

Optical Link Model for PAM-4 Multimode Channels with equalizers

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Brett Lane**

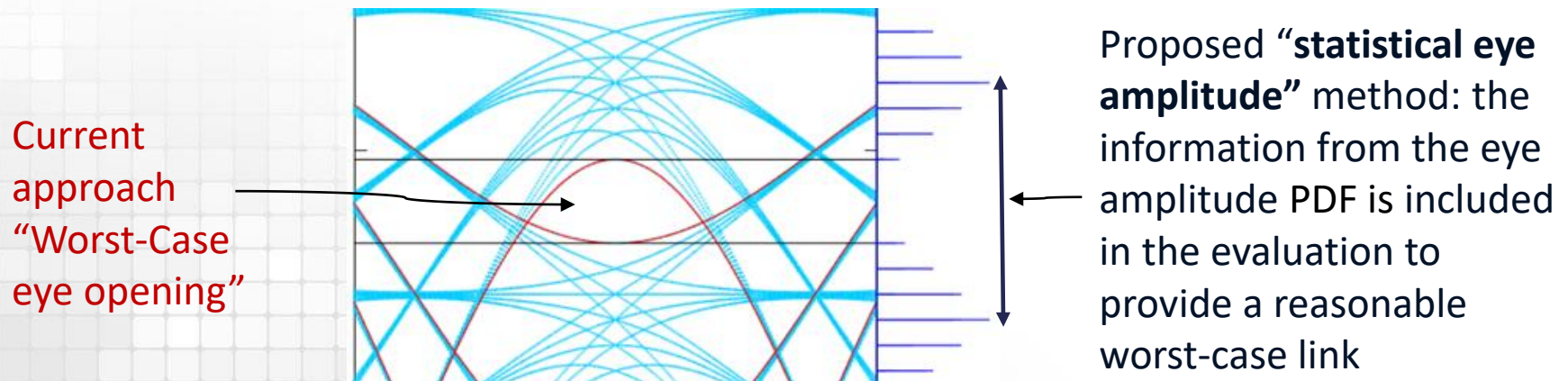
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Corporation

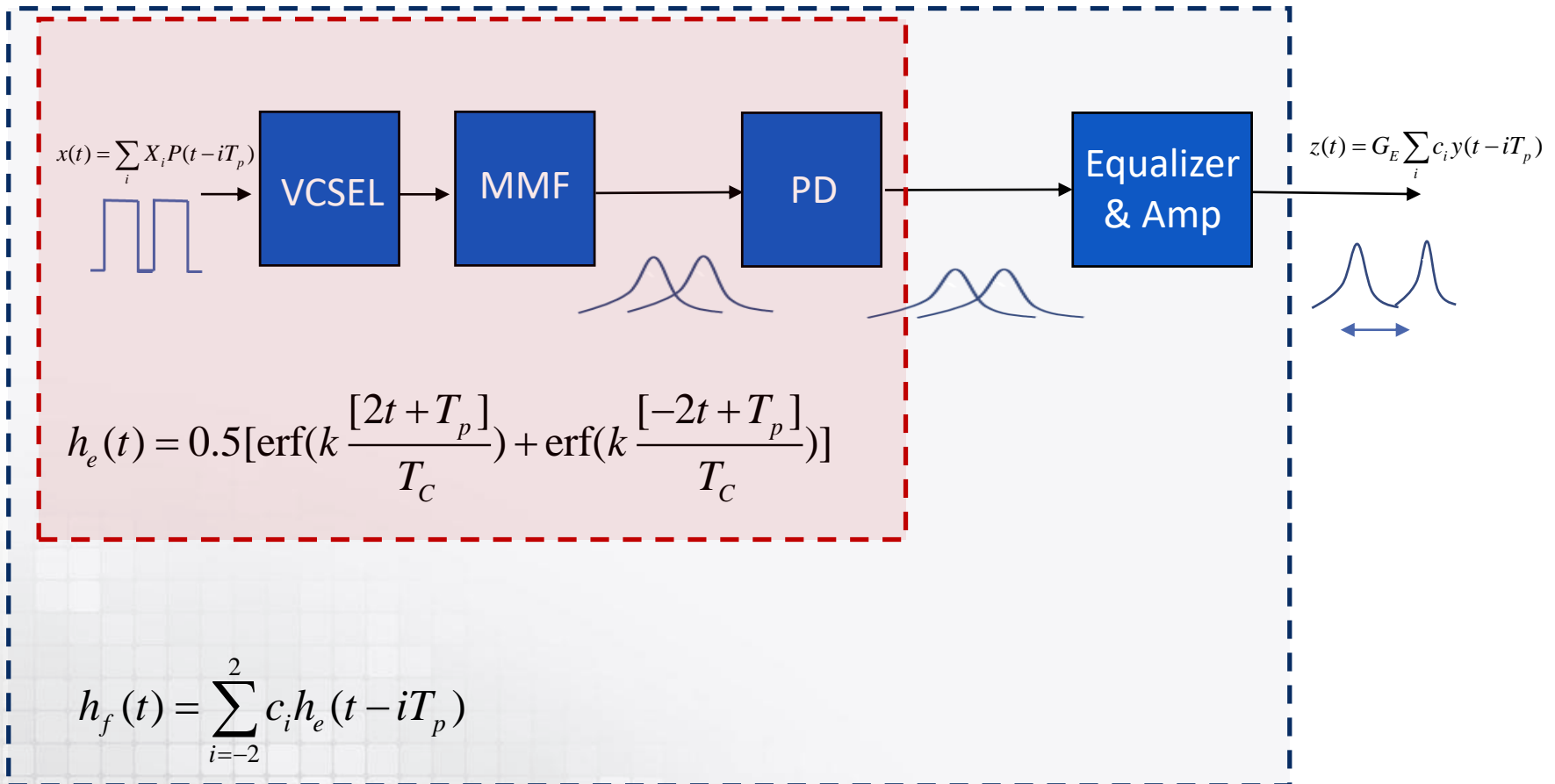
IEEE P802.3cm 400 Gb/s over Multimode Fiber Task Force
Bangkok, Thailand, November 2018

Introduction and Objectives

- Provide a link model tool to estimate reasonable worst-case channel reaches for multimode fiber links using VCSEL based transceivers and PAM-4 modulation
 - 50GBASE-SR, 100GBASE-SR2, 200GBASE-SR4, 400GBASE-SR8, 400GBASE-SR4.2, BiDi and others operating in the spectral window 840-953nm
- Previous link models compute penalties based on worst-case eye opening
 - Too pessimistic for equalized PAM-4 links
 - The statistical eye amplitude method (castro_3cm_01_0518) provides a fast and accurate estimation.
- This presentation describes the eye amplitude estimation method of all the penalties (ISI and noise penalties) in the link model.
- An implementation of the statistical eye amplitude link model in Matlab will be shown during the presentation.



Equalized Link model



Implementation

- Evaluated several options shown in Table.

Platform	Speed	Required License	Complexity	Size
Excel [®]	Very Slow	MS Office	Very High	Very small
Excel [®] with Visual Basic Application (VBA)	Slow	MS Office	Medium	Very small
Excel [®] with Dynamic time libraries	Fast	MS Office	High	Small
MATLAB[®] compiled	Fast	None	Medium	Large 500 Mbytes min

- Excel with simple VBA could be good for worst case eye closure but not for eye amplitude method.
- Latest version, presented here implemented in MATLAB (compiled)

Implementation

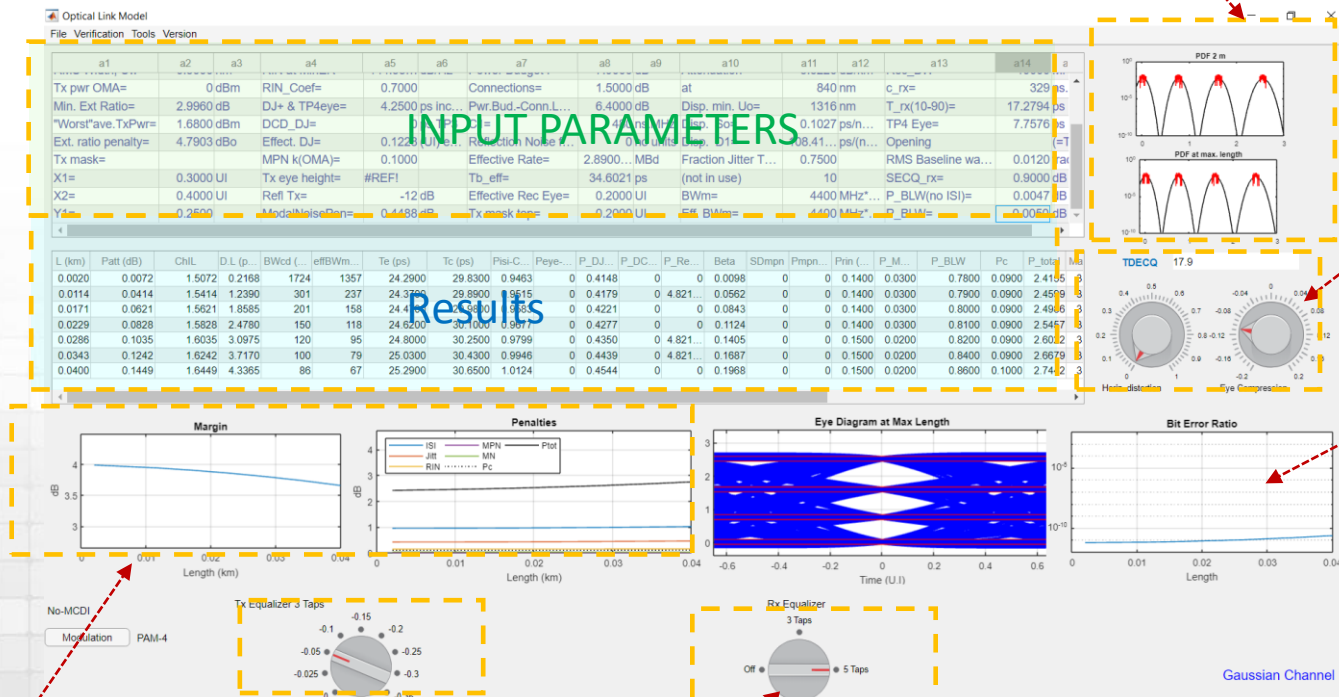
Spreadsheet approach

- Top menu for basic functions (save load,...)
- Section for input parameters
- Section for results
- Eye diagram (ISI-Jitter penalties)
- Histograms at 2 m and for the maximum reach
- Histograms at 2 m and for the maximum reach
- Controls for pre-emphasis, equalization, distortion

Eye Histograms

Eye compression knobs

BER vs length



Margin & penalties

Tx Equalizer knob

Equalizer knob

- Computation of link penalties for PAM-2 and PAM-4
- Transmitter equalizer only 3 taps (symmetric) with fixed options
- Receiver equalizer MMSE 3 or 5 Taps
 - Histograms computed at the center of the eye for 2 m and maximum reach
 - Show the histograms due to ISI-Jitter component (red trace) and also the noise components
 - Noise enhancement due equalizer included
- Eye compression knob only allow the range of values shown in dial
- Eye diagram (ISI-Jitter penalties only)
- Receiver equalizer MMSE 3 or 5 Taps
 - Noise enhancement due equalizer included

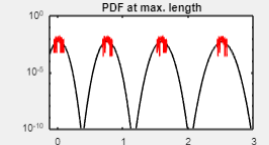
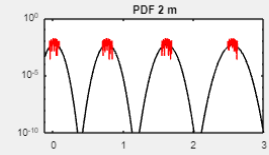
Implementation



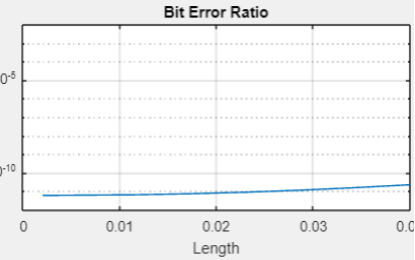
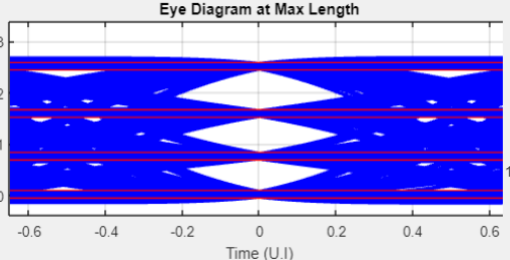
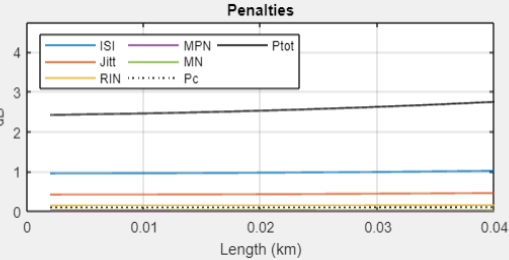
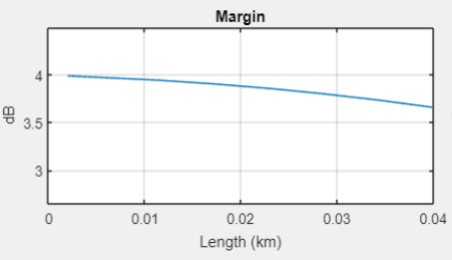
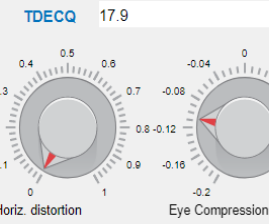
Real time demo shown during the presentation

File Verification Tools Version

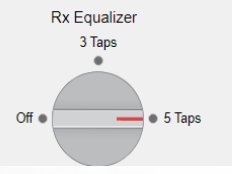
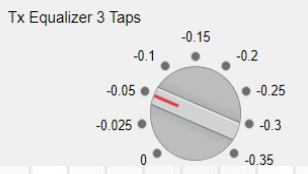
a1	a2	a3	a4	a5	a6	a7	a8	a9	a10	a11	a12	a13	a14
Tx pwr OMA=	0 dBm	RIN_Coef=	0.7000	Connections=	1.5000 dB	at	840 nm	c_rx=	329 ns.				
Min. Ext Ratio=	2.9960 dB	DJ+ & TP4eye=	4.2500 ps inc...	Pwr.Bud.-Conn.L...	6.4000 dB	Disp. min. Uo=	1316 nm	T_rx(10-90)=	17.2794 ps				
"Worst"ave.TxPwr=	1.6800 dBm	DCD_DJ=	0 ps TP3	C1=	480 ns.MHz	Disp. So=	0.1027 ps/n...	TP4 Eye=	7.7576 ps				
Ext. ratio penalty=	4.7903 dBo	Effect. DJ=	0.1228 (UI) e...	Reflection Noise f...	0 no units	Disp. D1=	-108.41...ps/(n...	Opening	(=T				
Tx mask=		MPN k(OMA)=	0.1000	Effective Rate=	2.8900... MBd	Fraction Jitter T...	0.7500	RMS Baseline wa...	0.0120 frac				
X1=	0.3000 UI	Tx eye height=	#REF!	Tb_eff=	34.6021 ps	(not in use)	10	SECQ_rx=	0.9000 dB				
X2=	0.4000 UI	RefI Tx=	-12 dB	Effective Rec Eye=	0.2000 UI	BWm=	4400 MHz*...	P_BLW(no ISI)=	0.0047 dB				
Y1=	0.2500	ModalNoisePen=	0.4488 dB	Tx mask top=	0.2000 UI	Eff. BWm=	4400 MHz*...	P_BLW=	0.0050 dB				



L (km)	Patt (dB)	ChL	D.L (p...	BWcd (...	effBwM...	Te (ps)	Tc (ps)	Pisi-C...	Peye...	P_DJ...	P_DC...	P_Re...	Beta	SDmpn	Pmpn...	Prin (...	P_M...	P_BLW	Pc	P_total	Ma
0.0020	0.0072	1.5072	0.2168	1724	1357	24.2900	29.8300	0.9463	0	0.4148	0	0	0.0098	0	0	0.1400	0.0300	0.7800	0.0900	2.4155	3
0.0114	0.0414	1.5414	1.2390	301	237	24.3700	29.8900	0.9515	0	0.4179	0	4.821...	0.0562	0	0	0.1400	0.0300	0.7900	0.0900	2.4599	3
0.0171	0.0621	1.5621	1.8585	201	158	24.4700	29.9800	0.9583	0	0.4221	0	0	0.0843	0	0	0.1400	0.0300	0.8000	0.0900	2.4986	3
0.0229	0.0828	1.5828	2.4780	150	118	24.6200	30.1000	0.9677	0	0.4277	0	0	0.1124	0	0	0.1400	0.0300	0.8100	0.0900	2.5457	3
0.0286	0.1035	1.6035	3.0975	120	95	24.8000	30.2500	0.9799	0	0.4350	0	4.821...	0.1405	0	0	0.1500	0.0200	0.8200	0.0900	2.6022	3
0.0343	0.1242	1.6242	3.7170	100	79	25.0300	30.4300	0.9946	0	0.4439	0	4.821...	0.1687	0	0	0.1500	0.0200	0.8400	0.0900	2.6679	3
0.0400	0.1449	1.6449	4.3365	86	67	25.2900	30.6500	1.0124	0	0.4544	0	0	0.1968	0	0	0.1500	0.0200	0.8600	0.1000	2.7442	3



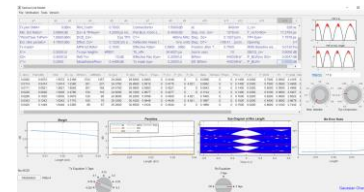
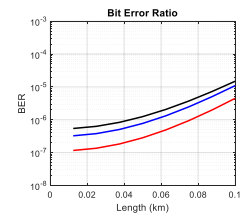
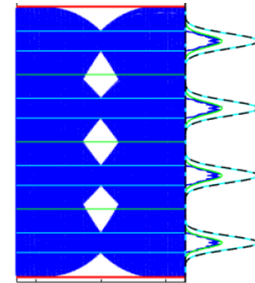
No-MCDI Modulation PAM-4



Gaussian Channel

Summary & Conclusions

- We described Panduit’s link model for PAM-4 signals over multimode fiber
 - Statistical eye amplitude method
- A general description of the functionalities and a demonstration shown during the presentation
 - Plot of histograms, eye diagrams and BER
 - Tested response time for any change in input parameters
- Model details of the model included in annexes:
 - Fast & accurate method to compute the eye diagram histograms
 - Signal dependent noise treatment
 - Computation Method for Margin and Penalties
- The model was implemented in Matlab GUI (compiled)
 - GUI implemented
 - Compiles, (no license required by user)
 - Modular
 - Penalties (currently being reviewed such as MN) could be updated
 - Could be available in IEEE website if solicited.



References

- Previous work for 1Gbps and 10Gbps using NRZ link models
 - Del Hanson, David Cunningham, Piers Dawe and David Dolfi (for 10G)
- Prior works for equalized channels :
 - D. Cunningham proposed a 3-tap equalizer for PI-6 (12-044v1, 12-123v0)
 - However, required several sheets (one per link length) and valid only for NRZ
 - PAM-4 power budget penalties require more sophisticated equations than NRZ
 - Equalization taps need to be efficiently computed for each length in one sheet
- In Fibre Channel, PAM-4 has been modeled using additional software packages
 - For Python languages 16-013 v0, 16-012v0 (Richard Johnson)
 - For Matlab 15-263v0
 - An Excel VBA was proposed in T11-2016-065v0
 - Fully implemented PI-6P (32GFC NRZ)
- Investigation of 60 Gb/s 4-PAM Using an 850 nm VCSEL and Multimode Fiber
 - Journal of Lightwave Tech. Vol 34 (16) , April 2016
- Optical Link Model for PAM-4
 - castro_3cm_01_0518

Backup

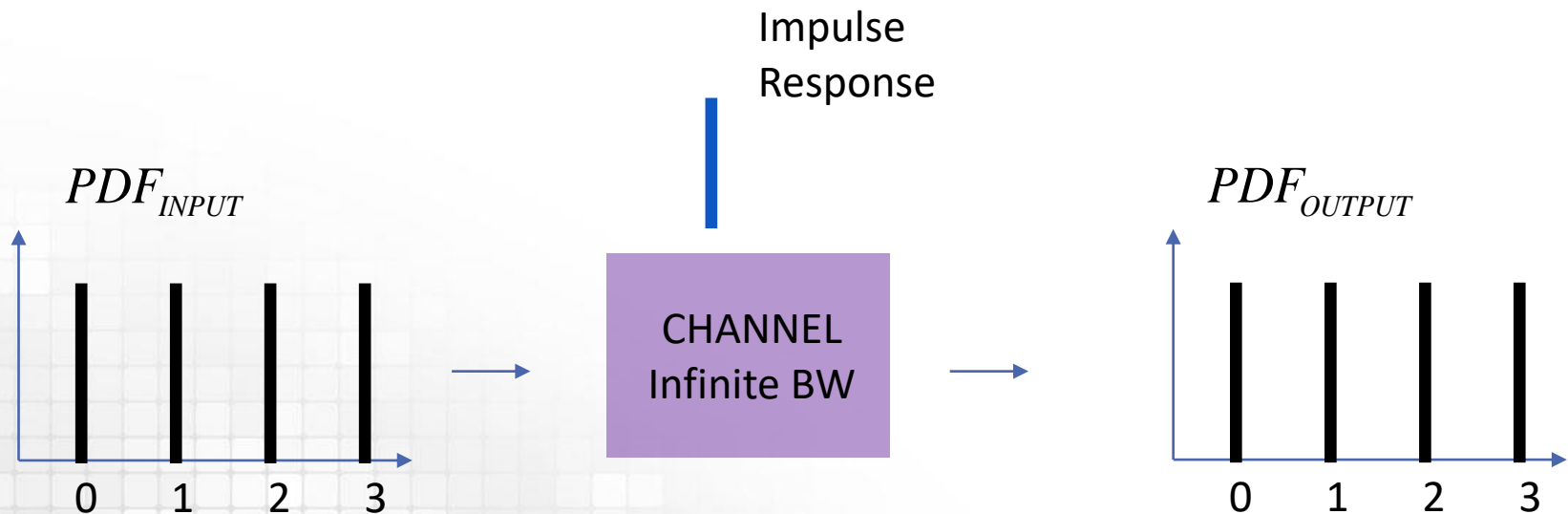
Annex I

**Direct Method to compute the Eye PDF from the input (ideal) PDFs
and from the channel response**

- The method shown in this annex provides an very accurate and fast computation of the eye diagram amplitude histogram.
 - It only needs the input distribution, i.e. for PAM-4 4 delta functions with 25% probability each, and the impulse response of the channel.
- It can include the deterministic jitter of the channel
- The proposed method provides a general solution that does not need the simulation of the channel (sending billion of symbols) . Therefore, is significantly faster and used in some parts of the presented link models.
- Examples, and more details of the operation in shown in next slides.

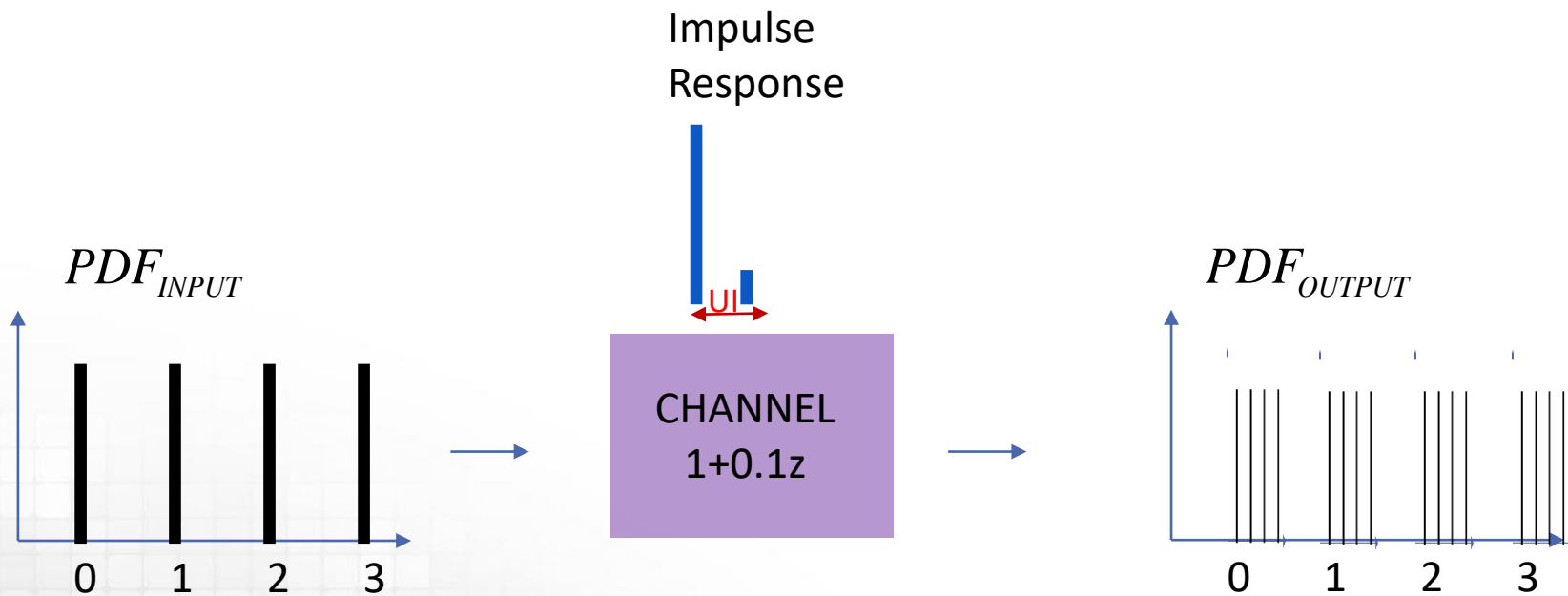
Eye Diagram Statistics

- For a time-invariant channel the PDF of the eye at a specific sampling time can be obtained using the statistical properties of the transmitted data (PDF) and the impulse response of the channel.
 - The resultant PDF using this method is equivalent of sending a pseudo random sequence of “infinite length”
- A very simple example to illustrate this method is shown in the following 3 steps
 1. *A PAM-4 signal in a channel with infinite bandwidth*



Eye Diagram Statistics

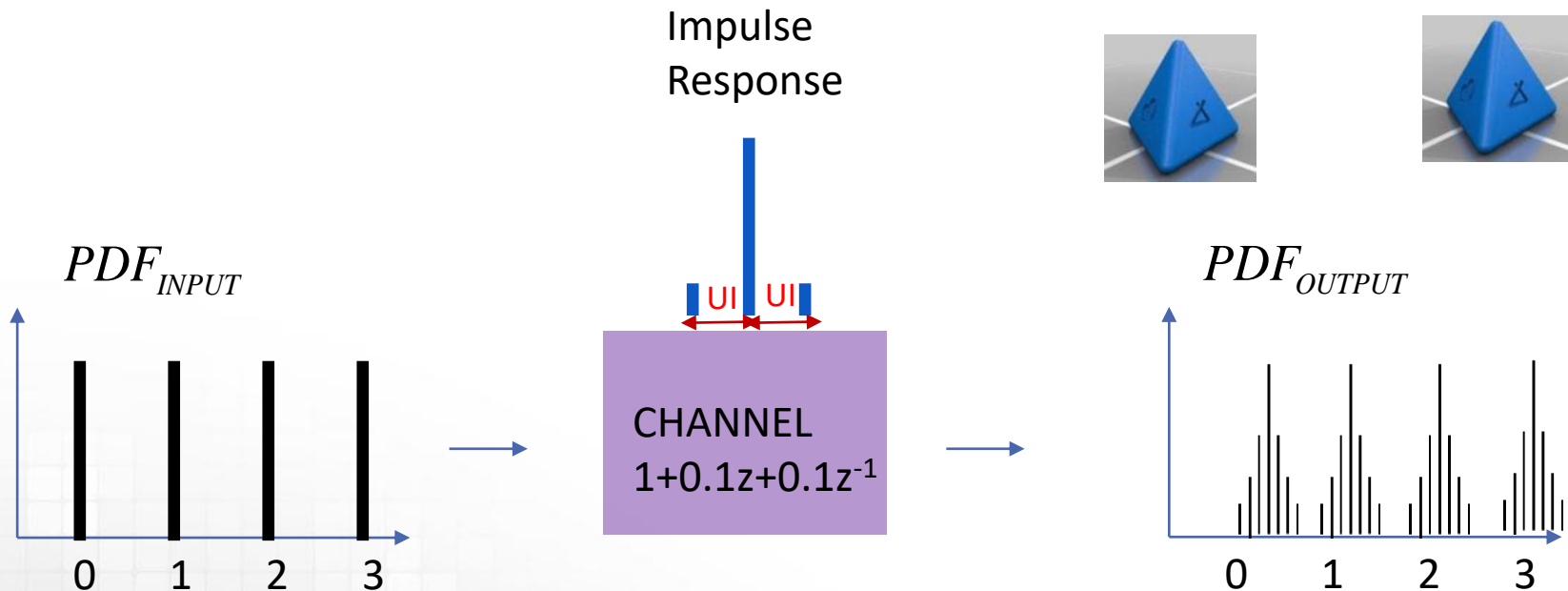
1. A PAM-4 signal in a channel with infinite bandwidth (previous slide)
2. A PAM-4 signal with a channel with response $1+0.1z$



The input PFD is modified by the adjacent pulse that add 0, 0.1, 0.2 or 0.3 each 25% of the time.

Eye Diagram Statistics

- A very simple example to illustrate the method is shown
 1. A PAM-4 signal in a channel with infinite bandwidth
 2. A PAM-4 signal with a channel with response $1+0.1z$
 3. A PAM-4 signal with a channel with response $1+0.1(z+z^{-1})$



- The input PFD is modified by the adjacent pulse to the left that adds 0, 0.1, 0.2 or 0.3 each 25% of the time and by the adjacent pulse to the right that adds 0, 0.1, 0.2 or 0.3 each 25% of the time.
- What is the final PDF?
 - The modification to the PDF can be obtained by convolving the effects from the left and right side. In some way, equivalent to launching two four-sided dice (tetrahedral die) each face marked with 0,0.1,0.2,0.3.

Eye Diagram Statistics

- **The received optical signal is given by,**

$$y(kT_p) = Y_k = \sum_i X_i h_e([k-i]T_p + J T_p) = h_0 X_k + \sum_{i>k} X_i h_{i-k} + \sum_{i<k} X_i h_{-(k-i)}$$

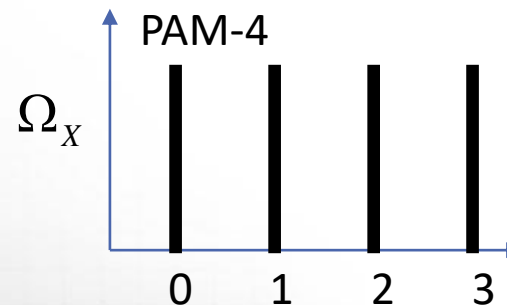
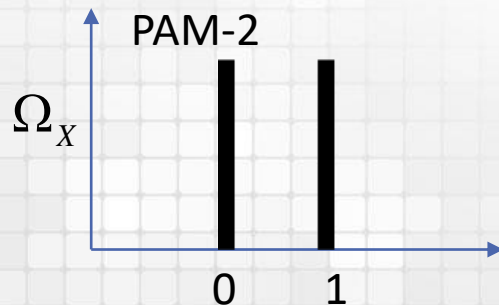
where J is the effective jitter

- **The Probability Density function (PDF) of Y can be obtained using**

$$PDF_{OUTPUT}(Y_k) = PDF(h_0 X_k + \sum_{i>k} X_i h_{i-k} + \sum_{i<k} X_i h_{k-i})$$

- **We can define the PDF of X as:** $\Omega_X = PDF_{INPUT}(X)$

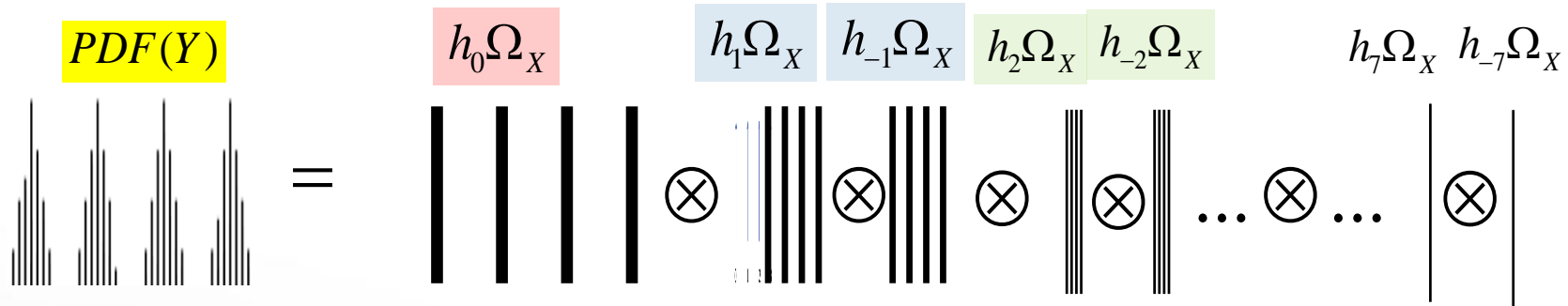
- **Assuming, equiprobable symbols, the PDF for PAM-2 and PAM-4 are shown below,**



Eye Diagram Statistics: General method

- The PDF of y can be obtained using:

$$PDF_{OUTPUT}(Y) = h_0\Omega_X \otimes h_1\Omega_X \otimes h_{-1}\Omega_X \otimes h_2\Omega_X \otimes h_{-2}\Omega_X \otimes h_3\Omega_X \otimes h_{-3}\Omega_X \otimes \dots \otimes h_7\Omega_X \otimes h_{-7}\Omega_X$$



Where \otimes represents the convolution operator

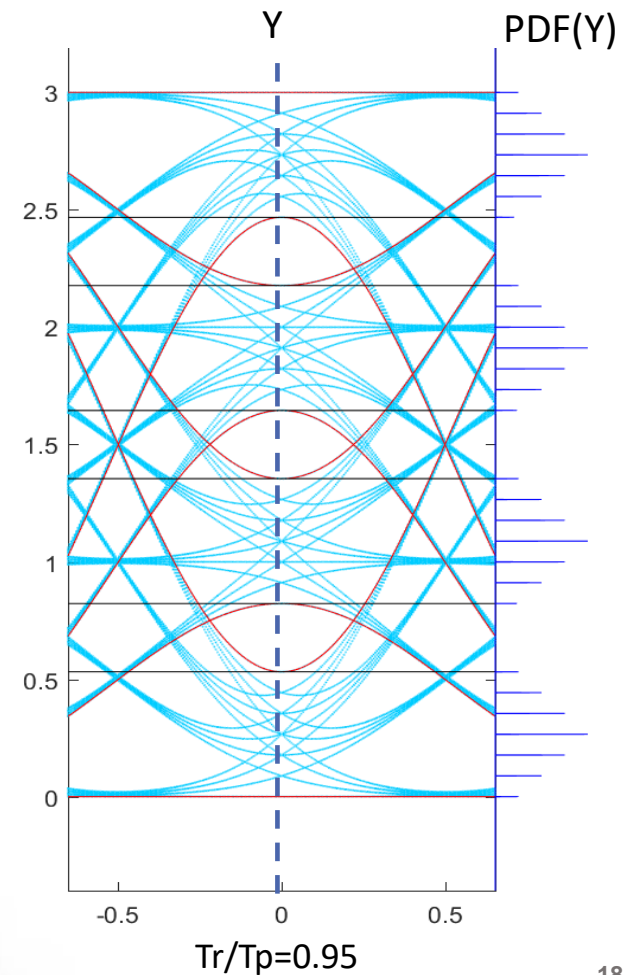
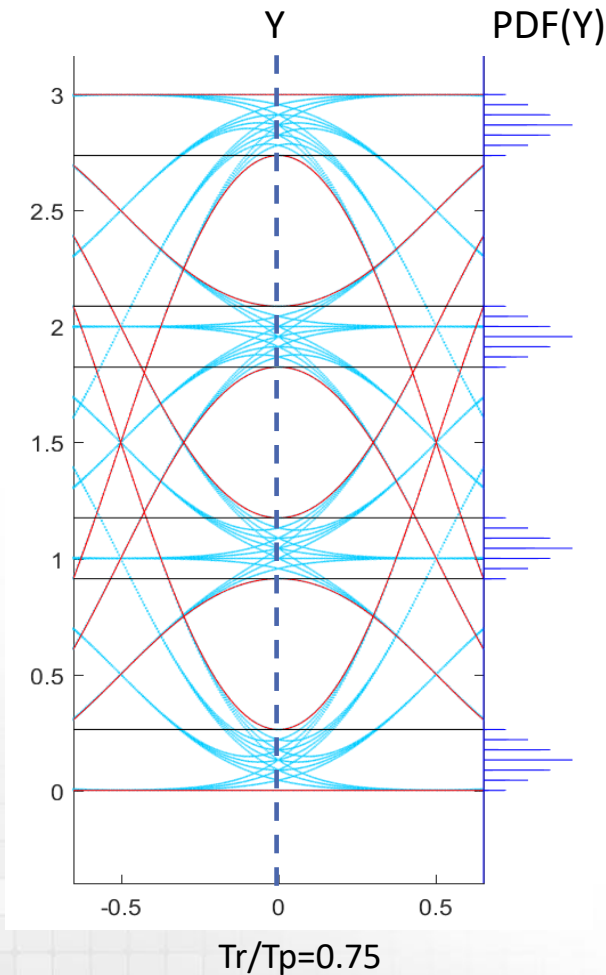
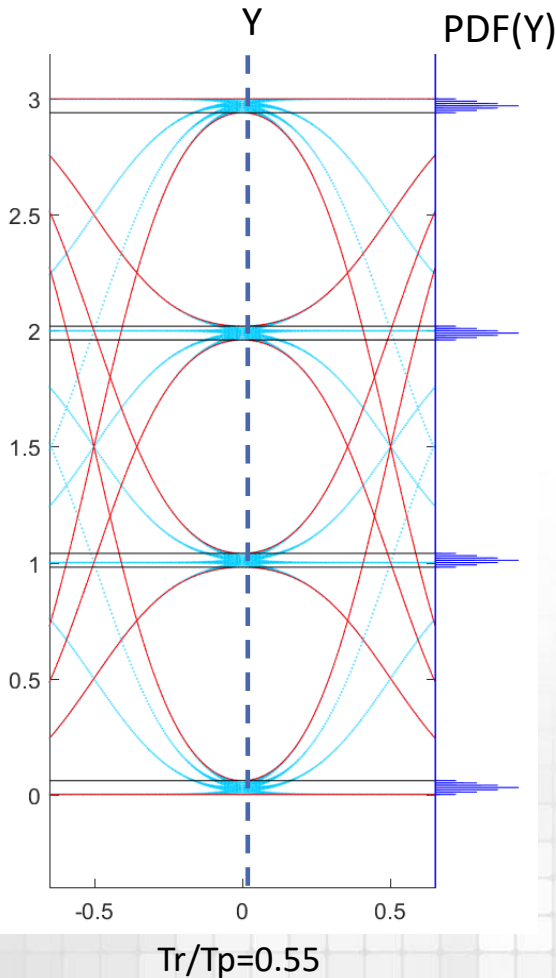
$$\Omega_X = PDF_{INPUT}(X)$$

and $h_0, h_1, h_{-1}, h_2, h_{-2}, \dots$ represents the impulse response of the channel sampled using the symbol period.

- The exact PDF of the eye diagram at a specific sampling time can be obtained without the need of sending a pseudorandom sequence, we just need to convolve scaled versions of the input signal PDF.
- The scaling factor is the value of the impulse response at $T, \pm T, \pm 2T$
- This method works also when dual-Dirac jitter is present.

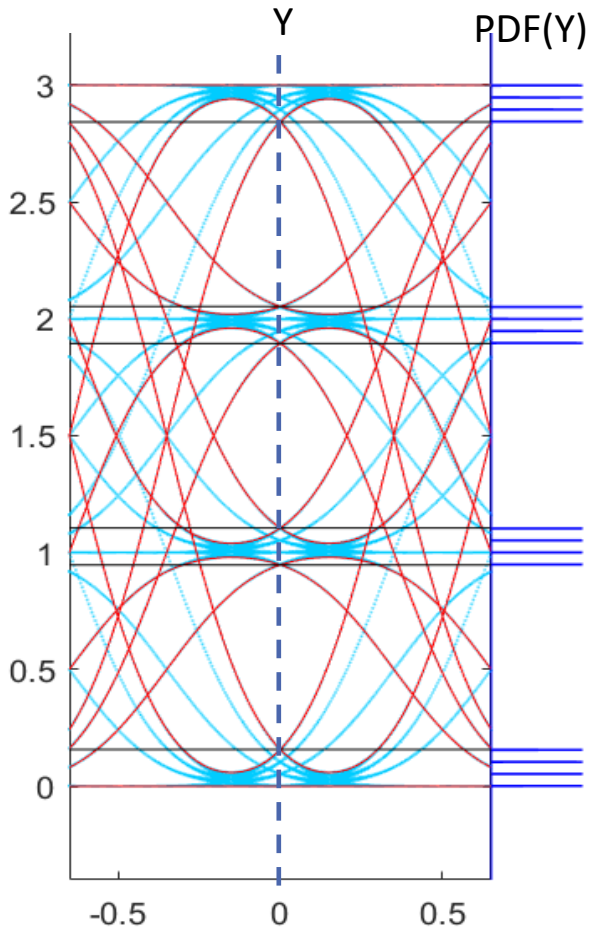
Examples Eye Diagram Statistics: No Jitter

- Using this method the PDFs for the received signal at the decision time can be computed as shown in the examples below.

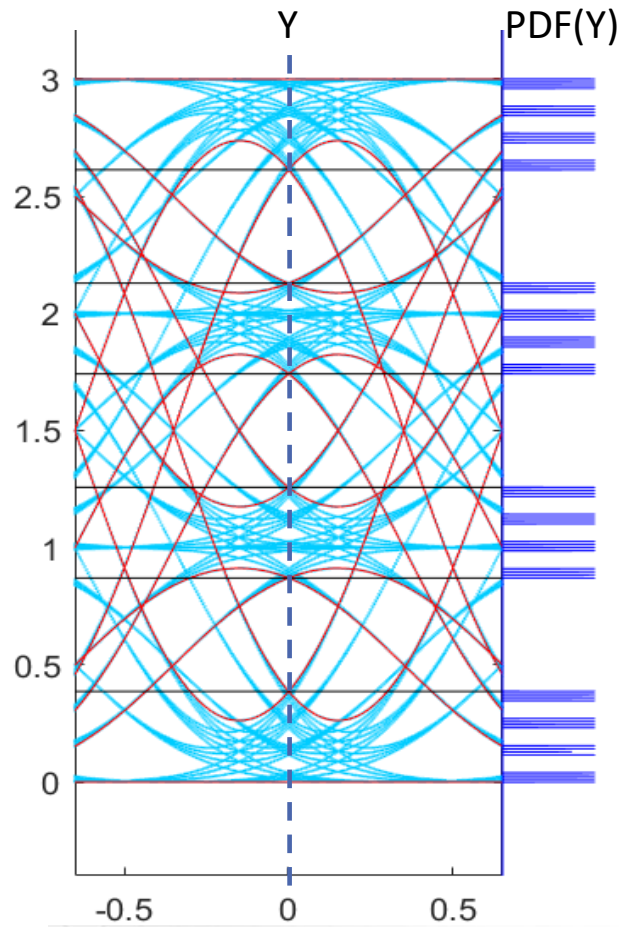


Example Eye Diagram Statistics: dual-Dirac Jitter

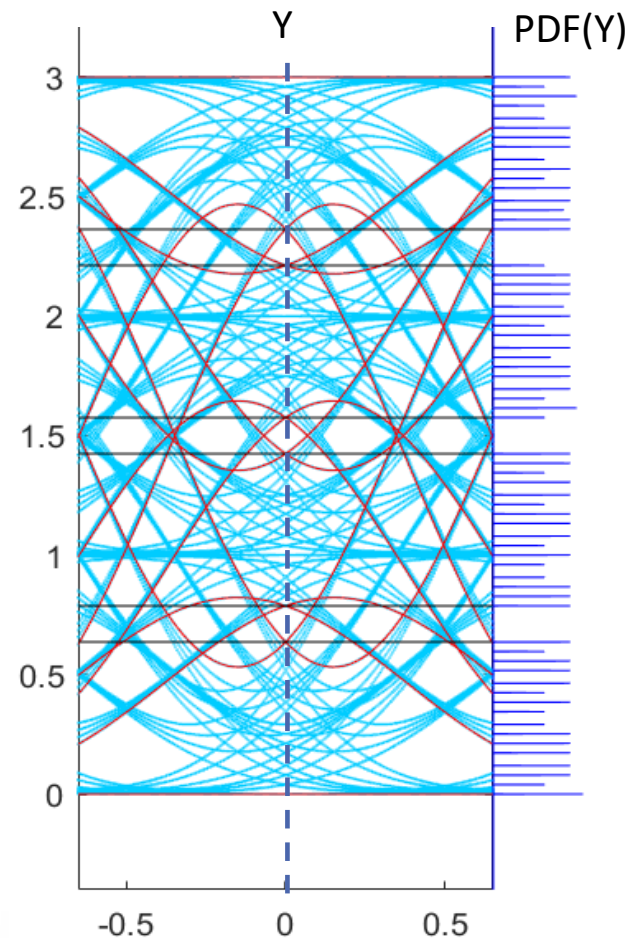
- Using this method the PDFs for the received signal at the decision time can be computed as shown in the examples below.



$T_r/T_p = 0.55$, effect. $J = 0.3$



$T_r/T_p = 0.75$, effect. $J = 0.3$



$T_r/T_p = 0.95$, effect. $J = 0.3$

Annex II
Treatment of signal dependent noises
example for RIN

Example of signal dependent noises RIN_{OMA}

- IEEE 802.3ae (clause 52.9.6) defines RIN_{OMA} as the ratio of the electrically noise power normalized to a 1 Hz bandwidth and the electrical power of a square wave modulation
- The RIN_{OMA} (outer) can be measured using a scope and a square wave pattern (i.e., 8 zeros and 8 threes as indicated in 802.3bs Table 139-9). The equations to relate the measured RIN parameters to our PAM-4 equalized optical link will be shown in this section.
 - The normalized variance due to RIN can be obtained using

$$\sigma_{RIN-OMA}^2 = \frac{n_0^2 + n_3^2}{2(\Delta/2)^2 \rho_{ISI-J}^2} = \frac{K_{RIN} 10^{-RIN/10} 10^6}{\sqrt{0.477 / BW_{RX}^2}} \quad (D.1)$$

- Where 3Δ is the optical modulation amplitude without any dispersion penalties, $K_{RIN} = 0.7$, BW_{RX} is the bandwidth of the receiver, and $\rho_{Te} = A_i(JT_p)$ is the reduction in the optical signal attributed only to fiber and laser (T_e).

RIN_{OMA} without eye compression

- The RIN variances (no-normalized) for each signal level is derived

$$n_0^2 = \rho_{ISI-J}^2 \frac{2(\Delta/2)^2}{1+ER^2} \sigma_{RIN-OMA}^2 = \left(\frac{\Delta}{2} \sigma_0\right)^2 \quad (A.1)$$

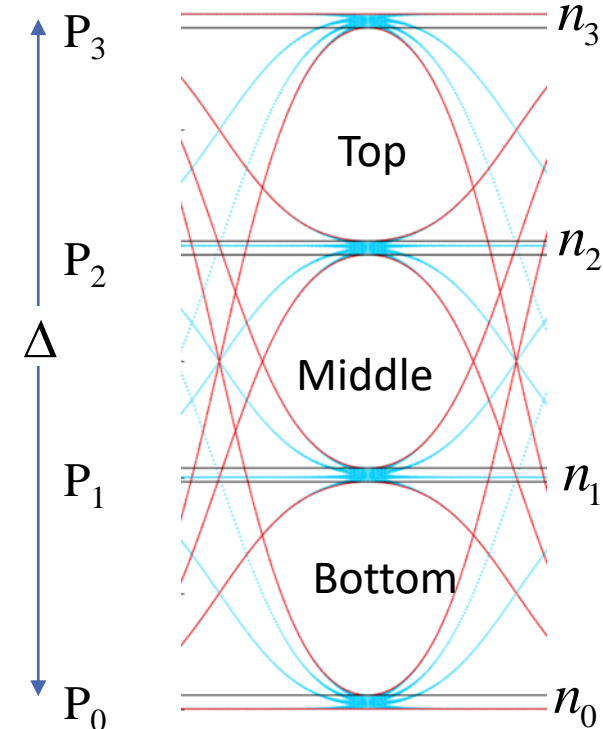
$$n_1^2 = \rho_{ISI-J}^2 2(\Delta/2)^2 \frac{(ER+2)^2}{9(1+ER^2)} \sigma_{RIN-OMA}^2 = \left(\frac{\Delta}{2} \sigma_1\right)^2 \quad (A.2)$$

$$n_2^2 = \rho_{ISI-J}^2 2(\Delta/2)^2 \frac{(2ER+1)^2}{9(1+ER^2)} \sigma_{RIN-OMA}^2 = \left(\frac{\Delta}{2} \sigma_2\right)^2 \quad (A.3)$$

$$n_3^2 = \rho_{ISI-J}^2 \frac{2(\Delta/2)^2}{1+ER^2} ER^2 \sigma_{RIN-OMA}^2 = \left(\frac{\Delta}{2} \sigma_3\right)^2 \quad (A.4)$$

$$\Delta = OMA_{Tx_outer_linear} 10^{-Losses/10} \quad (A.5)$$

$$Losses = Connector_Losses + Att Length \quad (A.6)$$



Annex III

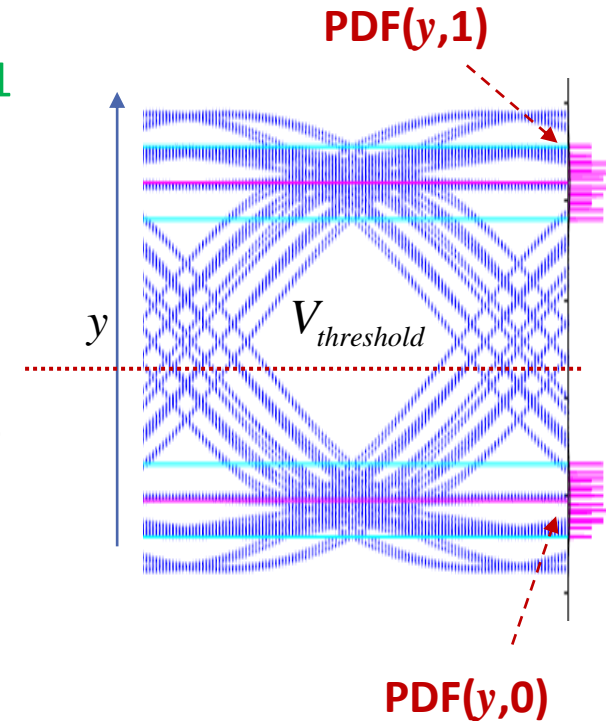
Computation Method for Margin and Penalties

Computation of Margin & Penalties PAM-2

- PAM-2 is used to explain the model (M=2 to facilitate the description)
- The Q factor for a y value in the histogram as a function of the OMA_{tx_linear} and transmission penalties P_z is given by,

$$Q_a(y, P_z) = \Delta \frac{y - V_{threshold}}{\sqrt{(P_z n_R)^2 + (n_S)^2}} = \Delta \frac{y - V_{threshold}}{\sqrt{(P_z n_R)^2 + \left(\frac{\Delta}{2} \sigma_S\right)^2}}$$

B.1



- Where y is the normalized received signal, $V_{threshold}$ is the decision threshold for the eye, $\Delta = OMA_{Tx_outer_linear} 10^{-Losses/10}$ is the OMA before the O/E, n_S is the signal (level) dependent noise (RIN, MPN, MN, baseline wander) for 0's or 1's, Q_t is the Q factor for a desired BER, P_z represents how much the AWGN can be increased from current values and still achieve the Q_t (more on Q_t in next slide)
- The AWGN, n_R , is given by,

$$n_R = \frac{1}{M-1} \frac{OMA_{Rx_outer_linear}}{2Q_T} = \frac{10^{Receiver_Sens - SECQ_{Tx}}}{2Q_T}$$

B.2

Computation of Margin & Penalties

- The allowable power that can be used to mitigate for transmission penalties is the remaining power budget after connector losses and attenuation as shown,

$$P_{B-L} = \frac{OMA_{outer_linear}}{OMA_{Rx_outer_linear}} L_{con} 10^{-att L/10} = \frac{\Delta}{OMA_{Rx_outer_linear}} \quad \text{B.3}$$

- Using B.2 to B.3 in B.1, we obtain the Q factor for each trace in the sampled eye

$$Q_a(y, P_z) = \frac{y - V_{threshold}}{\sqrt{\left(P_z \frac{OMA_{Rx_outer_linear}}{2Q_T \Delta}\right)^2 + (0.5\sigma_s)^2}} = \frac{y - V_{threshold}}{\sqrt{\left(\frac{P_z}{P_{B-L}} \frac{1}{2Q_T}\right)^2 + (0.5\sigma_s)^2}} \quad \text{B.4}$$

- The BER is obtained by integrating the normalized PDFs for each level, 0 and 1 as shown,

$$BER(P_z) = 0.5 \left[\int PDF(y, 0) \operatorname{erfc}(Q_{a_{01}}(y, P_z) / \sqrt{2}) dy + \int PDF(y, 1) \operatorname{erfc}(Q_{a_{10}}(y, P_z) / \sqrt{2}) dy \right] \quad \text{B.5}$$

- where

$$\int PDF(y, 0) dy = \int PDF(y, 1) dy = 0.5$$

Computation of Margin & Penalties

- At a given length, the actual BER of the system is obtained by using all the power budget (minus losses). This is equivalent of setting $P_z = 1$ (0 dB)

$$BER_{Link} = BER(P_z = 1) \tag{B.6}$$

- The Margin is obtained by solving B.5 (numerically) to obtain a BER that matches the BER targeted.

$$BER(P_z = \text{Margin}) = BER_{target} = 0.5 \operatorname{erfc}(Q_T / \sqrt{2}) \tag{B.7}$$

- The total penalties are obtained using,

$$\text{Penalties} = P_{B-L} / \text{Margin} \rightarrow P_{Budget_dB} - \text{Losses} - \text{Margin_dB} \tag{B.8}$$

- What is the meaning of Margin and Penalties in this model?
 - If there are no penalties (ISI, JITTER RIN, MPN...), the margin should be equal to the power budget minus losses. This is the ideal system with TDECQ=1 (0dB).
 - If the margin = 0 all the budget (minus) losses is used to compensate for ISI, Jitter, RIN, MPN, and MN penalties

Computation of individual Penalties

- **The methods to compute ISI, Jitter, RIN, MPN, MN , BL are given below**
 - For the ISI penalty, the jitter and all signal dependent noises are set to zero and P_z is numerically found. $P_{ISI} = P_{B-L} - P_z$ (in dB);
 - For Jitter penalty, all signal dependent noises are set to zero and P_z is numerically found. $P_{ISI-Jitter} = P_{B-L} - P_z$ (in dB); $P_{jitter} = -P_{ISI} + P_{ISI-Jitter}$
 - For RIN penalty all signal dependent noises with exception of RIN are set to zero and P_z is numerically found. $P_{RIN} = P_{B-L} - P_z - P_{ISI-Jitter}$ (in dB)
 - For MPN penalty all signal dependent noises with exception of MPN are set to zero, P_z is numerically found. $P_{MPN} = P_{B-L} - P_z - P_{ISI-Jitter}$ (in dB)
 - For MN penalty all signal dependent noises with exception of MN are set to zero, P_z is numerically found. $P_{MN} = P_{B-L} - P_z - P_{ISI-Jitter}$ (in dB)
 - For BL penalty all signal dependent noises with exception of BL are set to zero, P_z is numerically found. $P_{BL} = P_{B-L} - P_z - P_{ISI-Jitter}$ (in dB)
 - Cross term penalties is the difference between total penalty (previous slide) minus the sum of all the individual penalties (in dB).

Computation of Margin & Penalties



- **Summary of the model and differences compared to the worst-case eye?**
 - The Q factors are computed for each eye trace (at the center of the eye +/-Jitter).
 - The BER for each trace is computed
 - The total BER is the average of trace BER weighted using the PDFs of level 0 and 1
 - The margins are computed numerically. The total penalty is equal to the power budget minus losses minus margin (in dB).
 - The individual penalties are computed as shown in the previous slide
- **Fast checking with previous link models**
 - The margin and penalties solution for the proposed method (statistical eye are mainly numerically). However, if we select the worst case eye trace, the numerical solutions and *worst-case eye method* are identical.
 - For example if we use B.4 and make $Q_a = Q_t$

$$Q_a(y_{\text{worst_trace}}, P_z) = Q_T = \frac{0.5}{\sqrt{\left(\frac{P_z}{P_{B-L}} \frac{1}{2Q_T}\right)^2 + (0.5\sigma_s)^2}}$$

$$\text{Penalties}_{\text{worst_case-eye}} = \frac{P_z}{P_{B-L}} = \frac{1}{\sqrt{1 - (Q_T \sigma_s)^2}}$$

Link Model Margin & Penalties for PAM-4

The model is now applied for PAM-4

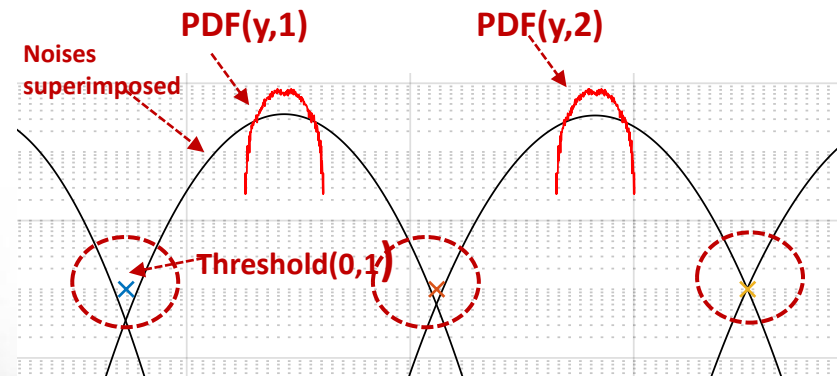
$$Q_{01}(y, P_z) = \frac{y - \text{threshold}(0,1)}{\sqrt{\left(\frac{P_z}{P_{B-L}} \frac{OMA_{outer}}{6Q_T}\right)^2 + (0.5\sigma_s(0))^2}}$$

$$Q_{10}(y, P_z) = \frac{y - \text{threshold}(0,1)}{\sqrt{\left(\frac{P_z}{P_{B-L}} \frac{OMA_{outer}}{6Q_T}\right)^2 + (0.5\sigma_s(1))^2}}$$

$$Q_{23}(y, P_z) = \frac{y - \text{threshold}(2,3)}{\sqrt{\left(\frac{P_z}{P_{B-L}} \frac{OMA_{outer}}{6Q_T}\right)^2 + (0.5\sigma_s(2))^2}}$$

$$Q_{32}(y, P_z) = \frac{y - \text{threshold}(2,3)}{\sqrt{\left(\frac{P_z}{P_{B-L}} \frac{OMA_{outer}}{6Q_T}\right)^2 + (0.5\sigma_s(3))^2}}$$

- The thresholds are computed numerically from the histograms. They are placed at the locations where the PDFs of each level intercept.
- The traditional equations for threshold does not apply here due to the arbitrary shape of the PDFs



Link Model Margin & Penalties

The *SER* is computed as follows,

$$\begin{aligned} SER(P_z) = & 0.5 \left[\int PDF(y, L0) \operatorname{erfc}(Q_{01}(y, P_z) / \sqrt{2}) dy + \right. \\ & \int PDF(y, L1) \{ \operatorname{erfc}(Q_{10}(y, P_z) / \sqrt{2}) + \operatorname{erfc}(Q_{12}(y, P_z) / \sqrt{2}) \} dy + \\ & \int PDF(y, L2) \{ \operatorname{erfc}(Q_{21}(y, P_z) / \sqrt{2}) + \operatorname{erfc}(Q_{23}(y, P_z) / \sqrt{2}) \} dy + \\ & \left. \int PDF(y, L3) \operatorname{erfc}(Q_{32}(y, P_z) / \sqrt{2}) dy \right] \end{aligned}$$

Where the PDFs of the signal for each level satisfies

$$\int PDF(y, L0) dy = \int PDF(y, L1) dy = \int PDF(y, L2) dy = \int PDF(y, L3) dy = 0.25$$

The BER is computed assuming Gray coding

$$BER(P_z) = 0.5 SER(P_z)$$

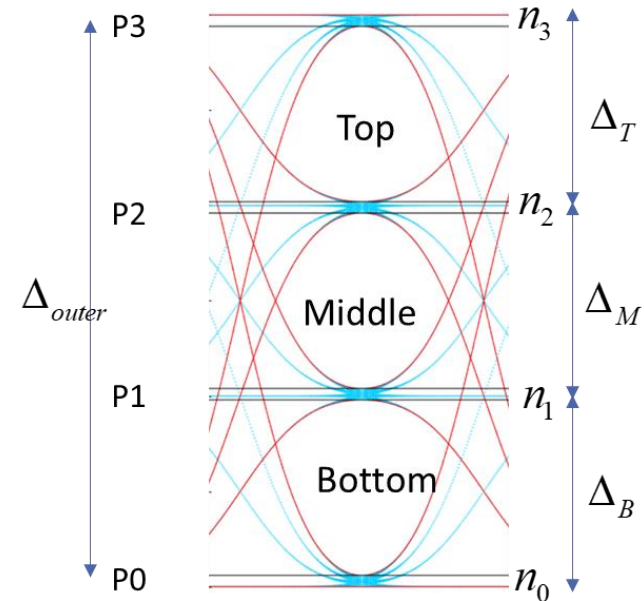
Link Model Margin & Penalties

- The BER of the system is given by,

$$BER_{Link} = BER(P_z = 1)$$

- The Margins are computed numerically by finding the P_z value that makes the link BER equal to the target BER. Provide the margin

$$BER(P_z = M \text{ arg in}) = BER_{target} = 0.5 \operatorname{erfc}(Q_T / \sqrt{2})$$



- Therefore all the eyes are solved at once. There is only one margin value for the system instead of three margins for each eye!
- The penalty for all signal dependent noises is given by,

$$Penalties = P_{Budget} - M \text{ arg in}$$

- The individual ISI, Jitter, RIN... penalties are computed using the same methodology as previously shown for the PAM-2 case

Annex IV Relationship of Link Model with TDECQ

TDECQ from link model margin derivation

The value of TDECQ can be computed as follows,

$$TDECQ = \frac{OMA_{outer}}{\sqrt{n_G^2 + n_R^2} 6Q_T} = \frac{OMA_{outer}}{n_T 6Q_T}$$

Where n_G is the maximum noise amount that can be added (before equalizer) while maintaining the BER target, . Therefore,

$$n_T = \sqrt{\left(\frac{OMA_{outer} M \arg in_{TDECQ}}{6P_{B-L} Q_T}\right)^2 - n_R^2 + n_R^2} = \left(\frac{OMA_{outer} M \arg in_{TDECQ}}{6P_{B-L} Q_T}\right)$$

$$TDECQ = \frac{OMA_{outer}}{\frac{OMA_{outer} M \arg in_{TDECQ}}{6} \frac{P_{B-L}}{Q_T} 6Q_T} = \frac{P_{B-L}}{M \arg in_{TDECQ}} \approx Penalties_{At2m,with_BW_TDECQ}$$

Notes:

- TDECQ in this computation only consider the noises at 2 m using the specified BW.
- Therefore is does not guaranty that longer reaches with more noise will work.
- Moreover, is a receiver with better sensitivity is used $n_r' = X n_r$, where $X < 1$, the TDECQ is also should reduced by X