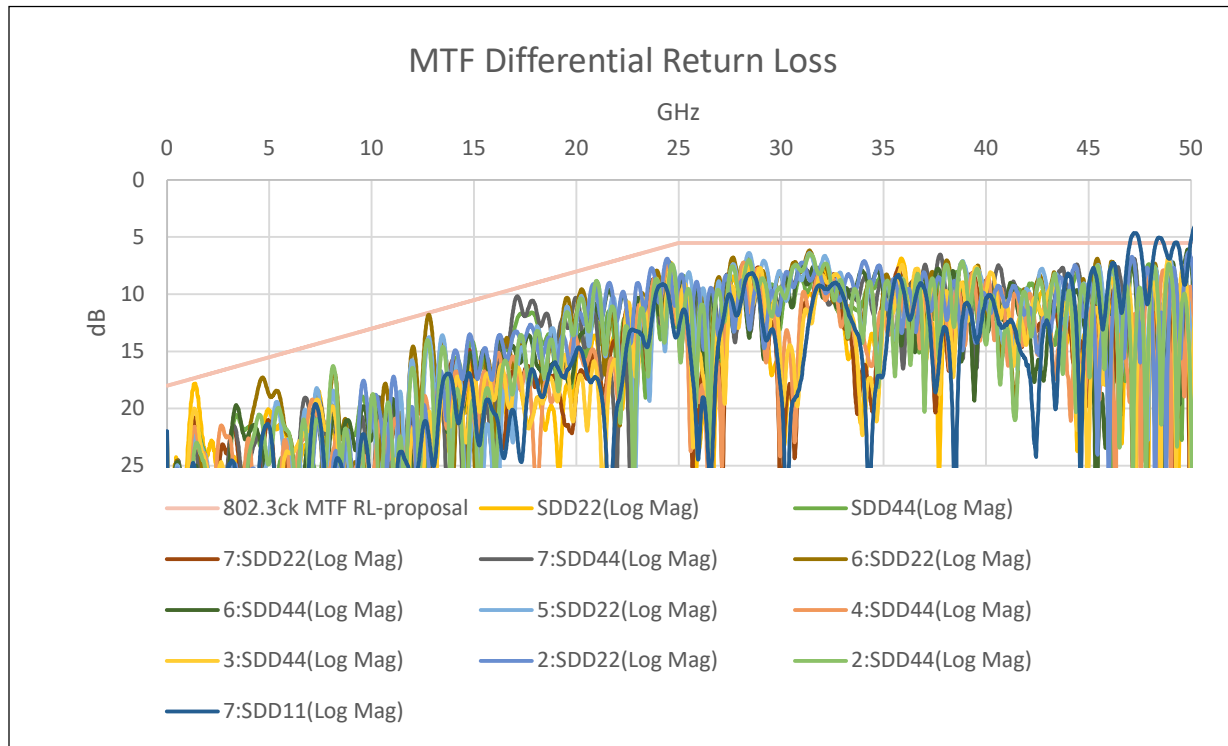
| | | |
|----|------|-------------------------------|
| 33 | DL1n | Receiver Data Inverted |
| 34 | GND | Ground |
| 35 | DL3p | Receiver Data Non-Inverted |
| 36 | DL3n | Receiver Data Inverted |
| 37 | GND | Ground |
| 38 | DL5p | Receiver Data Non-Inverted |
| 39 | DL5n | Receiver Data Inverted |
| 40 | GND | Ground |
| 41 | DL7p | Receiver Data Non-Inverted |
| 42 | DL7n | Receiver Data Inverted |
| 43 | GND | Ground |
| 48 | GND | Ground |
| 49 | SL6n | Transmitter Data Inverted |
| 50 | SL6p | Transmitter Data Non-Inverted |
| 51 | GND | Ground |
| 52 | SL4n | Transmitter Data Inverted |
| 53 | SL4p | Transmitter Data Non-Inverted |
| 54 | GND | Ground |
| 55 | SL2n | Transmitter Data Inverted |
| 56 | SL2p | Transmitter Data Non-Inverted |
| 57 | GND | Ground |
| 58 | SL0n | Transmitter Data Inverted |
| 59 | SL0p | Transmitter Data Non-Inverted |
| 60 | GND | Ground |

Comment Agenda

| Topic -162B | Comments |
|--------------------|-----------------|
| RL | [180],86,87 |
| CMIL | [180],88,89 |

#180 - MTF Differential Return Loss

#86,#87 - 162B.1.3.2 Mated test fixtures - **RL (TBD)** - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.



PROPOSAL: Differential Return Loss =

18-0.5*f_{GHz} 0.05 GHz ≤ f_{GHz} < 25 GHz

5.5 25 GHz ≤ f_{GHz} ≤ 40 GHz

#86,87 - MTF Differential Return Loss

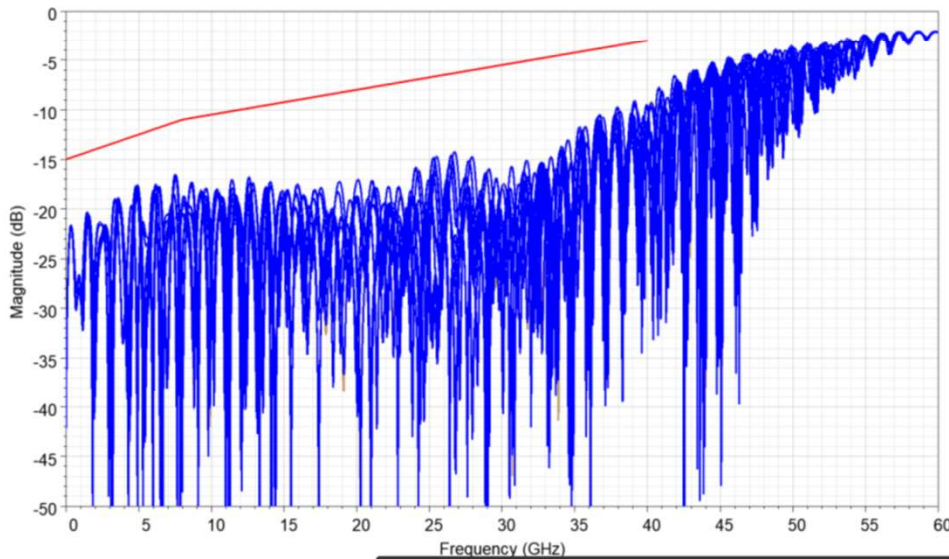
#86,#87 - 162B.1.3.2 Mated test fixtures - **RL (TBD)** - Change from 0.01 GHz $\leq f_{\text{GHz}} \leq 50$ GHz to **0.05 GHz $\leq f_{\text{GHz}} \leq 40$ GHz** and update figure.

SDD11:

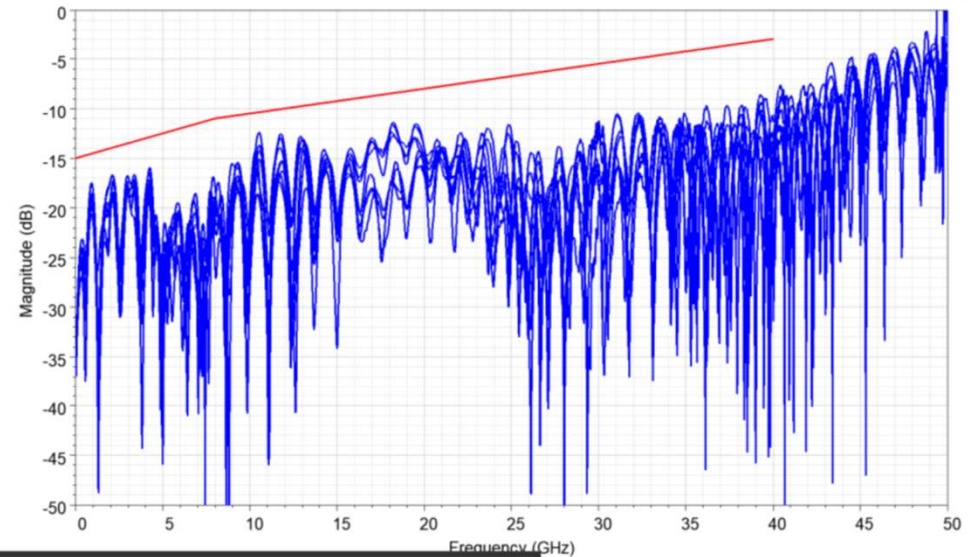
NOTE: 802.3ck D1.2 does not include a limit line for this parameter

Key:
BLACK = 802.3ck D1.2
RED = Proposal

Simulated Data:



Measured Data:



Proposal: $15 - 0.5f$ $f < 8 \text{ GHz}$
 $13 - 0.25f$ $8 \text{ GHz} \leq f \leq 40 \text{ GHz}$

molex

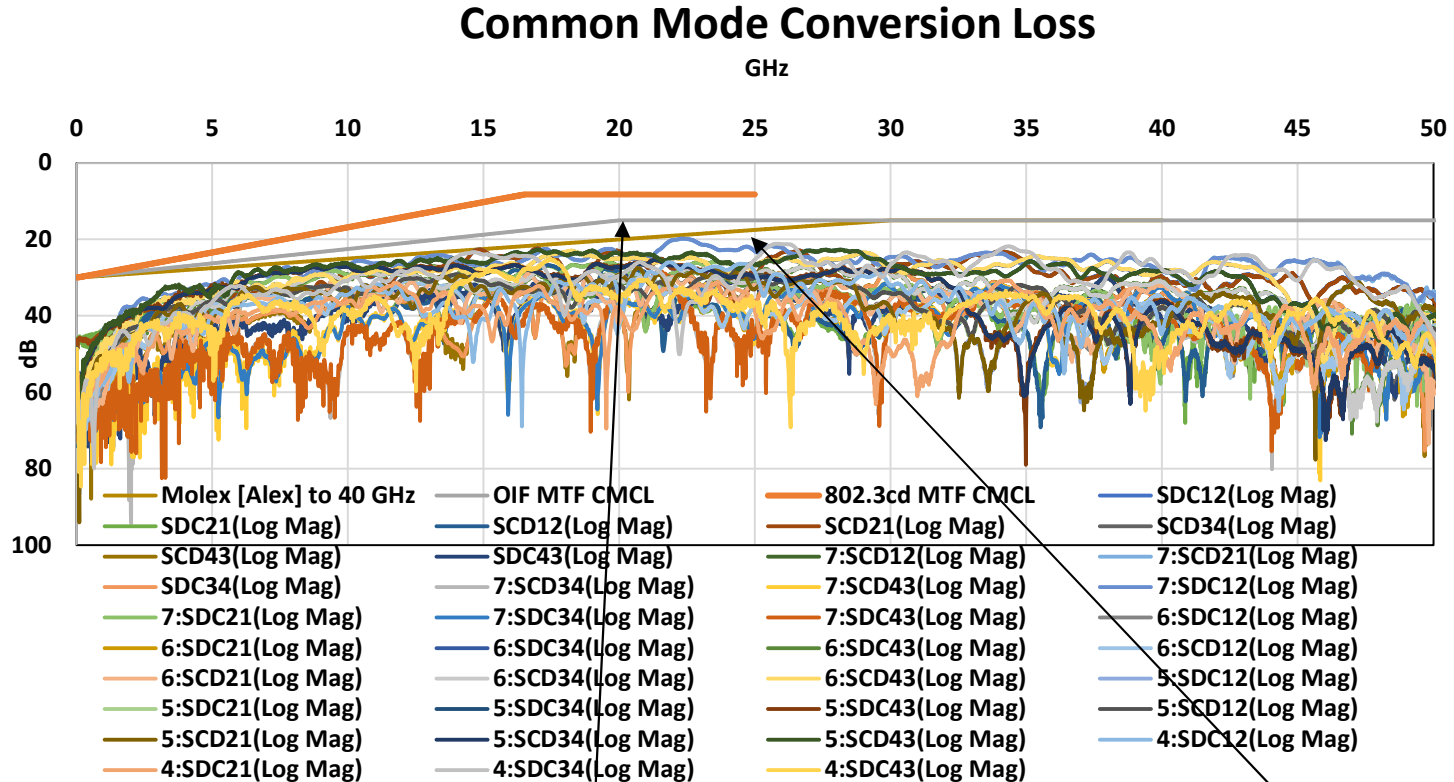
10

http://www.ieee802.org/3/ck/public/adhoc/jun24_20/haser_3ck_adhoc_01c_062420.pdf

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#180- MTF Common Mode Conversion Loss

#88,#89 - 162B.1.3.4 Mated test fixtures - **CMCIL (TBD)** - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.



PROPOSAL: Common Mode Conversion Loss =

$30 - (21/28) * f_{\text{GHz}}$ $0.05 \text{ TBD GHz} \leq f_{\text{GHz}} < 20 \text{ GHz}$

15 $20 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$

| | |
|-------------|---|
| $30 - 0.5f$ | $f < 30 \text{ GHz}$ |
| 15 | $30 \text{ GHz} \leq f \leq 40 \text{ GHz}$ |

#88,#89 -162B.1.3.4 Mated test fixtures - CMCIL

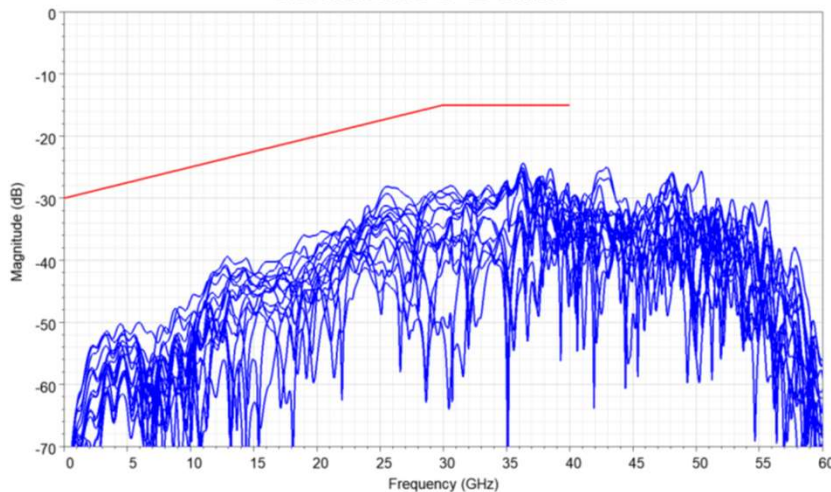
#88,#89 - 162B.1.3.4 Mated test fixtures - **CMCIL (TBD)** - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

SDC12:

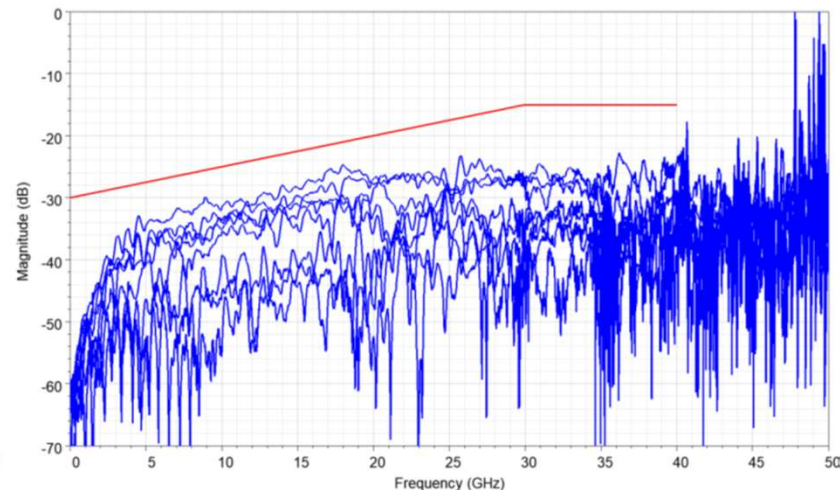
NOTE: 802.3ck D1.2 does not include a limit line for this parameter

Key:
BLACK = 802.3ck D1.2
RED = Proposal

Simulated Data:



Measured Data:



Proposal: $30 - 0.5f$ for $f < 30 \text{ GHz}$
 15 for $30 \text{ GHz} \leq f \leq 40 \text{ GHz}$

molex

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http://www.ieee802.org/3/ck/public/adhoc/jun24_20/haser_3ck_adhoc_01c_062420.pdf

Comment Agenda

| Topic -162B | Comments |
|--------------------|------------------------------------|
| Frequency Range | 91*,79,80,81,84,85,87,89,90 |
| FOM _{ILD} | 83* value, 84 frequency range, 180 |
| ICN | 92,93,94,95,96 |

Mated Test Fixtures – Frequency Range

- Proposal -
 - Comments 79,80,81,84,85,87,89,90,91
 - + Specify frequency range 0.05 GHz - 40 GHz to align with available in-house VNA ranges.
 - + For stop frequency; consider VNA ranges, MTF max IL, ICN sensitivity, and receiver BW ($0.75^* \text{ fb} = \sim 40 \text{ GHz}$); comment#91
 - + For start frequency; consider VNA ranges and FOMILD sensitivity.

Frequency range – 79,80,81,84,85,87,89,90,91

#79- 162B.1.1.1 Reference IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#80- 162B.1.2.1 Cable assembly test fixture reference IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#81,#82- 162B.1.3.1 Mated test fixtures max and min IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#83,#84 - 162B.1.3.1 FOM_{ILD} $T_t = \text{TBD} = 6.16 \text{ ps}$; change f_{min} to 0.05 GHz .

#85 - 162B.1.3.1 Mated test fixtures reference IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#85 - 162B.1.3.1 Mated test fixtures reference IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#86,#87 - 162B.1.3.2 Mated test fixtures - $RL \text{ (TBD)}$ - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#88,#89 - 162B.1.3.4 Mated test fixtures - $CMCIL \text{ (TBD)}$ - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#90, - 162B.1.3.5 Mated test fixtures CMDRL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#91, - 162B.1.3.6 Mated test fixtures integrated crosstalk noise – Add "Integrated crosstalk RMS noise voltages are measured over N uniformly-spaced frequencies f_n spanning the frequency range 50 MHz to 40 GHz with a minimum spacing of 10 MHz ." to the end of this section.

IL Frequency range Max – 79, 80, 81,82

#79- 162B.1.1.1 Reference IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

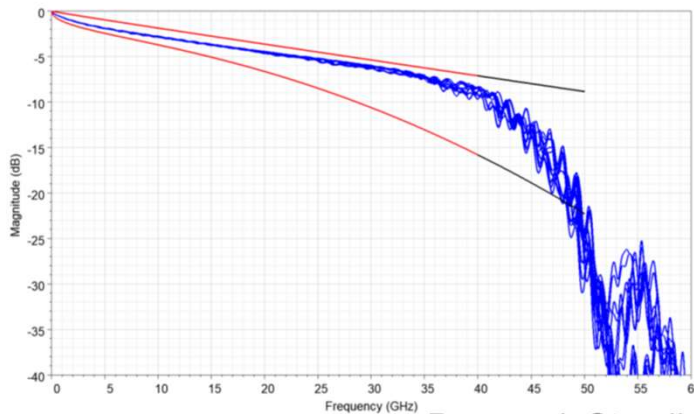
#80- 162B.1.2.1 Cable assembly test fixture reference IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

#81,#82- 162B.1.3.1 Mated test fixtures max and min IL - Change from $0.01 \text{ GHz} \leq f_{\text{GHz}} \leq 50 \text{ GHz}$ to $0.05 \text{ GHz} \leq f_{\text{GHz}} \leq 40 \text{ GHz}$ and update figure.

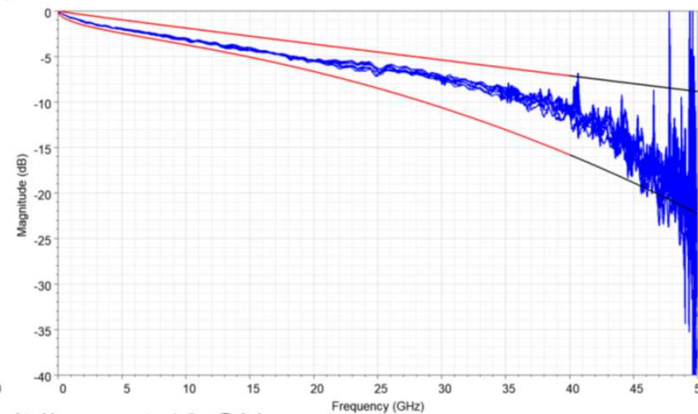
SDD21:

Key:
BLACK = 802.3ck D1.2
RED = Proposal

Simulated Data:



Measured Data:

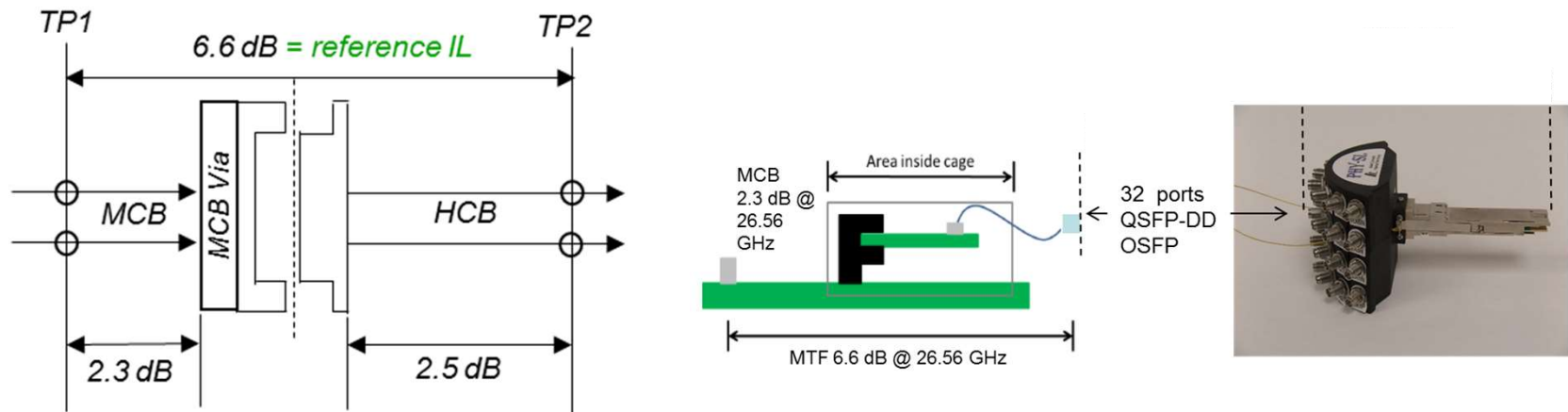


Proposal: Stop limit lines at 40 GHz

#180 - Mated Test Fixture Specifications

- Measurements with compliant PCB IL - HCB and MCB

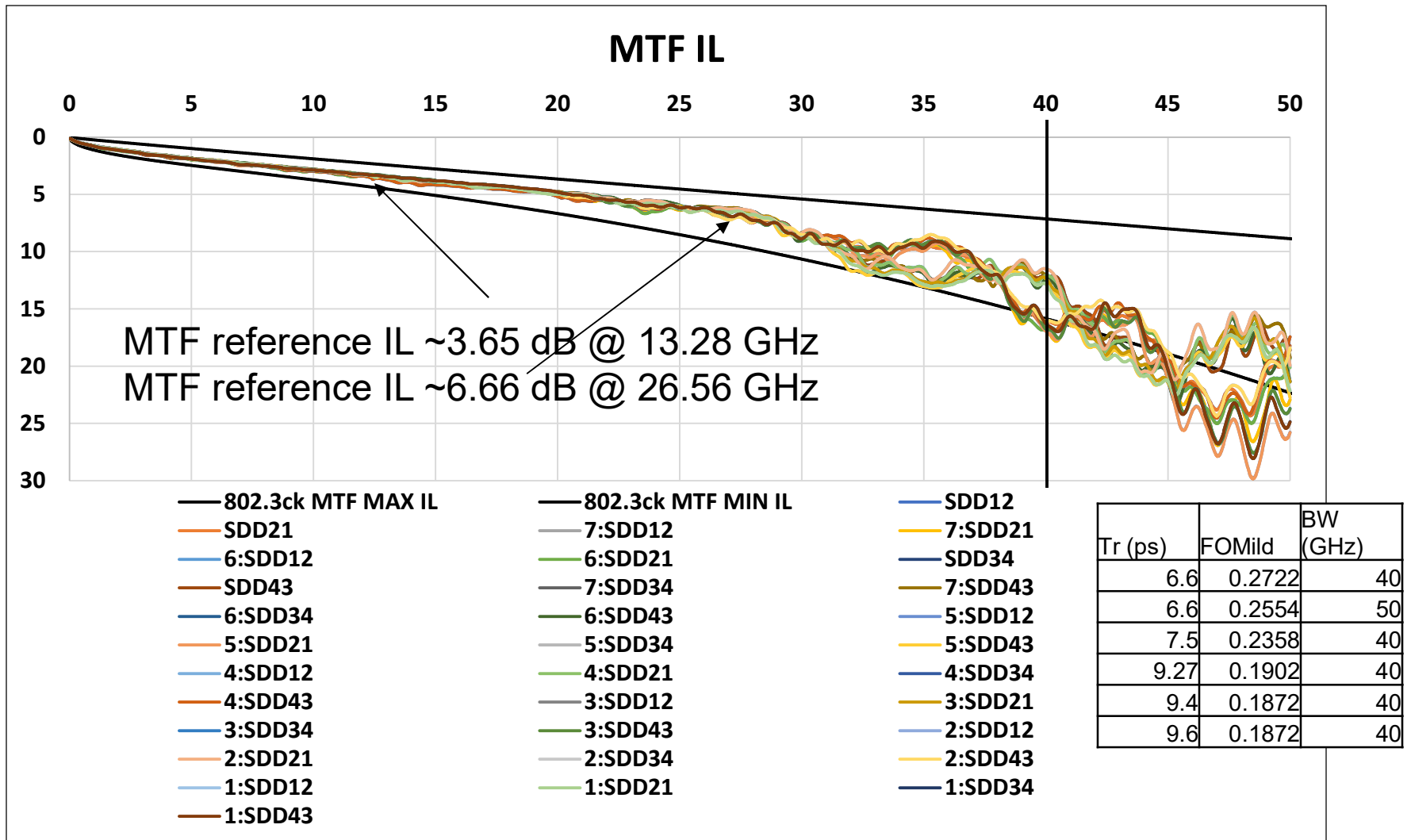
Mated Test Fixture Adopted in Baseline



Note: 2.3 dB MCB PCB includes test point IL
and MCB Via allowance is 0.2 dB

http://www.ieee802.org/3/ck/public/20_07/diminico_3ck_01_0720.pdf

In support of IL Frequency range Max – 79, 80, 81,82



- Measurements with compliant PCB IL - HCB and MCB

IL frequency range min- FOM_{ILD} 83, 84

FOM_{ILD}:

| Parameter | Value |
|--------------------------|--------------------|
| f_b | 53.125 GHz |
| T_r | 6.16 ps TBD |
| f_r | 0.75 x fb |
| f_{start} | 0.05 GHz* |
| f_{stop} | 40 GHz |
| FOM _{ILD} Limit | 0.18 dBrms |

* The current D1.2 specification identifies $f_{start} = 0.01$ GHz (see next slide for more information)

Key:
 Legacy Pair
 DD Pair
 Proposed Value

| Pair | Simulated | Measured |
|-----------------|--------------|--------------|
| 1 (Tx1) | 0.040 | |
| 2 (Tx3) | 0.042 | |
| 3 (Tx5) | 0.046 | |
| 4 (Tx7) | 0.053 | |
| 5 (Tx6) | 0.040 | 0.132 |
| 6 (Tx8) | 0.045 | 0.121 |
| 7 (Tx2) | 0.072 | 0.099 |
| 8 (Tx4) | 0.064 | 0.093 |
| 9 (Rx4) | 0.043 | |
| 10 (Rx2) | 0.040 | |
| 11 (Rx8) | 0.051 | |
| 12 (Rx6) | 0.047 | |
| 13 (Rx7) | 0.047 | 0.110 |
| 14 (Rx5) | 0.042 | 0.133 |
| 15 (Rx3) | 0.062 | 0.118 |
| 16 (Rx1) | 0.069 | 0.114 |
| MAX | 0.072 | 0.133 |

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- 7 #83 - $T_t = \text{TBD} = 6.16$ (TBD) ps;
 #84 - change **f_{min} to 0.05 GHz**

http://www.ieee802.org/3/ck/public/adhoc/jun24_20/haser_3ck_adhoc_01c_062420.pdf 23

ICN Frequency Range - 91

#91, - 162B.1.3.6 Mated test fixtures integrated crosstalk noise –
Add "Integrated crosstalk RMS noise voltages are measured over N uniformly-spaced frequencies f_n spanning the frequency range 50 MHz to 40 GHz with a minimum spacing of 10 MHz." to the end of this section..

Editors proposal; change first paragraph 162B.1.3.6 Mated test fixtures integrated crosstalk noise to read;

The SFP112 mated test fixture integrated near-end crosstalk noise voltage for the disturber near-end crosstalk loss is determined according to the method in 110B.1.3.7, given the disturber near-end crosstalk loss $NEXT_{loss}(f)$ is measured over N uniformly spaced frequencies f_n spanning the frequency range 50 MHz to 40 000 MHz with maximum frequency spacing of 10 MHz, and the parameters shown in Table 162B–1. The mated test fixture integrated near-end crosstalk noise voltage shall meet the specification in Table 162B–2.

Editors proposal; change 2nd paragraph 162B.1.3.6 Mated test fixtures integrated crosstalk noise to read;

The multi-lane mated test fixtures integrated crosstalk noise voltages is determined using Equation (92–44) through Equation (92–48), given the multiple disturber near-end crosstalk loss $MNEXT_{loss}(f)$ and multiple disturber far-end crosstalk loss $MDFEXT_{loss}(f)$ are measured over N uniformly-spaced frequencies f_n spanning the frequency range 50 MHz to 40 000 MHz with a maximum frequency spacing of 10 MHz, and the parameters shown in Table 162B–3 . The Multi-lane mated test fixture integrated crosstalk noise shall meet the specifications in Table 162B–4.

ICN -92,93,94,95,96

-#92- $T_{nt}=6.16$ (TBD) ps, #93- $T_{ft}=6.16$ (TBD)ps, #94 - $ICN_{FEXT}=4.2$ mV,
 #95 - $ICN_{NEXT}=1.5$ mV, #96 - $ICN_{Total}=4.4$ mV

| Max Values | Simulated | | | Measured | | |
|---------------------|--------------|--------------|---------------|--------------|--------------|---------------|
| Victim | ICN_{NEXT} | ICN_{FEXT} | ICN_{Total} | ICN_{NEXT} | ICN_{FEXT} | ICN_{Total} |
| $f_{stop} = 40$ GHz | 1.031 | 3.072 | 3.188 | 0.973 | 3.840 | 3.961 |
| $f_{stop} = 50$ GHz | 1.108 | 3.138 | 3.293 | 1.019 | 3.857 | 3.989 |

| Parameter | Value |
|---------------------|--------------------|
| f_b | 53.125 GHz |
| f_r | 0.75 x f_b |
| f_{min} | 0.05 GHz |
| f_{max} | 40 GHz |
| A_{nt}, A_{ft} | 600 mV |
| T_{nt}, T_{ft} | 6.16 ps TBD |
| ICN_{NEXT} Limit | 1.5 mV* |
| ICN_{FEXT} Limit | 4.2 mV* |
| ICN_{Total} Limit | 4.4 mV* |

- The ICN values calculated with a 40 GHz stop frequency are roughly the same as those calculated with a 50 GHz stop frequency
- This is due to the decay of the weighting function over this frequency band
- Calculating ICN all the way to 50 GHz has a minimal impact on the results
- Recommendation: For ICN, $f_{stop} = 40$ GHz
- NOTE: $0.75 \times f_b = 39.84$ GHz

* No change from 802.3cd spec

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http://www.ieee802.org/3/ck/public/adhoc/jun24_20/haser_3ck_adhoc_01c_062420.pdf 25

MDI - 232,233,234,251,252, 253,254

| Topic – MDI | Comments |
|---|------------------------------|
| MDI connectors require normative references | 232,233,234,251,252, 253,254 |

- **MDI connectors require normative references. We need these references to close on MDI connector naming.**

1.3 Normative references

Insert the following new references in alphanumeric order:

DSFP MSA Dual small form factor pluggable module, Rev. 1.0.¹

OSFP MSA Specification for OSFP octal small form factor pluggable module, Rev 3.0.²

QSFP112 **TBD**

QSFP-DD MSA QSFP-DD Hardware Specification for QSFP double density 8x pluggable transceiver, Rev 5.0.³

QSFP-DD800 MSA QSFP-DD Specification for 800G operation, Rev 1.0.⁴

SFP112 **TBD**

SFP-DD MSA SFP-DD Hardware Specification for SFP double density 2X pluggable transceiver, Rev 3.0.⁵

Editor's note: Some references above are placeholders for required references to be provided at a later date.

MDI - 232,233,234,251,252, 253,254

| Topic – MDI | Comments |
|---|------------------------------|
| MDI connectors require normative references | 232,233,234,251,252, 253,254 |

PROPOSED ACCEPT IN PRINCIPAL.

In 1.3, list the following normative references:

DSFP MSA Dual small form factor pluggable module, Rev. 1.0 September 12, 2018

OSFP MSA Specification for OSFP octal small form factor pluggable module, Rev 3.0 March 14th, 2020

QSFP+ - Specification for QSFP+ 28 Gb/s 4X Pluggable Transceiver Solution SFF-8665, Rev 1.9, June 29, 2015

QSFP-DD800 MSA QSFP - DD Specification for 800G operation, Rev 1.0 March 6, 2020

SFP+ Specification for SFP+ Module and Cage, SFF-8432, Rev 5.2a November 30, 2018

SFP-DD MSA SFP-DD Hardware Specification for SFP double density 2X pluggable transceiver, Rev 3.0 April 10, 2019

Throughout the draft...

Replace "SFP112" with "SFP+"

Replace "SFP112-DD" with "SFP-DD"

Replace "QSFP112" with "QSFP+"

Replace "QSFP112-DD" with "QSFP-DD800"

Implement with editorial license.