D2.2 Comment

Annex 162 (CA), 162A/B/C/D

| Clause | Topic | Comments |
|------------|-----------------------|---|
| 162 | CA RLcc | 89(R) |
| 162A | Host PCB ILdd | 18, 19 |
| 162B | MTF ILdc/ILdc | 138 |
| 162B | MTF RLcc | 136 |
| 162C | MDI pins table | 157 |
| 162D | CA types | 140 |
| 1/162/162D | MDI labels/references | 156, 158, 151, 153, 152, 154, 155, 161, 162 |

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Comments #89, 18, 19,

8023ck_D2p1_final_closedcomments.pdf

CI 162 SC 162.11.6 P 181 L 38 # 79

Dudek, Mike Marvell

Comment Type T Comment Status R

As was pointed out in the unsatisfied comment # 177 against draft 2.0 th

As was pointed out in the unsatisfied comment # 177 against draft 2.0 the existing specification for common mode return loss limit effectively doesn't exist once the test fixture loss exceeds 0.9dB. The rejection however had a valid point that there is a potential issue up to 4GHz where the loss is low.

SuggestedRemedy

Change the limit to 1.8dB from 0 to 4GHz, 2.2-0.1*f from 4GHz to 40GHz.

Response Status C

REJECT.

The commenter provided the following update to the suggested remedy.

1.8 0.5</= f(GHz) </= 4 GHz 1.4+0.1*f 4< f(GHz) </= 30 GHz

The revised specification may result in currently posted channels failing.

The comment and updated suggested remedy does not provide sufficient justification to support the change to the draft.

Further analysis and a consensus proposal is required.

C/ 162A SC 162A.4 P 287 L 45 # 18

Wu, Mau-Lin MediaTek Inc.

TR

The recommended maximum IL for TX or RX PCB is 6.875 dB at 26.56 GHz, which is defined in (162A-1). However, the equation of (162A-1) is not correct. By quick check of the equation, ILdd PCBmax(26.56) ~= 6.6 dB, which is NOT 6.875 dB. According to the closed

response of comment #18 in https://www.ieee802.org/3/ck/comments/draft1p3/8023ck_D1p3_final_closedcomments.pdf, the equation of (162A-1) shall be modified as

"0.9809*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))" . However, the equation of

Comment Status D

"0.9809*(0.417*SQRT(f)+0.1194*f+0.002*(f^2))" was adopted, instead, which is wrong.

SuggestedRemedy

Comment Type

Change (162A-1) from "0.9809*(0.417*SQRT(f)+0.1194*f+0.002*(f^2))" to "0.9809*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))". Redraw Figure 162A-1 accordingly if necessary.

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Change (162A-1) from "0.9809*(0.417*SQRT(f)+0.1194*f+0.002*(f^2))"

to "0.9809*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))".

Figure 162A-1 uses correct equation.

CI 162 SC 162.11.6 P 189 L 38

Dawe, Piers Nvidia

Comment Type TR Comment Status D

CA RLcc

As in previous comments: this common mode return loss spec RLcc becomes useless at the frequency when the MCB loss is 1.8/2 dB, which is only 8.5 GHz. We need a common mode return loss spec to stop large common-mode voltages building up through multiple low-loss reflections. The revised proposed remedy for D2.1 comment 79 seems OK: 1.8 dB 0.5<= f <= 4 GHz, 1.4+0.1*f dB 4< f <= 30 GHz. The 30 GHz fmax allows margin for real-world coax-PCB transitions (although the mated compliance boards are specified >= 3 dB to 50 GHz); the cable itself should pass this comfortably because it is insulated from the test by the MCB loss.

SuggestedRemedy

CA RLcc

Host PCB ILdd

Use a frequency-dependent mask 1.8 dB $0.5 \le f \le 4$ GHz, $1.4 + 0.1 \le f$ dB $4 \le f \le 30$ GHz. f is in GHz. Similarly for Tx, Table 162-11, 162.9.3.6.

Proposed Response Response Status W

PROPOSED REJECT.

This comment is a restatement of D2.1 comment #79.

The suggested remedy does not provide sufficient additional justification to support the change to the draft.

 CI 162A
 SC 162A.4
 P 289
 L 1
 # 19

 Wu, Mau-Lin
 MediaTek Inc.

 Comment Type
 TR
 Comment Status
 D
 Host PCB ILdd

The recommended maximum IL from TP0 to TP2 is 10.975 dB at 26.56 GHz, which is defined in (162A-3). However, the equation of (162A-3) is not correct. By quick check of the equation, ILdd_HostMax(26.56) \sim 10.54 dB, which is NOT 10.975 dB. According to the closed response of comment #19 in

https://www.ieee802.org/3/ck/comments/draff1p3/8023ck_D1p3_final_closedcomments.pdf, the equation of (162A-3) shall be modified as

"1.5658*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))" . However, the equation of

"1.5658*(0.417*SQRT(f)+0.1194*f+0.002*(f^2))" was adopted, instead, which is wrong.

SuggestedRemedy

Change (162A-3) from "1.5658*(0.417*SQRT(f)+0.1194*f+0.002*(f^2))" to "1.5658*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))". Redraw Figure 162A-2 accordingly if necessary.

Proposed Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

Change (162A-3)

from "1.5658*(0.417*SQRT(f)+0.1194*f+0.002*(f^2))"

to "1.5658*(0.471*SQRT(f)+0.1194*f+0.002*(f^2))".

Figure 162A-2 uses correct equation.

Comment #138 - Mated Test Fixture

If common-mode to differential-mode insertion loss is what we want to control, that's ILdc. However, we want to control both ILdc and Ilcd, as we have both RLcd and RLdc specs in 120G. There is an argument that they are the related, and specifying one is enough, but I'm not sure it always holds.

SuggestedRemedy

Specify both ILcd and ILdc. It may be possible to specify one in one direction and the other in the other: Scd21 and Scd12, or Sdc21 and Scd12, where 1 is an input (instrument connector that would be connected to a pattern generator) and 2 is an output. I haven't thought through which we need, or maybe we need all four. It is simpler to require all four.

Proposed Response Response Status W

PROPOSED ACCEPT IN PRINCIPLE.

This comment does not apply to the substantive changes between IEEE P802.3ck D2.2 and D2.1 or the unsatisfied negative comments from previous drafts. Hence it is not within the scope of the recirculation ballot.

However, the proposed change is an improvement to the draft.

As pointed out by the comment both Ilcd and Ildc of the MTF must be similarly constrained. Since ILcd12 and ILdc21 are reciprocal and ILdc21 and ILdc12 reciprocal, the insertion loss mode conversion can be constrained by measuring either Ilcd (or Ildc) in both directions. The text as written was intended to require this but the wording could be improved

Also, the variable "IIcd" should be "IIdc" to correctly reflect the subclause title and text.

Change: "measured at either test fixture test interface"

To "measured in both directions"

and

Change variable name "Ilcd" to "Ildc".

162B.1.3.3 Mated test fixtures common-mode to differential-mode insertion loss

The common-mode to differential-mode insertion loss of the mated test fixtures measured at either test fixture test interface shall meet the values determined using Equation (162B-6).

$$ILcd(f) \ge \begin{cases} 30 & (21/28)f & 0.01 \le f < 20 \\ 15 & 20 \le f \le 50 \end{cases}$$
 (162B-6)

Error ILcd should be ILdc

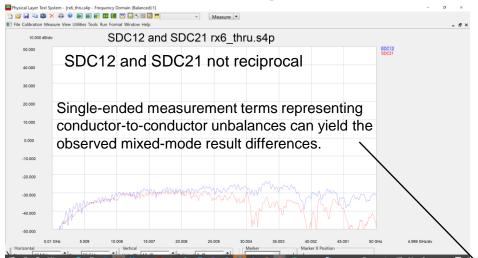
where

ILcd(f) is the common-mode to differential-mode insertion loss in dB at frequency f is the frequency in GHz

 As these are test fixture specifications, SDC12, SDC21,SCD12, and SCD21 should be specified

MTF measurements

https://www.ieee802.org/3/ck/public/tools/cucable/kocsis_3ck_02_0719_MTFosfp.zip







Source: Curtis Donahue, Rhodes and Swartz
$$Sdc_{21} = \frac{S_{31} + S_{32} - S_{41} - S_{42}}{2} \quad Sdc_{12} = \frac{S_{13} + S_{14} - S_{23} - S_{24}}{2}$$

$$\frac{S_{31} + S_{32} - S_{41} - S_{42}}{2} = \frac{S_{13} + S_{14} - S_{23} - S_{24}}{2}$$

$$S_{32} - S_{41} = S_{14} - S_{23}$$

$$S_{32} + S_{23} = S_{14} + S_{41}$$

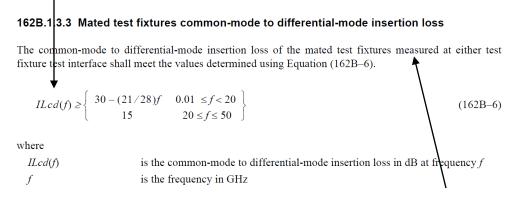
$$2 \times S_{32} = 2 \times S_{14}$$

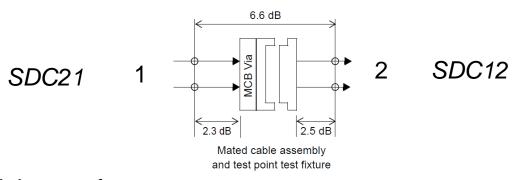
$$S_{32} = S_{14}$$

Need a minimum of two measurements SDC12 and SDC21 SCD12 and SCD21 SDC12 and SCD12 SDC21 and SDC21

Comment #138 - Mated Test Fixture

- Minimal changes to the draft
 - Correcting ILcd to align with subclause description
 - Change "the mated test fixture measured at either test interface" to "the mated test fixture measured in both directions"





Need a minimum of two measurements SDC12 and SDC21

Comments #136,157, 140

C/ 162B

SC 162B.1.3.4

P 298

Just as for the cable RLcc spec: this 3 dB becomes useless when the MCB trace loss is

L 30

SC 162C.1 C/ 162C

Ghiasi, Ali

Comment Type

P 306

L 10

Ghiasi Quantum/Inphi

157

MDI pins table

Dawe, Piers

Nvidia

Comment Type TR Comment Status D

MTF RLcc

136

Per unsatisfied comment from D2.2.

TR

Table 162C-3 needs to be better organized

SuggestedRemedy

An improved and beter organized table will be submited as ghiasi 3ck 01 0921.pdf

Proposed Response

Response Status W

Comment Status D

PROPOSED REJECT.

The following related presentation was provided for consideration: https://www.ieee802.org/3/ck/public/21 09/ghiasi 3ck 01 0921.pdf

For task force discussion of cited presentation.

SuggestedRemedy

As for the cable RLcc spec but 1 dB lower to 30 GHz, easing up to 50 GHz; 12 -9f dB 0.01 <= f <1, 3 dB 0.5<= f <= 4 GHz, 2.6+0.1*f dB 4< f <= 30 GHz, 9.5-1.3*f dB 30< f <= 50 GHz f is in GHz

Proposed Response

Response Status W

PROPOSED REJECT.

half of 3 = 1.5 dB (16 GHz).

The comment and suggested remedy does not provide sufficient information or justification to support a change to the draft.

C/ 162D SC 162D.1.1

P 317 Nvidia

L 6

140

Dawe, Piers

Comment Type

Comment Status D

CA types

In table headers:

"supportable PMDs

Number"

SuggestedRemedy

Change to: Maximum number of PMDs (merge two cells vertically). Similarly in the following tables.

If changing to "maximum", change "supportable" to "maximum" in the text and table captions too, and in 162C.1.

Proposed Response

Response Status W

PROPOSED REJECT.

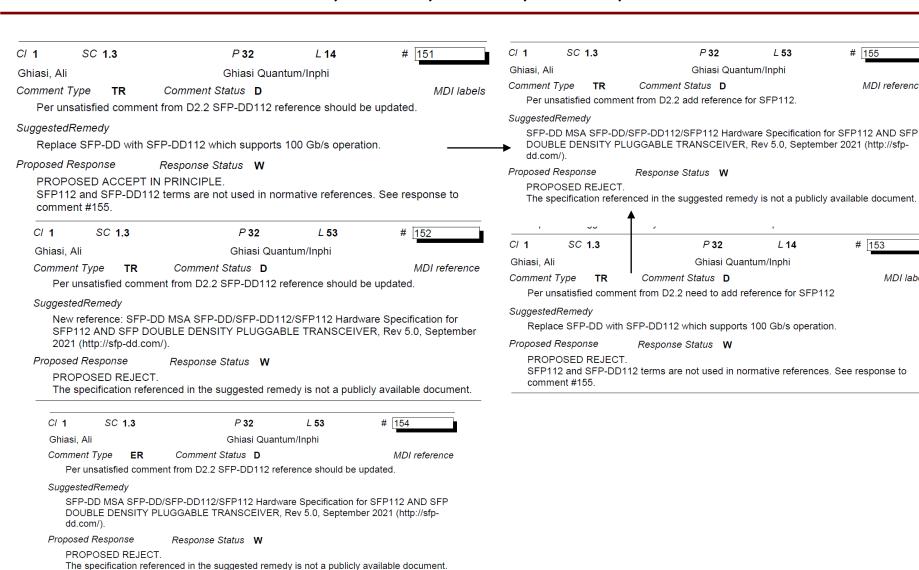
This comment does not apply to the substantive changes between IEEE P802.3ck D2.2 and D2.1 or the unsatisfied negative comments from previous drafts. Hence it is not within the scope of the recirculation ballot.

The suggested change is not necessary.

Table 162D-2—100GBASE-CR1 cable assembly types and supportable number of PMDs

| one end | | other end | | supportable PMDs |
|-----------------|--------|-----------------|--------|------------------|
| Receptacle/Plug | Number | Receptacle/Plug | Number | Number |
| SFP+ | 1 | SFP+ | 1 | 1 |
| SFP-DD | 1 | SFP+ | 2 | 2 |
| DSFP | 1 | SFP+ | 2 | 2 |
| QSFP+ | 1 | SFP+ | 4 | 4 |
| QSFP-DD800 | 1 | SFP+ | 8 | 8 |
| OSFP | 1 | SFP+ | 8 | 8 |
| SFP-DD | 1 | SFP-DD | 1 | 2 |
| DSFP | 1 | DSFP | 1 | 2 |
| QSFP+ | 1 | QSFP+ | 1 | 4 |
| QSFP-DD800 | 1 | QSFP-DD800 | 1 | 8 |
| OSFP | 1 | OSFP | 1 | 8 |

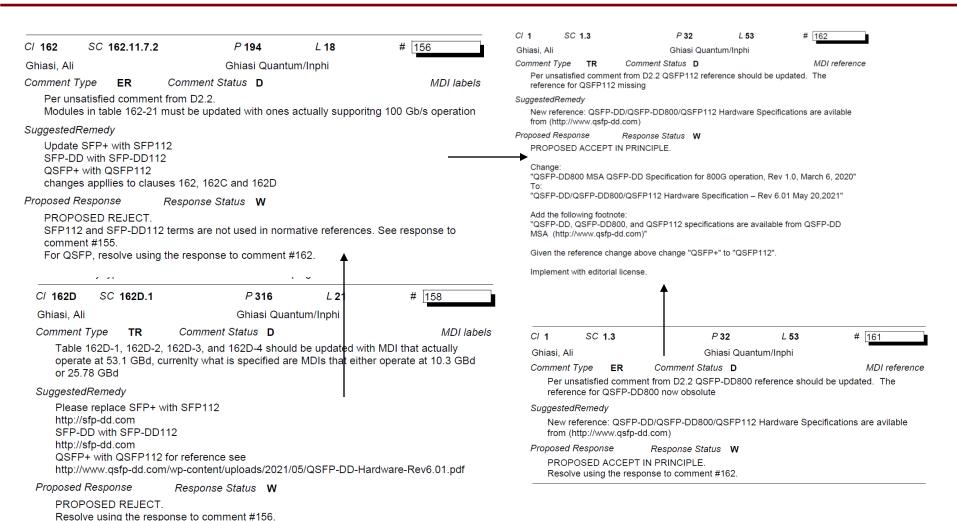
Comments 151, 152, 153, 154, 155



MDI reference

MDI labels

Comments 156, 158, 161,162



Comments #136

C/ 162B

SC 162B.1.3.4

P 298

L 30

136

Dawe, Piers Comment Type

Nvidia

MTF RLcc

Just as for the cable RLcc spec: this 3 dB becomes useless when the MCB trace loss is half of $3 = 1.5 \, dB \, (16 \, GHz)$.

SuggestedRemedy

As for the cable RLcc spec but 1 dB lower to 30 GHz, easing up to 50 GHz: 12 -9f dB 0.01 <= f <1, 3 dB 0.5<= f <= 4 GHz, 2.6+0.1*f dB 4< f <= 30 GHz, 9.5-1.3*f dB 30< f <= 50 GHz. f is in GHz.

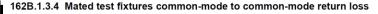
Proposed Response

Response Status W

Comment Status D

PROPOSED REJECT.

The comment and suggested remedy does not provide sufficient information or justification to support a change to the draft.



The common-mode to common-mode return loss of the mated test fixtures measured at each test fixture test interface shall meet the values determined using Equation (162B–7).

$$RLcc(f) \ge \begin{cases} 12 - 9f & 0.01 \le f < 1 \\ 3 & 1 \le f \le 50 \end{cases}$$
 (162B-7)

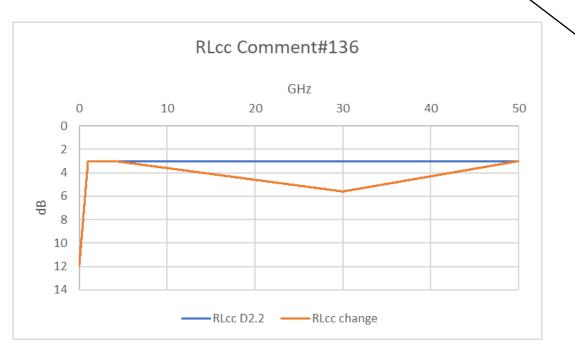
where

RLcc(f)

is the common-mode to common-mode return loss in dB at frequency f

is the frequency in GHz

The mated test fixtures common-mode to common-mode return loss is illustrated in Figure 162B-5.



12 -9f 3

0.01 <= f < 11<= f <4 GHz 2.6+0.1f $4 \le f \le 30 \text{ GHz}$ 9.5-0.13f 30<=f<=50 GHz