Comment Summaries: 93A, Cross-clause editorial, TPOv

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IEEE P802.3ck Task Force October 19,2020

CC 162/163/120F Editorial

C/ 162	SC 162.9.3	P 147	L1	# 49		J _{RMS} J3u Even-odd jitter, pk-pk ^d	162.9.3.3 162.9.3.3 162.9.3.3	0.023 0.115 0.019	UI UI UI
Ran, Adee	9	Intel				Unit interval nominal		18.82353	ps
Comment Footno test pr	Type T ote d includes imp rocedure, not as a	Comment Status D portant information for measu a comment on the table (it doe	rement that shou es not change the	editorial Id be stated in the e specification).		^a Measurement uses the method described in 93.8.1.3 with the exce ^b Implementations are recommended to use the same step size for a ^c Measurement uses the method described in 120D.3.1.6 with the e used.	ption that the PRI Il coefficients. xception that the	3S13Q test pattern is used linear fit procedure in 162	.9.3.1.1 is
Suggested Delete by clar	dRemedy e footnote d and ir luse 163 and shou	nstead add an informative NC Ild also be used for 120F).	TE in 162.9.3.3 (which is referred to		Copyright © 2020 IEEE. All r This is an unapproved IEEE Standards	ights reserved. draft, subject to c	hange.	
Also d	delete footnote e in	n Table 163-5.				148			
Proposed	Response	Response Status W				140			
PROP	POSED ACCEPT.								
[Editor	r's note: CC: 163,	120F]			I	Draft Amendment to IEEE Std 802.3-2018 IEEE P802.3ck 100 Gb/s, 200 Gb/s, and 400 Gb/s Electrical Interface dIf the measuring instrument is triggered by a clock based on the si- iitter may not be correctly observed.	es Task Force gnaling rate divid	IEEE Draft P802 1st Septer ed by an even number, the	2.3ck/D1.3 nber 2020 : even-odd
Also 163. 120f	apply the .9.2 (note F.3.1.	e implementatior e in Table 163-5)	n to and to	Insert —		Note: If the measuring instrument is triggered by a clo by an even number, the even-odd jitter may not be con 162.9.3.1 Transmitter output waveform The transmit function includes programmable equalization to co of the channel and facilitate data recovery at the receiver. The fur each lane is the five-tap transversal filter shown in Figure 162–3.	ock based on t rectly observe mpensate for the actional model for	he signaling rate div ed. frequency-dependent lo r the transmit equalizer o	vided oss on

-1 Output jitter (max)

Implementation:

93A

IEEE P802.3ck Task Force, October 2020

C/ 93A	SC 93A.1	
Healey, A	Adam	

P 195 Broadcom Inc. L 24

description

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Comment Type E Comment Status D

What is a "pad" in this context and does the description really fit this parameter? Note that this change to the parameter name, should it persist, should be propagated to every COM parameter table in IEEE Std 802.3 and not just the ones created or modified by this amendment. This does not seem worthwhile since the change to the name does not add any descriptive value.

SuggestedRemedy

Remove "pad" from the description of this parameter (i.e., undo the change). Update Tables 162-18, 163-11, and 120F-7 accordingly.

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Implement the suggested remedy. Also change "single-ended device bump capacitance" to "single-ended humn canacitance"

[Editor's note: CC: 162, 163, 120F]

Implementation:

Table 93A-1-COM parameters

Parameter	Reference	Symbol	Units
Signaling rate	93A.1.1	fb	GBd
Maximum start frequency	93A.1.1	f_{\min}	GHz
Maximum frequency step	93A.1.1	Δf	GHz
Device package model Single-ended device <u>pad</u> capacitance ^a <u>Single-ended device series inductance^a</u> <u>Single-ended device bump capacitance^a</u> Transmission line length ^a Single-ended package capacitance at package-to-board interface ^a Transmission line characteristic impedance ^a <u>Transmission line 2 length^a</u> <u>Transmission line parameter, a₁^b <u>Transmission line parameter, a₂^c</u> <u>Transmission line 2 characteristic impedance^a</u></u>	93A.1.2	C ユン ポン ポン ない 2 ユー コン	F H H H H H H H H H H H H H H H H H H H

Also apply the implementation to Table 162-18, Table 162-11, Table 120F-7.

C/ 93A SC 93A.1.2.1 P 198 L 3 # 233 Dawe, Piers Nvidia Comment Type T Comment Status D cascade Do we need to consider cascading 4-port networks? SuggestedRemedy Proposed Response Response Status W PROPOSED REJECT. The comment is in the form of a question and there is not remedy provided.

CI 93A SC 93A.1.2.1 P 198 L 10 # 234 Dawe, Piers Nvidia Comment Status D Comment Type T cascade It may be helpful to the reader (particularly someone programming this function) to know that cascade() is associative. SuggestedRemedy Add a sentence: cascade is associative: cascade(S(w), cascade(S(x), S(y))) = cascade(cascade(S(w), S(x)), S(y)). Proposed Response Response Status W PROPOSED REJECT.

Although the forms shown in the suggested remedy are valid, they can be deduced from equations already provided.

TPOv: 163A/120F/163

Comments 29 & 62

C/ 163	SC 163.9.2	P 176	L 44	# 29
Healey, Adam		Broadcom Inc.		
Comment 1	Type T	Comment Status D		TP0v method

The reference to 163A.3.2.2 is in danger of becoming circular. Annex 163A is mostly written to be generic and states that PHY/interface-specific parameters are "specified by the clause that invokes this method". However, no such specifications can be found in this clause, or in Annex 120F, that provides this information. This includes "test channel requirements", electrical characteristics used to compute S^(tp), values for Tr, fr, At, Tb, etc. One could assume that "test channel" requirements are given in the transmitter test fixture definition in 163.9.2.1, and the other values are the same as those used to compute COM from 163.10.1, but this should not be left to assumptions. It is unclear whether test 1 or test 2 (or test 1 AND test 2) characteristics for S^(tp) should be used and clarity on this point needs to be provided.

SuggestedRemedy

Add a new subclause to Clause 163 and change the reference for "dERL", "dvf", and "dvpeak" to this new subclause. The content of this subclause should be specifications for the PMD/interface-specific parameters that Annex 163A says are to be defined by the "clause that invokes this method". Similar changes would be necessary for Annex 120F.

w

Proposed Response	Response	Status
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PROPOSED ACCEPT IN PRINCIPLE.

Resolve using the response to comment #62. [Editor's note: CC: 163, 120F]

C/ 163	SC 163.9.2	P 1	76	L 48	# 62
Ran, Adee		Intel			
Comment Ty	pe T	Comment Status	D		TP0v method

dv_f and dv_peak refer directly to 163A.3.2.1, but some parameters are missing for the calculations:

A_t - should be taken from table 163-11 (or specify as the value 0.4 V)

z_p - should be the maximum value from table 163-11

SuggestedRemedy

Add a subclause under 162.9.2 (similar to 163.9.2.3 for dERL) to define the calculation of dv_f and dv_peak; in that subclause, point to 163A.3.2.1 and supply the required parameters as in the comment.

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Implement suggested remedy under 163.9.2 with editorial license. For task force discussion [Editor's note: CC: 163, 120F]

Implementation: Insert 163.9.2.1 with definitions and values or calculations (as appropriate) for T_r, f_r, A_t, T_b, dv_f, dv_peak, & test fixture. Specify reference package conditions (1, 2, or both).

C/ 163A SC 163A.1 P 280 L 47 # 205 Wu, Mau-Lin MediaTek Comment Type T Comment Status D TP0v method

By adopting "TP0v" test fixture methodology, not only ERL, vf, vpeak, but also AC commonmode RMS voltage shall be scaled by IL of TP0v test fixture.

SuggestedRemedy

If we take the V_ACCM as the notation for "AC common-mode RMS voltage", propose to change the blocks of "Measured ERL, V_f, V_peak" & "Reference ERL, V_f, V_peak" in Figure 163A-1 to "Measured ERL, V_f, V_peak, V_ACCM" & "Reference ERL, V_f, V_peak, V_ACCM".

The paragraphs in Annex 163 related to this change shall be modified accordingly. Some new paragraphs may need if necessary.

Plan to provide one contribution, wu_3ck_01_1120.pdf, for more details.

Proposed Response Response Status W

PROPOSED REJECT.

The proposed remedy is not sufficiently complete to implement. Pending presentation and task force discussion. [Editor's note: Add presentation URL.]

Comment #205 – How to derive V_{ACCM} at TPOv

- Take V_{ACCM} as the notation for "AC common-mode output voltage"
- Procedures to derive dV_{ACCM}
- Define V_{ACCM} at source (Device TX out or TPO, TBD) as TBD mV
- Derive reference V_{ACCM} based on Equation (TBD)
 - Equation is TBD
- Measured V_{ACCM} at TPOv
- Calculate difference between measured and reference AC common-mode output voltage (max), *dV_{ACCM}* as
 - Measured V_{ACCM} reference V_{ACCM}

Proposals

- Define V_{ACCM} at source (Device TX out or TPO, TBD) as TBD mV
- Change the blocks in Figure 163A-1
 - − Measured ERL, V_f , V_{peak} → Measured ERL, V_f , V_{peak} , V_{ACCM}
 - − Reference *ERL*, V_{f} , V_{peak} → Reference *ERL*, V_{f} , V_{peak} , V_{ACCM}

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- The paragraphs in Annex 163 related to this change shall be modified accordingly
 - Some new paragraphs may need
 - Editorial license

IEEE

P802.3ck

https://www.ieee802.org/3/ck/public/20_10/wu_3ck_01_1020.pdf



Figure 163A-1—Measurement method for transmitter reference steady-state voltage, pulse peak and ERL

Also refer to https://www.ieee802.org/3/ck/public/adhoc/sept09 20/wu 3ck adhoc 01 090920.pdf



Change the title of 163A.2 to "Test fixture" and replace its contents with the following: "The test fixture is between test points TP0 and TP0v as shown in Figure 163A-2. Test fixture requirements are specified by the clause that invokes this method."

Proposed Response Response Status W

PROPOSED ACCEPT.

Implementation:

163A.2 Test points Test fixture

The transmitter test channel is defined between test points TPO and TPOv in the transmitter test fixture, and is depicted in Figure 163A-2. The test channel requirements are specified by the clause that invokes this method.

The test fixture is between test points TP0 and TP0v as shown in Figure 163A-2. Test fixture requirements are specified by the clause that invokes this method.



TP0 is the interface between Transmitter package ball and PCB as shown in Figure 163-3. TP0 is not stable for measurement, because TP0 is highly non-TEM mode. A replica test fixture may have a test point corresponding to TP0, but this cannot be exactly same as TP0 due to the difficulty of measurement at TP0. In order to remind this difference, we should make the label of the test point for replica test fixture different from TP0. We should not assume replica test fixture is same as actual test fixture. Also for clarification, I suppose we should differentiate the label of TP0v between the test fixture attached to DUT and the replica test fixture.

SuggestedRemedy

Use TP0r and TP0vr as the labels for the test points where the replica test fixture may be used.

Proposed Response Response Status W

PROPOSED REJECT.

Defining different test point labels is not necessary or helpful. The suggested remedy does not add clarity to the specification.



L 25 P 281 # 35 C/ 163A SC 163A.3.1 Healey, Adam Broadcom Inc. Comment Type Comment Status D Т TP0v method In Figure 163A-2, termination resistance at TP0v should represent an instrument and not a device (i.e., it should be the reference resistance R_0 and not the device resistance R_d). SuggestedRemedy Replace "R_0" with "R_d". Proposed Response Response Status W PROPOSED ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Implementation:



NOTE-The transmitter reference package uses the maximum length specified by the referring subclause.

Figure 163A–2—Configuration for transmitter reference steady-state voltage, pulse peak and ERL

Т

C/ 163A SC 163A.3.1

Ran, Adee

Comment Type

P 281

Intel

58

Comment Status D TPOv method

L 40

"The scattering parameters for the reference package, S(tp), are determined using the method in 93A.1.2, with electrical characteristics specified in the clause that invokes this method"

Typically there are two reference package for the Tx and two possibly other ones for the Rx. It is not stated which one should be used.

A DUT should be allowed to be as "bad" as the worst of the two reference packages for any of the parameters.

Editorially it seems that this should be stated separately in 163A.3.1.1 for v_peak and v_f and in 163A.3.1.2 for ERL (although the same rule applies in both cases).

SuggestedRemedy

Add a sentence in 163A.3.1.1 after the paragraph "The reference pulse response peak (...) is the peak value of h(t)"

such as the following:

"If the invoking clause lists more than one set of reference package parameters, the calculation is performed with each set, and the minimum value is used as the reference value."

Add a similar sentence at the end of 163A.3.1.1 (after the definition of $v_f(ref)$) and at the end of 163A.3.1.2 (for ERL reference).

Proposed Response Response Status W PROPOSED ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Implementation:

The reference pulse response peak, $v_{peak}^{(ref)}$, is the peak value of h(t).

From the output pulse response calculate the reference value for the transmitter output steady state voltage, $v_f^{(ref)}$, using Equation (163A–3).

$$v_f^{(ref)} = \sum_{i=0}^{n_v} h(t - (i \cdot t_b))$$
(163A-3)

where t_b

is the unit interval in ps

 N_{v}

represents the number of symbols to take into account and has the same value as for the measured steady-state voltage in 162.9.3.1.2.

163A.3.1.2 Effective return loss reference value

Effective return loss (ERL) is defined in 93A.5. The ERL reference value is determined as follows. Obtain the pulse time-domain reflection (PTDR) response from $S^{(0)}$ using Equation (93A–58) and Equation (93A–59). Determine the ERL reference value from the PTDR response using the method in 93A.5.2.

Insert the following text at the locations marked with the arrows above.

If the invoking clause lists more than one set of reference package parameters, the calculation is performed with each set, and the minimum value is used as the reference value.



IEEE specifies interfaces not devices, and the term DUT is not used.

Comment #277 & 278







[Ohms] and the single-ended termination resistance, R_d, specified by the clause that invokes this method."

Proposed Response Response Status W

PROPOSED ACCEPT.

Implementation:

163A.3.1.1 Steady-state voltage and pulse peak reference values

Calculate the voltage transfer function, $H_{2I}(f)$, of the terminated virtual reference channel from $S^{(0)}$ using Equation (93A-17) and Equation (93A-18) with the reference impedance, R_0 , set to 50 Ω and the singleended termination, R_d , specified by the clause that invokes this method.

Calculate the voltage transfer function, $H_{21}(f)$ from the scattering parameters of the virtual reference channel, $S^{(0)}$, using Equation (93A-18) where Γ_1 is given by Equation (93A-17) and Γ_2 is set to 0. In Equation (93A-17), the single-ended reference resistance R_0 is set to 50 ohms and the single-ended termination resistance, R_d , specified by the clause that invokes this method.



Implement the suggsted remedy with editorial license.

Implementation:

C/ 163A	SC 163A.3.1.2	P 282	L 30	# 37
Healey, Adam		Broadcom Inc.		

Comment Type T

Comment Status D

Equation (93A-58) and Equation (93A-59) do not calculate the PDTR response from S^(0). There is an additional step required to obtain the reflection coefficient $s_{ii}(f)$ for the case where R_d is not equal to R_0. Also, the value of T_fx should be 0.

SuggestedRemedy

Replace the contents of 163A.3.1.2 with the following: "The reference reflection coefficient at TP0v is given by Equation (93A-7) where $[s_22]^{(x)}$ is GAMMA1 as defined by Equation (93A-17) and $[s_ji]^{(y)}$ are the components of the scattering matrix of the virtual reference channel S^(0). In Equation (93A-17), the single-ended reference resistance R_0 is set to 50 [Ohms] and the single-ended termination resistance, R_d, specified by the clause that invokes this method. The referece pulse time-domain reflection (PTDR) response is computed from the referece reflection coefficient at TP0v using Equation (93A-58) and Equation (93A-59). The reference ERL value is determined from the reference PTDR response using the method in 93A.5.2 with T_fx set to 0 and other parameters specified by the clause that invokes this method."

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Implementation:

163A.3.1.2 Effective return loss reference value

Effective return loss (ERL) is defined in 93A.5. The ERL reference value is determined as follows. Obtain the pulse time-domain reflection (PTDR) response from $S^{(0)}$ using Equation (93A-58) and Equation (93A-59). Determine the ERL reference value from the PTDR response using the method in 93A.5.2.

The reference reflection coefficient at TP0v is given by Equation (93A-7) where $s_{22}^{(x)}$ is Γ_1 as defined by Equation (93A-17) and $s_{ii}^{(y)}$ are the components of the scattering matrix of the virtual reference channel S⁽⁰⁾. In Equation (93A-17), the single-ended reference resistance R_0 is set to 50 Ohms and the single-ended termination resistance, Rd specified by the clause that invokes this method. The reference pulse time-domain reflection (PTDR) response is computed from the reference reflection coefficient at TP0v using Equation (93A–58) and Equation (93A–59). The reference ERL value is determined from the reference PTDR response using the method in 93A.5.2 with $T_{\overline{Tx}}$ set to 0 and other parameters specified by the clause that invokes this method.

TP0v method

C/ 163A SC 163A.3.2.2

P 283

L 12



Ran, Adee

Comment Type E Comm

Comment Status D

Intel

TP0v method

Both ERL(ref) and ERL(meas) in equation 163A-6 are undefined terms.

SuggestedRemedy

Add below the equation

"Where

ERL(ref) is the ERL reference value defined in 163A.3.1.2 ERL(meas) is the measured Effective return loss"

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Implement the suggested remedy with editorial license.

Implementation:

163A.3.2.2 Effective return loss		5
Measure the effective return loss using the method defined in $93.4.5$		6
Measure the effective return loss using the method defined in 95A.5.		8
The difference between the measured and reference ERL, dERL, is calculated using Equation (163A-6).		
$dERL = ERL^{(meas)} - ERL^{(ref)}$	(163A–6)	10 11 12

where $ERL^{(ref)}$ is the ERL reference value defined in 163A.3.1.2 $ERL^{(meas)}$ is the measured effective return loss

1