

# Initial ILT setting and maximum Tx swing

Comments #218, #263

Adee Ran, Cisco

# The comments

<i>Cl</i> 179	<i>SC</i> 179.9.4.1.3	<i>P</i> 383	<i>L</i> 31	# 263
Ran, Adee		Cisco		
<i>Comment Type</i>	<b>TR</b>	<i>Comment Status</i>	<b>D</b>	<i>Max swing &amp; initial ILT setting</i>
The "initialize" values adopted in D1.4 are different for CR and for C2M.				
This requires different initialization in the transmitter and, very likely, a different algorithm in the receiver, depending on the mode chosen for the port (whether a module or a copper cable is plugged). These create an unnecessary burden for firmware developers, possibly increasing the code size and development/debugging time.				
The motivation for choosing preset 6 for the initial setting was to limit the initial swing reaching the receiver input. The maximum transmitter swing with preset 6 is 0.75 V. In comparison, CR initial setting is preset 1, which has a maximum transmitter swing of 1 V.				
It is reasonable to assume that CR receivers can handle 1 V output swing of the transmitter (which will be attenuated by the channel, assumed to have considerable loss at frequencies present in the ILT signal).				
If preset 6 is used as the initial value for CR too, the transmitter's $v_f$ (measured near the transmitter with preset 1) for these PMDs can be allowed to be as high as 0.6 V; If a device has $v_f$ at this maximum value, then with preset 6, the transmitter swing will be 0.9 V, lower than the 1 V currently allowed. If a device has $v_f$ of 0.5 (the maximum in D1.4) its maximum will be 0.8 V. Either way, the receiver will see an even lower swing.				
This will enable using a higher output swing for CR, potentially increasing their reach (if the transmitter is capable), and using the same adaptation algorithms in the receiver.				
This change does not require increasing $A_{ne}$ in COM; having transmitter swing at the maximum on one end of the cable and at the minimum on the other is not a likely situation and can be excluded from cable compliance assumptions. Devices should work with cables that meet the existing specifications.				
A similar argument can be made for KR vs. C2C.				

## *SuggestedRemedy*

In Table 179-7, change the Transmitter steady-state voltage  $v_f$  range from "0.4 to 0.5" to "0.4 to 0.6", and change "differential peak-to-peak voltage (max) , transmitter enabled" from "1" to "1.2".

In Table 179-8, change the "initialize" setting to match preset 6, and delete "and initialize" in the footnote.

In Table 179-10, change the "Amplitude tolerance" value from "0.5" to "0.6".

in 179.9.5.2, add an informative note as follows:

"NOTE--The steady-state voltage in Table 179-10 corresponds to preset 1. It is not initially generated by a transmitter, due to the initialize setting in Table 179-8. The receiver is not required to tolerate preset 1 unless it specifically requests for it."

Optionally, apply the corresponding changes in clause 178.

<i>Cl</i> 179	<i>SC</i> 179.9.4.1.3	<i>P</i> 383	<i>L</i> 31	# 218
Dawe, Piers		Nvidia		
<i>Comment Type</i>	<b>TR</b>	<i>Comment Status</i>	<b>D</b>	<i>Max swing &amp; initial ILT setting</i>
Transmitters are supposed to start Training at medium amplitude (preset 6) now, not the loudest, to avoid possible crosstalk and linearity issues. A receiver that prefers a louder signal on a particular channel can ask for it.				
<i>SuggestedRemedy</i>				
In Table 179-8, for "initialize", change 1 to 0.75, add the tolerances, and delete "and initialize" in the table footnotes. As in Table 176D-9 (which applies to 176C).				
<i>Proposed Response</i>				
<i>Response Status</i> <b>W</b>				
PROPOSED ACCEPT IN PRINCIPLE.				
For CRG discussion, along with comment #263.				

# The suggested changes

## **Both comments suggest**

- A. Changing the “initialize” setting for CR PHYs to have  $c(0)$  of 0.75 (as in preset 6) instead of 1 (as in preset 1), identical to AUI-C2M.

(for different reasons: #263 is about transmitter initialization logic and receiver adaptation algorithms, #218 is about crosstalk and linearity).

## **#263 additionally suggests**

- B. Adding an informative note explaining amplitude tolerance (179.9.5.2), as in the proposed response to comment #126 (which addresses amplitude tolerance in C2M).
- C. Changing the maximum steady-state voltage for CR PHYs from 0.5 V to 0.6 V and make corresponding changes in the peak-to-peak (1.2 V) and amplitude tolerance specifications.
- D. Considering change C for clause 178 too.

This presentation assumes that item A (common to both comments) and item B (non-controversial) will be implemented; it focuses item C.

# Why is max steady-state voltage 0.5 V?

- The maximum  $v_f$  was 0.6 V (1.2 Vpp) in D1.2, and in many previous electrical PMD clauses.
- The change to 0.5 V was proposed in [simms 3dj 01 2411](#) with reasoning shown in the next slide.
  - Straw poll #E-1 indicated support: Y: 22 N: 10 NMI: 5 A: 9 (see response to comment #345 against D1.2)
  - The proposal was adopted and implemented D1.3.
- In D1.4 there was an additional change of the initial equalizer value in the AUI C2M/C2C transmitter...
  - Further reducing the signal at the receiver input
  - This change was not applied for CR/KR PMD transmitters

# The reasons for the reduction

## Summary

### Reducing $V_f$ max from 0.6V to 0.5V

- Reduces complexity of receiver design
- Enables lower power supply SERDES
- Enables current and future silicon process nodes
- Increases compatibility with other SERDES Specifications
- Reduces system power and noise

- The main technical argument was the complexity of receiver design to handle a large input swing, especially with current and future silicon process nodes.
  - Enabling lower power supply is likely related to that.
- Other benefits mentioned seem less relevant – since they could be achieved by design choice even with the previous limits.
- It was also mentioned that COM improves by this reduction.

Source: [simms 3dj 01 2411](#) slide 9

# Addressing receiver input swing

- The initial signal sent over the cable is training frames at the “initialize” setting, synchronous PRBS13 and PAM2 modulation.
- Even if a transmitter has the maximum allowed swing, the signal seen by the receiver will be attenuated by the channel
  - And by the “initialize” setting, assuming we adopt the proposed change (A).
- For CR, there is a minimum cable assembly loss, specified as 16 dB (Table 179–13)
  - This is between TP2-TP4
  - TP0d to TP5d is likely significantly higher!
- A receiver can (and likely will) change the Tx equalization setting through ILT; for a high loss channel, it is likely that the full swing (maybe with some Tx equalization) will be beneficial
  - What setting is used depends on the receiver’s ILT algorithms
- Simulation results in the subsequent slides show the effect of a 16 dB channel and Tx equalization on the Rx input swing.

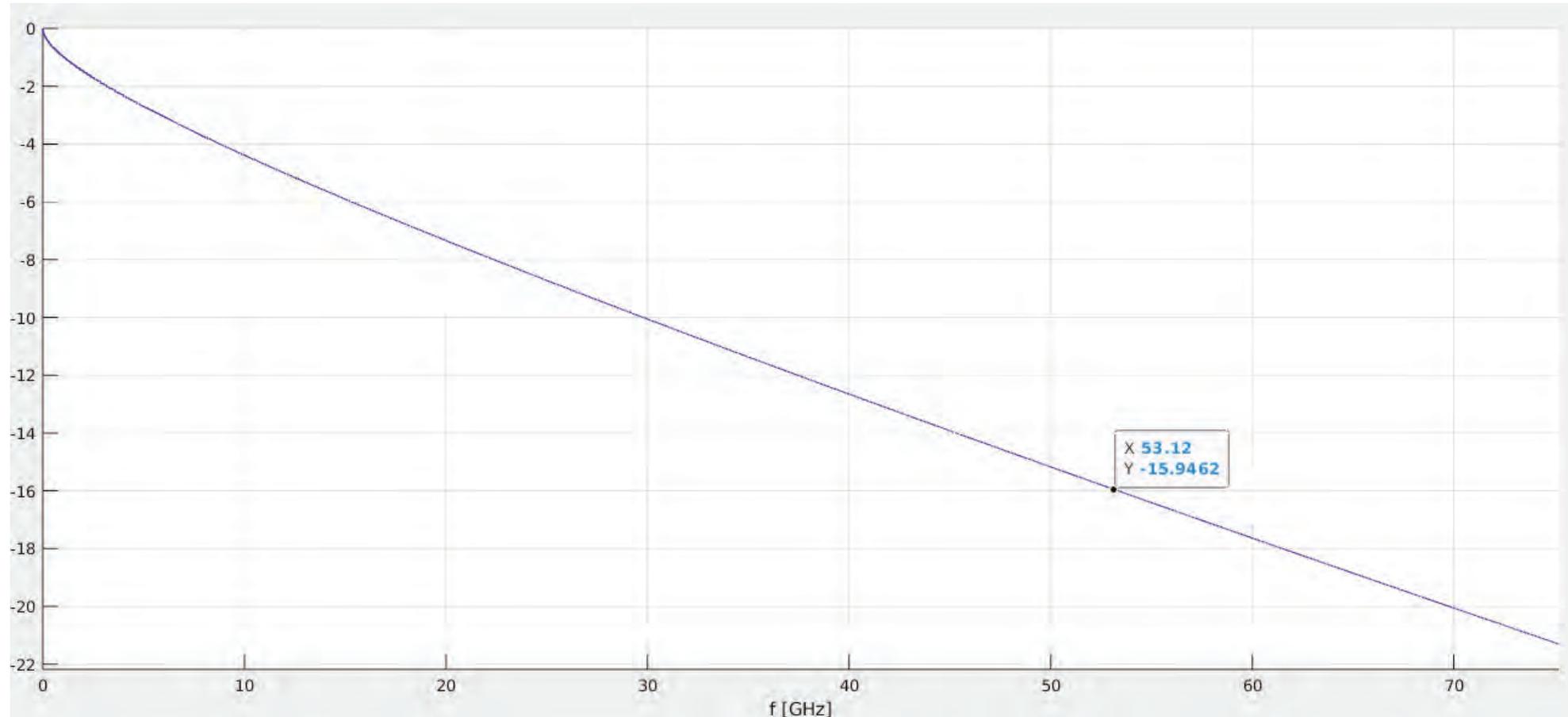
# Simulation setup

- Pattern: two training frames with PRBS13 PAM2,
- Tx output swing: 1 Vpp
- Test cases:
  1. 1 dB channel (very close to Tx output) with preset 1 (initial training pattern in CR)
  2. 16 dB channel (Rx input, minimum IL) with preset 1
  3. 16 dB (Rx input, minimum IL) + preset 4

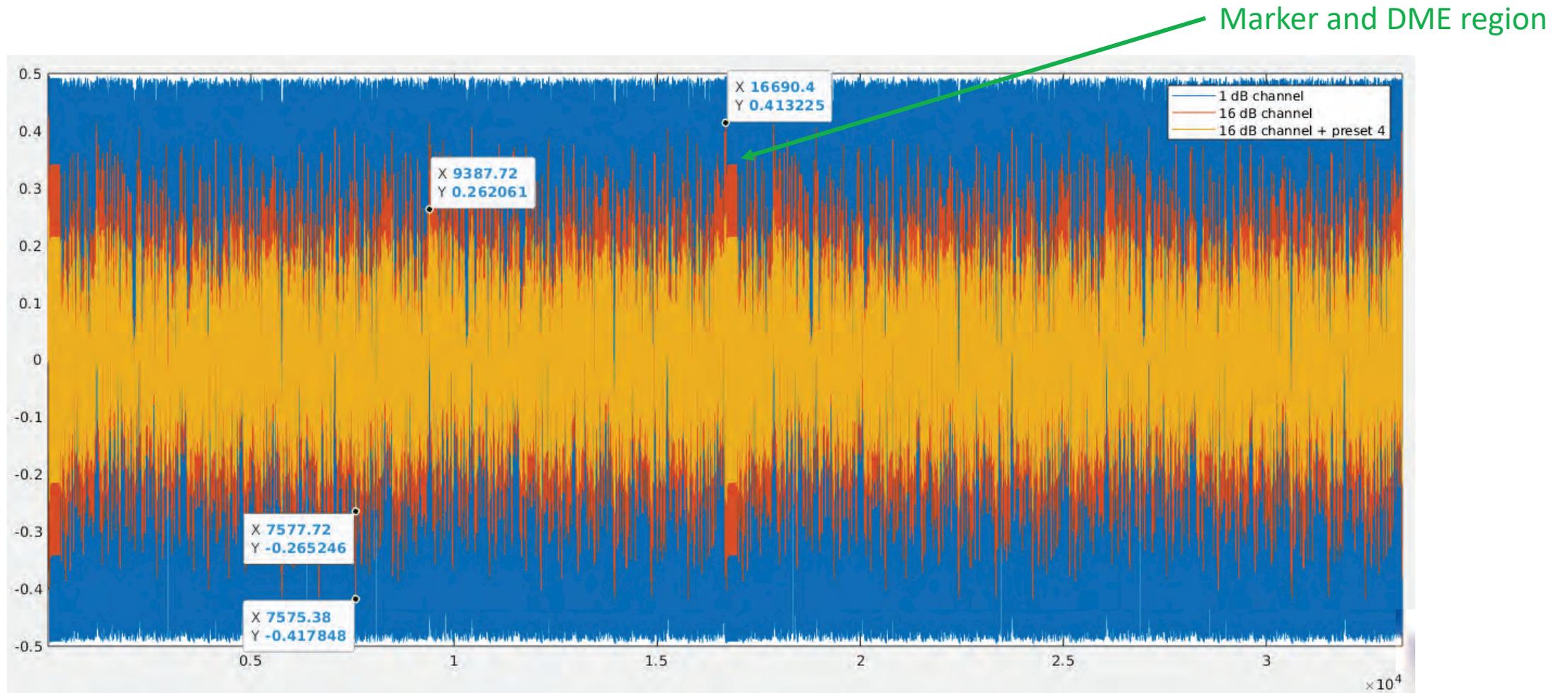
Note: preset 4 (nominal coefficients [0.05, -0.2, 0.75]) creates a DC voltage attenuation of 0.6 (-4.4 dB).

# 16 dB Channel used in the simulation

(smooth channel created using the PCB mathematical model)

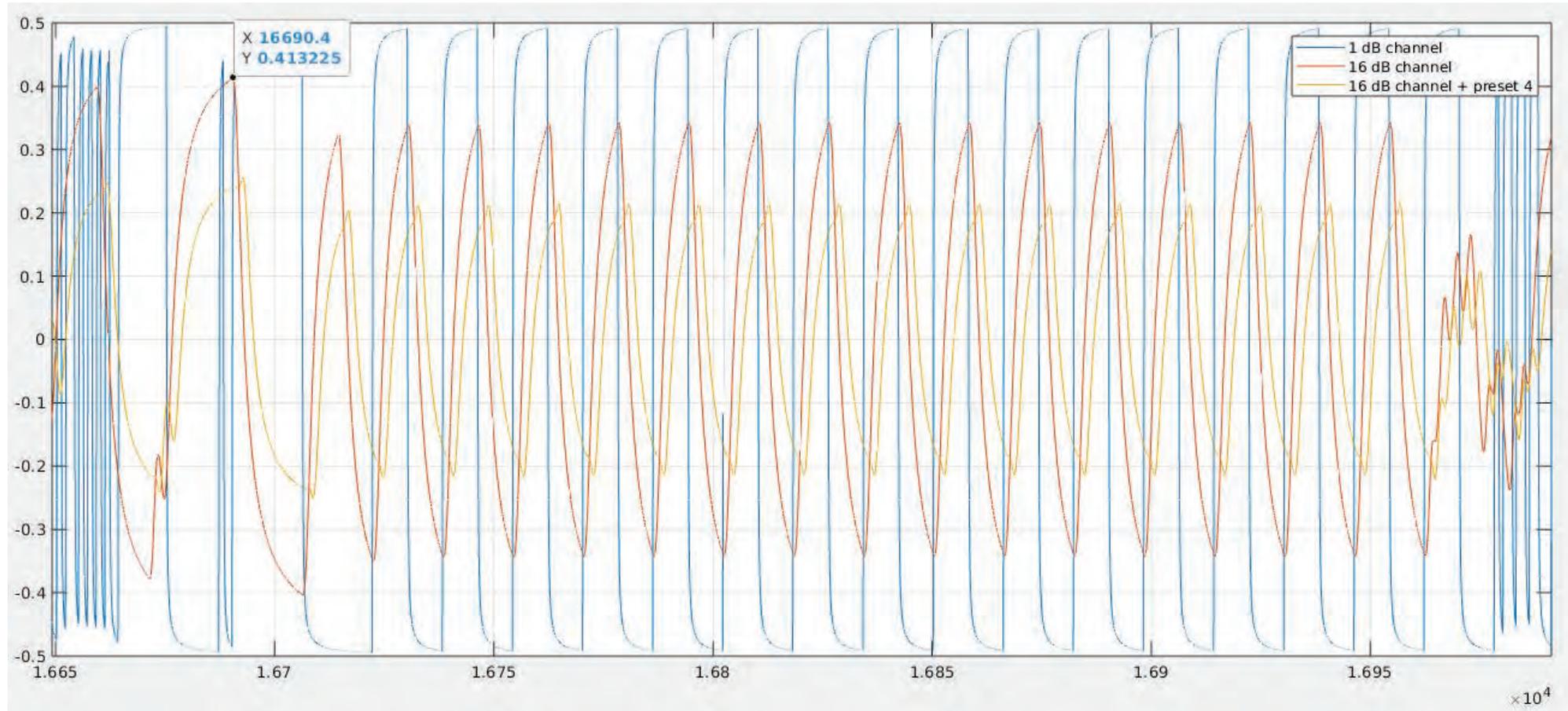


# Waveforms: two full training frames



The signal is attenuated by the channel and by the Tx equalizer – the Tx output swing is never seen by the receiver

# Zooming on the training frame marker + DME



# Observations

- The 16 dB channel reduces the swing of the training signal from 1 Vpp (Tx) to **0.83 Vpp** (Rx)
  - If preset 6 is used for initialize (change A), it would become **0.62 Vpp** at the Rx input
  - If preset 6 is used for initialize *and* maximum Tx swing is increased to 1.2 Vpp (change C), it would become **0.747 Vpp** at the Rx input – still lower than the current 0.83 V
- Applying preset 4 in the Tx reduces the Rx input swing to **0.53 Vpp**
  - If maximum Tx swing is increased to 1.2 Vpp (change C), it would become **0.636 Vpp** at the Rx input
  - With preset 4, the maximum possible Rx input swing in data mode is **0.72 V** (extremely rare long runs)
- **The input swings listed above should not be a problem for current Rx designs**
  - Experience from 100G SerDes confirms that.
- Practical CR channels have loss much higher than 16 dB – so the values above are conservative.

# Summary of results

Specification	Initial Tx output swing [V]		Initial Rx input swing, 16 dB channel, PRBS13 [V]		Max Rx input swing, 16 dB channel, data mode with preset 4 [V]	
	Min	Max	Min	Max	Min	Max
802.3ck PMDs (e.g. 200GBASE-CR2)	0.8	1.2	0.73	1.09	$0.8*0.6=0.48$	$1.2*0.6=0.72$
200GBASE-CR1 (D1.3 and current) <i>200GAUI-1 in D1.3</i>	0.8	1	0.7	0.87	$0.8*0.6=0.48$	0.6
200GAUI-1 (current)	$0.8*0.75=0.6$	0.75			$0.8*0.6=0.48$	0.6
200GBASE-CR1, per comment #263 (A)	$0.8*0.75=0.6$	0.75	0.52	0.65	$0.8*0.6=0.48$	0.6
200GBASE-CR1, per comment #218 (A&C)	$0.8*0.75=0.6$	$1.2*0.75=0.9$	0.52	0.78	$0.8*0.6=0.48$	$1.2*0.6=0.72$

# What about COM?

- COM is a channel metric, not a predictor of real link performance
  - The combination of  $A_v$ ,  $A_{fe}$ ,  $A_{ne}$  (victim, FEXT, and NEXT amplitudes) has always been “the worst combination”
  - Thus, the values we have today are based on min  $v_f$  (0.4 V) and max  $v_f$  (0.5 V)
- What if we increase max  $v_f$  to 0.6 V?
- Assume some device uses that allowance and has  $v_f$  above 0.5 V
  - Its partner has a larger signal (and FEXT) – it is generally beneficial for Rx performance (if not, it can attenuate it)
  - The device has to endure the higher NEXT it creates on its own Rx
    - This may be within the implementation budget (3 dB COM)
    - It should be an implementation choice
- If both sides of a link have the same  $v_f$ , increasing it can provide benefits:
  - Longer reach for the same Rx performance
  - Better Rx performance (lower BER, FLR) for a given channel
- The PMD specification should allow that
- We can keep the COM amplitude parameters as they are in D1.4, or change them to match  $v_f$ 
  - Either way, this can be done after D2.0
  - Note that cable assembly channels (TP2 to TP4) have not been contributed so far...

# What about transmitters?

- The  $v_f$  range min/max should cover both design freedom and variations between devices.
- The reduced range limits design freedom.
- Given receivers can handle it, whether Tx implementations will reach the maximum swing should be an implementation choice
  - Perhaps no implementation will reach  $v_f$  of 0.6 for practical reasons...
  - But the current maximum will unnecessarily limit implementations.
- Enabling higher swing can be used to increase cable reach, which can reduce overall power by removing the need for retimers or reducing the number of hops in a network.
  - An unnecessary limiting spec might be ignored by the market!

# What about clause 178 (KR)?

- The same arguments made for CR also apply to KR
  - Except that there is no defined minimum channel IL
- How likely is it that a backplane system has ILdd (TP0d to TP5d) lower than 16 dB?
  - This possibility does not seem to justify a different specification.
  - Tx output can be reduced by device configuration.

# Summary

- Referring to the changes listed on [slide 3](#):
  - **Change A** is suggested by both comments and will hopefully be in consensus.
  - **Change B** provides clarification of amplitude tolerance, and matches a proposed response to #126.
  - **Change C** would enable broader application space for CR PHYs, while not harming receivers, as shown.
  - **Change D** would align the KR and CR specifications.
- Recommendation: implement all four changes.

# That's all

Questions?