

P802.3z Draft 4.2 Comments

CI 00 SC P L [redacted]
Michael A Fischer Digital Ocean, Inc.

Comment Type T

Entered by H. Frazier from handwritten note which accompanied ballot

Reason for Abstaining on 802.3z/D4.0 recirc. Michael Fischer

I have reviewed this draft with the same care as had I been voting, and have found [underline] nothing [underline] which would have caused me to vote "negative". However, I must abstain because I am involved as a witness in a lawsuit which concerns certain implementations of 802.3 standards.

Proposed Response

CI 00 SC P L # 82 [redacted]
Michael A Fischer Digital Ocean, Inc.

Comment Type T Comment Status D

Entered by H. Frazier from handwritten note which accompanied ballot

Reason for abstaining - Michael Fischer

I reviewed the document with the same care as if I had been voting. I found nothing that I considered a technical flaw that would justify a vote of "negative."

However, I cannot cast an actual vote at this time because I am involved as both a fact and expert witness in a patent infringement lawsuit that concerns some of the provisions in IEEE 802.3u, and might also be relevant to 802.3z in the future. Because this ballot is due before the suit has ended, I must abstain.

SuggestedRemedy

Proposed Response Response Status O

CI 00 SC 7.3.2 P7.1 L1 # 99004 [redacted]
Bay Networks, Inc.

Comment Type TR

Restore the clock specification for 10 Mb/s that was inadvertently deleted by P802.3x (CIs 07)

It is recognized that this is a service to humanity and not within the nominal scope of the extension to the existing standard to specify Gigabit operation. It is a very important piece of the standard as a whole. I wish to insure that no future edition of the merged standard is printed without the correction of this error.

I will not let this item be a critical path item in the approval of this standard. If a case can be made that this is a critical path item I will withdraw this comment.

SuggestedRemedy

This comment has been recycled from Draft D4.1 (was #112) Page and Line numbers refer to D4.1.
Change 7.3.2 paragraph 1 to read:

The signaling rate specified here is 10 million bits per second ± 0.01%. Other signaling rates are specified elsewhere in this standard.

Proposed Response

REJECT.

This change would be outside the scope of 802.3z.

[Editor's note: Because the commentor believes this to be an important issue, and wishes to have this comment widely circulated within the 802.3 community, he has chosen to not APPROVE of this response at this time. The remainder of the clause 34 subtask force unanimously rejected the comment.]

[Additional note: The 802.3 maintenance committee plans to recommend this change in the recirculation of P802.3aa, Maintenance #5, which is expected to reach publication in the same time frame as 802.3z.]

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Comment Status **D**

Comment transcribed by H. Frazier from handwritten submission.
Text in brackets [] was inserted by H. Frazier.
The ballot associated with this comment was marked "Affirmative with Comments".

I agreed w/ Mr G. Thompson [regarding his unresolved negative comment number 112 on 802.3z/D4] and felt that his strong position/point would have been "accepted"

I now "comment" that the plans of 802.3aa M#5 committee to accept this fix in a timely manner to [illegible] the transition relevance from the 10 Mbps heritage.

SuggestedRemedy

Proposed Response *Response Status* **O**

1

Comment Status **D**

I want to know why I cannot view all the edited pages per our last meeting in Irvine.
Thanks

SuggestedRemedy

Proposed Response *Response Status* **O**

Bill Lane

CSU Chico

The statement, "The PLS service primitives provided by the Reconciliation sublayer, and described here, behave in exactly the same manner as defined in clause 6.", is not completely correct. When the PLS_xxx.indication primitives were changed to PLS_xxx.indicate primitives in the just-published 802.3x and y, not all instances of "indication" were changed to "indicate".

SuggestedRemedy

6.2.3 - All enumerated PLS_xxx.indication primitives need to be changed to PLS_xxx.indicate - 4 places.

6.2.1.2 - PLS_DATA.indication in the subclause title should be

6.3.1.2.3 - In the note, indication should be changed to indicate.

6.3.2.3 - PLS_DATA_VALID.indication in the subclause title should be changed to PLS_DATA_VALID.indicate.

6.3.2.3.2 - PLS_DATA_VALID.indication should be changed to PLS_DATA_VALID.indicate.

6.3.2.3.3 - PLS_DATA_VALID.indication should be changed to PLS_DATA_VALID.indicate.

I do not know whether these correction should be made in 802.3z or whether they should be added to the list of things to be done when all of these supplements are merged into the next edition of the base standard. Either is OK, but approval of 802.3z should not be delayed.

It is a good standard and you are to be congratulated. Well done.

Proposed Response

PROPOSED ACCEPT.

None of the service primitives in this clause are changed by 802.3z, and therefore, implementing the suggested remedy should be considered as a service to humanity. The inconsistency in use of .indicate and .indication was noted by the 802.3z editorial staff earlier in the process and determined to be outside the scope of our work.

The comment will be conveyed to the IEEE editor for possible resolution in production of a new version of 802.3. If this is not possible, the comment will be resubmitted for consideration in a maintenance project.

howard frazier cisco systems, inc # 18

"maximize" should be "maximizes".

Change "maximize" to "maximizes".

Proposed Response

CI 35 SC 35.4.2.1 P35.23+ L # 2

Brad Booth Jato Technologies

Comment Type **E** *Comment Status* **D**

Figures 35-17, 35-18, 35-19, 35-20 and 35-21 sit in the middle of the paragraph.

SuggestedRemedy

Move figures to be between paragraphs.

Proposed Response *Response Status* **W**

PROPOSED ACCEPT IN PRINCIPLE.

The anchoring of figures within paragraphs is done so they appear closer to the referencing text. No efforts have or will be made to optimize figure placement during the development of the standard. Final location of figures, handling of white space and the like will be done in publication of the standard by the IEEE editor.

The IEEE editor will be informed that the current anchor definitions split paragraphs.

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CI 36 SC 36.2.5.1.3 P36.22 L 9 # 41
Joe Kryzak gigether

Comment Type T Comment Status D

Please withdraw my previous comment (my error!):

My question is enabling cgbad vs. cggood, in respect to the synchronization state machine. For example, in the state sync_acquired_1 on page 36.34, there are two next states, one enabled by cggood, the other by cgbad. My understanding is that both of these can be enabled at the same time. Is cgbad to have priority? If I receive a valid comma in that state while rxeven is true, what would the next state be? Both cggood and cgbad would be enabled!

SuggestedRemedy

Proposed Response Response Status Z

Comment withdrawn by commenter.

CI 36 SC 36.2.5.1.3 P36.22 L 9 # 24
Joe Kryzak Gigether

Comment Type T Comment Status D

My question is enabling cgbad vs. cggood, in respect to the synchronization state machine. For example, in the state sync_acquired_1 on page 36.34, there are two next states, one enabled by cggood, the other by cgbad. My understanding is that both of these can be enabled at the same time. Is cgbad to have priority? If I receive a valid comma in that state while rxeven is true, what would the next state be? Both cggood and cgbad would be enabled!

SuggestedRemedy

1. Explain why a code group is "bad" or "good" because you are receiving a valid comma when rxeven is true. It's obvious why a invalid code group is considered bad, but when you OR it with the comma and the rxeven function, it becomes vague.
2. The titles cggood and cgbad imply a binary relationship, where one is the opposite of the other. Pick a name that incorporates priority.

Proposed Response Response Status Z

Comment withdrawn by commenter.

CI 36 SC 36.2.5.1.6 P36.27 L 13 # 8
Brad Booth Jato Technologies

Comment Type E Comment Status D

PMA_UNITDATA.request is not sent by the PMA Transmit process, it is sent to the PMA Transmit process.

SuggestedRemedy

Change to read:
"A signal sent to the PMA Transmit process conveying the next code-goup ready for transmission over the medium (see 36.3.1.1)."

Proposed Response Response Status W

Accepted per suggested remedy.

cisco systems, inc

Comment Status **D**

"Pause priority resolution" is an inappropriate term, since the resolution of the pause configuration does not depend on any relative prioritization of the configuration options.

SuggestedRemedy

Reword the second paragraph of 37.2.4.2 as follows:

Priority resolution is supported for the full and half duplex modes of operation. Full duplex shall have priority over half-duplex. Resolution of the pause capability shall be resolved as specified by table 37-4. Resolution which precludes operation....{remainder unchanged}

Change the title of table 37-4 to read:

Table 37-4-- Pause capability resolution

Proposed Response *Response Status* **W**

Accepted per suggested remedy.

P802.3z Draft 4.2 Comments

Joe Gwinn Raytheon # 44
Comment Status D

CI 38 SC 38.10 P38.19 L 1-14 # 60
Dan Brown AMP
Comment Type T Comment Status D

SuggestedRemedy

On Figure 38-1, show where the "MDI" blocks or interfaces are.

On Figure 38-7, show where the various test points and bulkheads are.

An accountant should be able to correlate the two drawings.

Proposed Response Response Status O

than tables 38-5 and 38-9 to describe identical parameters. For example:

Tables 38.5 and 38.9 use the terms "operating distance" and "channel insertion loss" while Table 38-11 uses the terms "link length" and "channel attenuation".

SuggestedRemedy

Suggest deleting Table 38-11 in its entirety. Global change references to Table 38-11 to "tables 38-5 and 38-9" (specific references contained in clauses 38.10, 38.11.2.1, and 38.11.2.2).

Proposed Response Response Status O

CI 38 SC 38.10 P38.18 L 40 # 21
howard frazier cisco systems, inc.
Comment Type T Comment Status D

The reference to "channel insertion loss" seems incorrect, since table 38-11 lists "channel attenuation", and the values are different from the "channel insertion loss" shown in other tables. If "Channel insertion loss" is the correct term, then the values in the table appear to be wrong. If the values are actually supposed to represent "channel attenuation", then the reference to "channel insertion loss" in this paragraph, and in the title of the table, should be changed to "channel attenuation".

SuggestedRemedy

Either:

1) Change "channel insertion loss" to "channel attenuation" in the text and in the table title, or

2) Change "channel attenuation" to "channel insertion loss" in column 1, row 4 of table 38-11, and correct the values in row 4.

Proposed Response Response Status O

CI 38 SC 38.10 P38.19 L 13 # 79
Lucent Technologies
Comment Type E

Note b. is obtuse. The link lengths referred to are included within the associated table, Table 38-11. No reference to other tables is necessary, and doing so causes confusion.

SuggestedRemedy

Change Note b. to read:
"Link lengths used to calculate channel attenuation are those specified in this table."
An alternative is to delete Note b. and change the "Link length" row heading to "Link length of calculation".

Proposed Response

Lucent Technologies

Specification for 50 micron 1300 nm bandwidth is unclear. The present style can be misinterpreted to be an 850/1300 nm spec.

SuggestedRemedy

Change "400/500" to "400 or 500".

Proposed Response

P802.3z Draft 4.2 Comments

Steven E. Swanson Corning Inc. # 32

As written, significant confusion will exist between "connections" and "interfaces." Separate definitions are needed and recommended.

SuggestedRemedy

Reword this subclause as follows:

"38.11.2 Optical fiber connection

An optical fiber connection as shown in Figure 38-7 consists of a pair of connector plugs mated through a connector adaptor. The 1000BASE-SX and 1000BASE-LX PMD is coupled to the optical cable plant through a connector plug into the MDI optical receptacle (see 38.11.3).

38.11.2.1 Connection insertion loss

The insertion loss is specified for a connection, which consists of a pair of connector plugs mated through a connector adaptor.

[Insert text from current 38.11.2.1]

[Insert text from current 38.11.2.2]

38.11.2.2 Connection return loss

[Insert text from current 38.11.2.3]

Proposed Response

CI 38 SC 38.11.2.1 P38.20 L 14 # 52
Joe Gwinn Raytheon

Comment Type E *Comment Status* D

The lower modal-bandwidth cell for 1310-nm SMF is empty, while the upper cell contains a "N/A". To be perfectly clear and consistent, the empty cell should be filled.

Either add a "N/A" in the empty cell, or delete the horizontal line between the current N/A and blank cells, so the N/A will apply to both.

Proposed Response *Response Status* O

CI 38 SC 38.11.2.4 P38.20 L 47 # 15
Bob Musk Hewlett Packard

Comment Type E *Comment Status* D

Figure 38.8 - 1000BASE-LX Offset mode conditioning patchcord assembly. Some confusion related to keying features of the SC Duplex connector in this figure have been observed. Keying features are not identified in this drawing.

SuggestedRemedy

Propose that the existing figure is replaced with an improved drawing to identify the keying features of the SC connectors. A suitable drawing has been prepared and is available upon request. It will also be presented at the Interim meeting.

Proposed Response *Response Status* O

CI 38 SC 38.11.2.4 P38.21 L 23 # 54
Joe Gwinn Raytheon

Comment Type T *Comment Status* D

I think we want to ask that it be made difficult for a user to take one of these mode conditioning patch cords apart without destroying it, to prevent curious users from discombobulating our careful little offsets, which are of order the diameter of human hair, and thus hard to see.

SuggestedRemedy

Add a sentence strongly suggesting that mode conditioning patch cords be made in such a manner as to make them quite difficult to disassemble without destroying them, to ensure survival of the careful offsets in the face of day to day bumps, and the curious.

Proposed Response *Response Status* O

CI 38 SC 38.11.2.4 P38.21 and 3 L 16-55 and # 34
Steven E. Swanson Corning Inc.

Comment Type E *Comment Status* D

Since the mode conditioning patch cord is a special connection, create a separate subclause.

SuggestedRemedy

Create 38.11.4, "Mode conditioning patch cord for MMF operation of 1000BASE-LX"

Proposed Response *Response Status* O

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35

Cl 38 SC 38.11.3 P38.22 L 17 # 33

Comment Status D

Since polarity is important for the mode conditioning patchcord, the drawing should show the key location.

Use a plug drawing similar to that in Figure 38-9 for Figure 38-8.

Proposed Response Response Status O

Steven E. Swanson

Comment Type E

As written, significant confusion will exist between "connections" and "interfaces." Separate definitions are needed and recommended.

SuggestedRemedy

Joe Gwinn Raytheon
Comment Status D

multimode fiber and mechanical connection between SC connector paths.

SuggestedRemedy

Use some other drawing symbology to signify mechanical connection, a symbology that does not resemble any of the fiber paths. Probably, two thin lines joining the path bodies (which contain TX and RX) would work.

Proposed Response Response Status O

- a) meet the dimension and interface specifications of IEC 61754-4 and IEC 61754-4 Part 4.2
- b) meet the performance specifications as specified in IS 11801
- c) ensure that polarity is maintained
- d) the receive side of the receptacle is located on the left when viewed looking into the transceiver optical ports with the keys on the bottom surface.

A sample drawing of a duplex SC connector plug and an MDI optical receptacle is provided in Figure 38-9.

[Insert Figure 38-9]"

Proposed Response

Steven E. Swanson

Item PMS3 on launch power is redundant with PMS1 since the transmitter shall meet all specifications defined in Table 38-3 and launch power is one of them.

Proposed Response

38

Comment Status D

Consistent with my comments clarifying the difference between a "connection" and "interface" in 38.11.3 above, a connection necessarily requires two plugs and an adaptor or a plug and receptacle.

SuggestedRemedy

Change L12 to read: "MDI optical receptacle"

Proposed Response Response Status O

Steven E. Swanson

receptacle.

SuggestedRemedy

Change L11 to read: "MDI optical plug"

Proposed Response

Joe Gwinn

Raytheon

Comment Status D

SuggestedRemedy

On Figure 38-1, show where the "MDI" blocks or interfaces are.

On Figure 38-7, show where the various test points and bulkheads are.

An accountant should be able to correlate the two drawings.

Proposed Response Response Status O

CI 38 SC 38.2.4 P38.4 L 35 # 7

howard frazier cisco systems

Comment Type T Comment Status D

The text and table describing the Signal Detect function is unnecessarily complex, and subject to misinterpretation. The essential requirements are not obvious, and there is a certain amount of redundancy.

SuggestedRemedy

Replace all of 38.2.4 with the following:

38.2.4 PMD signal detect function

The PMD Signal Detect function shall report to the PMD service interface, using the message PMD_SIGNAL.indicate(SIGNAL_DETECT) which is signaled continuously. PMD_SIGNAL.indicate is intended to be an indicator of optical signal presence.

The SIGNAL_DETECT parameter shall be set to FAIL under the conditions defined in Table 38-1. The SIGNAL_DETECT parameter shall be set to OK under the conditions defined in Table 38-1, provided that the optical input is generated by an appropriate optical transmitter which is transmitting 1000BASE-X code-groups as defined in this standard.

Under all other conditions, the value of the SIGNAL_DETECT parameter is unspecified. This standard imposes no response time requirements on the generation of the SIGNAL_DETECT parameter.

Table 38-1 SIGNAL_DETECT value definition

Receive Conditions	Value
Input optical power < -30dBm	FAIL
-30dBm < Input optical power < Receive Sensitivity	unspecified
Input optical power > Receive Sensitivity	OK

As an unavoidable consequence of the requirements for the setting of the SIGNAL_DETECT parameter, implementations must provide adequate margin between the input optical power level at which the SIGNAL_DETECT parameter is set to OK, and the inherent noise level of the PMD due to cross talk, power supply noise, etc.

Various implementations of the Signal Detect function are permitted by this standard, including implementations which generate the SIGNAL_DETECT parameter values in response to the amplitude of the 8B/10B modulation of the optical signal and implementations which respond to the average optical power of the 8B/10B-modulated optical signal.

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Proposed Response

Response Status **O**

CI 38 SC 38.2.4 P38.4 L 39 # 4
Pat Gilliland Methode Electronics
Comment Type **T** Comment Status **D**

lines 39-40 state,

"SIGNAL_DETECT shall be set to OK when the circuitry receives a valid optical signal."

1.0 Unfortunately, most optical transceivers already have a Signal_Detect output. Signal_Detect as implemented in these transceivers cannot reliably indicate the presence of a "valid optical signal". Therefore, we

If you are well versed in the subject of communications system design, you may want to skip or merely scan the material between the dotted lines and go right to the conclusion.

1.1 There are two basic types of signal detect circuits. Both types of signal detect circuitry are insufficient to reliably establish the presence of a "valid optical signal". Some Signal_Detect outputs simply indicate the presence of light above a certain level. These circuits are very easy to design and implement. They only require a bias resistor, a reference voltage and a comparator. They will still respond positively even if there is no modulation of the optical input (i.e. CW optical input).

1.2 Another type of signal detect responds to the amplified electrical output of the optical detector. These are further divided into three subgroups. The first is a simple AC rectifier circuit which compares the AC rectified voltage against the DC average value of the detected and amplified optical input. When the difference exceeds a certain threshold, a comparator sets the SD logical output to "TRUE".

1.2.1 Type 1 as described above suffers from a different problem. If there is no optical modulation, the circuit could respond to random noise or spurious signals generated in the receiver amplifier chain. Because the receiver needs to respond to optical signals at or below 10uW, there is a tremendous amount of power gain (in a typical receiver ~ 60dB) depending on the choice of AGC or limiting amplifier. Since the Type 1 SD circuit cannot discriminate between noise, spurious signals (oscillations) and valid optical pulses, it is possible for the Type 1

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SD to generate false positives.

1.2.2 Type 2 attempts to resolve some of the problems of the Type 1 circuit by adding a matched filter to the AC rectifier circuit. This optimal bandpass filter passes the 800ps GbE pulse relatively unattenuated, and filters out noise and spurious signals not in the passband of the filter. This type of circuit greatly increases the reliability of the SD logic.

Of course, Type 2 has its limits. None of the currently available optical transceivers employ such a filter. Additionally, not all valid optical pulses are 800ps in duration. By choosing the appropriate time constant for the AC rectifier circuit, we can deal with this problem.

More worrisome is the potential for auto-induced false triggers of the SD detect output in a transceiver module. Because of the very high gains in the small package, there is the possibility of crosstalk from the transmitter coupling into the receiver chain and triggering the SD comparator.

1.2.3 Type 3 adds circuitry to detect a characteristic pattern in the signal. In addition to the matched filter, we can add a multi input AND gate which looks in parallel at the serial data output as it streams by. When a common pattern is detected (e.g. K28.5), the SD logic is set to "TRUE". This type of SD circuit has the greatest processing gain of all, and is inherently the most reliable.

Even the Type 3 has limitations which make it in practice no better than the Type 2 when implemented inside the small optical transceivers common in today's implementations. Because of the intimate association of an optical transmitter and receiver in a small package, a degree of cross coupling can be expected. The high gain of the receiver creates the possibility of a false SD "TRUE" output.

Since none of the present transceiver manufacturers implement the more reliable Type 2&3 circuits anyway, we must distinguish between the SD as presently implemented and the one which is desired to be "set to OK when the PMD circuitry receives a valid optical signal."

Suggested Remedy

1.3 I propose the following solution. Leave Signal_Detect as it is. Since it is defined somewhat differently by all the transceiver manufacturers anyway, allow each to implement it according to their current rules.

If we use the capabilities of our SERDES chips we have both the Type 2&3 Signal_Detect already implemented. Deserializers

implement clock recovery with a phase locked loop. Most of these PLLs use a phase-frequency discriminator. Most also have a Lock_Detect output which indicates if the PLL has acquired phase lock on the incoming signal. This is the equivalent of a Type 2 SD as described above. The PLL is operating as a high quality synchronous filter (translate: bandpass filter in the frequency domain). Therefore, Lock_Detect indicates the presence of 800ps pulses.

Deserializers also commonly implement a Comma_Detect circuit to assist in framing. This type of data pattern detect is the same as Type 3 described above.

Ultimately, the most reliable Signal_Detect would be a logical combination of an optical power detect from the optical module and the Lock_Detect and Comma_Detect outputs of the SERDES. I am not 100% sure all SERDES vendors employ a phase/frequency discriminator in their PLL circuits, so we could eliminate the Lock_Detect if it is not universal. We could also leave open the option of optical power detect or rectified AC signal detect since there is no universal agreement on this topic.

I propose we rename the 38.2.4 clause "PMD Signal Integrity" and define it as the logical "AND" of Comma_Detect from the SERDES and Signal_Detect from the optical transceiver.

Then it will be possible to claim as we desire in line 40 the existence of a "valid optical signal".

Proposed Response

O

Pat Gilliland

Methode Electronics

5

power is below -30 dBm."

In the table on page 38.5 line 22 there is note b which states,

"b. The SIGNAL_DETECT values in this table are generated by processing the 8B/10B character signal through an AC coupled receiver. The SIGNAL_DETECT values should respond to the amplitude of the 8B/10B modulation signal and not respond

These two statements are contradictory. In one place we are asking for a threshold which is based on the optical power of -30dBm, yet we specify in note b the SIGNAL_DETECT shall not respond to optical power.

The desired -30dBm limit is most certainly indicative of the average optical power. Optical power meters do not respond to peak power. Optical power meters do respond directly to average optical power.

SuggestedRemedy

Eliminate note b. The particular method used to derive the SIGNAL_DETECT power indication is of no consequence to the end user. The optical receiver vendors are responsible for engineering the necessary circuits. The preferable way is a direct indication of optical power.

Proposed Response

CI 38

SC 38.2.4

P38.4

L 41

6

Pat Gilliland

Methode Electronics

Comment Type T *Comment Status* D

The statement I object to is,

"Examples of a FAIL condition are when the link is unplugged or the transmitter to which it is attached is changed to the OFF state."

Any reference to an "OFF" state for the optical transmitter anticipates there is some mechanism for creating such a state.

The vast majority of optical transceivers being sold into the GbE market today have no such "OFF" control inputs.

SuggestedRemedy

Remove any references to an "OFF" state for an optical transmitter in the standard. Line 41 should read,

"An example of a FAIL condition is when the link is unplugged."

Proposed Response *Response Status* O

CI 38

SC 38.3

P38.5

L 42

45

Joe Gwinn

Raytheon

Comment Type T *Comment Status* D

In Table 38-2, we fail to specify that by "modal bandwidth", we mean overfilled launch bandwidth as measured using TIA/EIA <whatever>, or even to mention overfilled launch. By contrast, Table 38-5 (on page 38.8) and Table 38-9 (page 38.10) do mention overfilled launch.

SuggestedRemedy

Add words to say, either directly or by reference, that we mean overfilled launch bandwidth as measured using TIA/EIA <whatever>.

Proposed Response *Response Status* O

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Mike Dudek Cielo Communications # 99001
Comment Status R RESUBMITTED

With the recent changes to output power in single mode fiber there is a large unallocated margin in the link power budget. The RIN12 specification is much tighter than is necessary for single mode operation.

SuggestedRemedy

This comment has been recycled from Draft D4.1 (was #49) Page and Line numbers refer to D4.1.
Change the single mode column specification for RIN on line 23 table 38-7 from "-120" to "-116".
Also change page 38.9 the single mode column on table 38-9 line 34 (Link power penalties) from "1.20" to "1.30" and the unallocated margin for the single mode column on line 35 from "3.26" to "3.16"

Proposed Response Response Status U
REJECT.

- 1. It was established when the -120 dB/Hz specification was set that vendors could easily meet this specification.
- 2. Even if there is more than adequate margin in the LX SMF link to relax the RIN specification, this change would impact the margin for the MMF cases where the ISI

Motion to adopt this response 9-mar-98 8:28 pm: Y:11 N:3 A:8

Joe Gwinn Raytheon
Comment Status R RESUBMITTED

Note b to table 38-7 fails to fully drive the nail home on why one should avoid radial overfilled launches.

This comment has been recycled from Draft D4.1 (was #60) Page and Line numbers refer to D4.1.
Add a sentence saying that the point is to reduce the fraction of the total optical flux carried in mode groups that pass through the centerline defects found in all practical multimode fiber.

Proposed Response Response Status U
REJECT.

Given the use of offset jumpers, Radial Over-Filled Launches are no longer an issue for 1000BASE-LX on MMF, thus the note can be deleted.

Delete note b under table 38-7.

[Editor's note: During the PMD meeting, there were no objections to this response]

[Editor's note: By deleting the entire note b in table 38-7, Mr. Gwinn's comment has been rendered moot. However, a similar note exists in the SX table 38-3 which was not specifically called out in Mr. Gwinn's comment. We are recirculating this comment at this time to ensure that this issue is widely understood. Regarding Mr. Gwinn's proposed changes, it is the policy of 802.3z to be definitive in our standards, but not to make unnecessary tutorial statements. The proposed changes would have been tutorial in nature.]

Cl 38 SC 38.4.1 P38.9 L2 # 72
Paul Kolesar Lucent Technologies

Comment Type E Comment Status D
Inconsistent terminology.

SuggestedRemedy

Change "singlemode fiber offset launch" to "mode conditioning hybrid".

Proposed Response Response Status O

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73
 Lucent Technologies
 Inconsistent terminology.
 Delete "SMF offset-launch".
 Proposed Response

Joe Gwinn Raytheon
 Comment Status D
 The description of mode conditioning jumpers and their use is a bit confusing, as it seems to imply that one uses the offset-launch jumper fiber at both transmitter and at receiver, which is not correct, and thus appears to conflict with Figure 38-8 on page 38.22. In fact, the duplex jumper contains one ordinary fiber plus one mode-conditioning fiber.
 SuggestedRemedy
 Add the word "duplex" between "conditioning" and "hybrid", so the first sentence reads "... mode conditioning duplex hybrid patch cord, ...".
 Add a sentence saying that only the outbound (transmit) fiber of the duplex does any mode conditioning at all, and that the inbound (receive) path is plain vanilla multimode fiber, and referencing Figure 38-8.
 Proposed Response Response Status O

CI 38 SC 38.4.1 P38.9 L7 # 76
 Paul Kolesar Lucent Technologies
 Comment Type E Comment Status D
 Most values in Table 38-7 are redundant.
 Simplify Table 38-7 by merging redundant cells across columns. Retain separate cells for entries with different values. See Table 38-4 for example.
 Proposed Response Response Status O

CI 38 SC 38.4.2 P38.10 L 21 # 57
 Dan Brown AMP
 Comment Type T Comment Status D
 Inclusion of "Vertical eye closure penalty" in Table 38-8 is inconsistent with rest of table which specifies receiver characteristics. Vertical eye closure penalty is not a receiver characteristic, it is a test condition for measuring stressed receive sensitivity.
 SuggestedRemedy
 1) Remove Vertical eye closure penalty from Table 38-8 and add footnote "C" associated with Stressed receive sensitivity which states "Stressed receive sensitivity measured with 2.6 dB vertical eye closure penalty".
 2) Add footnote "C" associated with Vertical eye closure penalty which states "Vertical eye closure penalty is a test condition for measuring Stressed receive sensitivity. It is not a required characteristic of the receiver".
 Proposed Response Response Status O

CI 38 SC 38.4.2 P38.10 L 48 # 62
 Dan Brown AMP
 Comment Type T Comment Status D
 The channel insertion loss numbers for 1000BASE-LX have been calculated incorrectly. They are stated correctly in Table 38-11.
 SuggestedRemedy
 Replace current values for channel insertion loss given in Table 38-9 with following values " 2.32; 2.32; 2.32; 4.5". For each column, increase unallocated margin in link power budget accordingly.
 Proposed Response Response Status O

CI 38 SC 38.4.3 P38.10 L 42 # 74
 Paul Kolesar Lucent Technologies
 Comment Type TR Comment Status D
 Wavelength of modal bandwidth not specified.
 SuggestedRemedy
 Change "modal bandwidth (minimum, overfilled launch)" to "Modal bandwidth @ 1300 nm (minimum, overfilled launch)".
 Proposed Response Response Status O

P802.3z Draft 4.2 Comments

Dan Brown AMP # 77

Comment Status **D**

Terminology is not used in a consistent manner throughout this clause, leading to confusion for the reader.

SuggestedRemedy

In order to make subclause 38.6.11 more clear and concise, suggest the following changes:

Change title of subclause 38.6.11 to "Test signal at TP3 for receiver conformance testing."

Change the first sentence of clause 38.6.11 to read "Receivers conforming to the stressed receive sensitivity requirements of clause 38.6.7 and the total jitter requirements of clause 38.6.8 shall use a signal at TP3...".

Change second sentence to read "The conformance test signal shall be generated using the short continuous random test pattern defined in Clause 36A.5, and is conditioned..."

Change the title of Figure 38-5 to read "Apparatus for generating receiver conformance test signal at TP3".

Proposed Response Response Status **O**

CI 38 SC 38.6.12 P38.16 L 21-51 # 81

Comment Type **T** Comment Status **D**

The test procedure for measuring receiver 3 dB electrical upper cutoff frequency is not developed sufficiently. Since this is an entirely new test which is not officially documented elsewhere, the procedure needs to be more formal in nature. In other words, it needs to look more like an FOTP with specific step by step instructions.

For example the current procedure instructs the reader to calibrate out the frequency response of the laser and modulator yet gives no clue how to do it. It tells the user to convert from optical to electrical dB but provides no equation to perform such a conversion. See suggested remedy below for specific recommendations.

SuggestedRemedy

Suggest replacing current text in section 38.6.12 with following in order to make the test procedure more formal:

"Measurement of the receiver 3 dB electrical upper cutoff frequency shall be performed using the test setup shown in Figure 38-6. This test involves measuring the receiver amplitude vs. frequency characteristics using a digital data signal with an analog RF signal added asynchronously to the data pattern. The data pattern used is the short continuous random test pattern defined in clause 36A.5. Due to the labor intensive nature of this test, computer instrument control and software automation is recommended to reduce the cycle time for each device tested. The upper 3 dB upper cutoff frequency is determined using the following steps a through f.

a) In order to obtain an accurate measurement, the frequency response characteristics of the test equipment including the RF signal generator, RF power combiner, and laser source must be calibrated out of the final measurement. In practice, this is done by substituting a high speed analog O/E converter for the DUT and a network analyzer for the BERT in Figure 38-6. The pattern generator is not required for this purpose.

Using the network analyzer to control the RF signal generator, sweep the RF signal over a range of frequencies corresponding to the expected 3 dB electrical upper cutoff frequency of the receiver to be tested (an added margin of several hundred Megahertz is recommended). At periodic frequency intervals, use the network analyzer to measure and record the optical power amplitude (dBm) vs. frequency of the test system.

b) Adjust the test equipment configuration as shown in Figure 38-6. Care should be taken to minimize any changes to the signal path which would effect the system frequency response after the calibration (step a) has been performed. Using the pattern generator, modulate the laser source with the specified data pattern. With no RF modulation applied, set the optical power to the stressed receive sensitivity level in Table 38-4 for 1000BASE-SX receivers and in Table 38-8 for 1000BASE-LX receivers. Ensure that the laser source extinction ratio is adjusted for worst case conditions (9 dB).

c) Using the BER tester, perform a clock-to-data alignment function in order to locate the center of the received eye. Apply RF modulation to the laser source while maintaining the same average optical power level established in step b.

d) Sweep the RF signal generator over the same range of frequencies used to calibrate the

P802.3z Draft 4.2 Comments

CI 38 SC 38.6.3 P38.12 L 4 # 49
 Joe Gwinn Raytheon

Comment Type E Comment Status D

The description of extinction ratio measurement is confusing, in that the section number "36A.5" is first (wrongly) read as the name of a repeated Fibre Channel 10-bit symbol used as a data pattern.

SuggestedRemedy

Change the sentence to read: "... the node transmitting the data pattern specified in 36A.3."

Proposed Response Response Status O

CI 38 SC 38.6.3 P38.12 L 7 # 3
 Brad Booth Jato Technologies

Comment Type E Comment Status D

Note references K28.7, but K28.7 has been removed from proceeding paragraph.

SuggestedRemedy

Delete or update note.

Proposed Response Response Status O

f) The receiver 3 dB electrical upper cutoff frequency is that frequency where the corrected RF modulation amplitude increases by 3 dB (electrical)."

I realize that this proposal is not perfect however I believe it comes much closer to representing a formal test procedure than what we currently have. At the interim meeting it should be possible to fill in the few remaining blanks which would allow this revised procedure to be included in Clause 38.

Proposed Response Response Status O

CI 38 SC 38.6.3 P38.12 L 4 # 12
 Del Hanson Hewlett-Packard Co.

Comment Type E Comment Status D

During the editing process for D4.2, the test pattern to be used for extinction ratio measurements was mistakenly changed from "repeating K28.7" to "36A.3". It should have been changed to "36A.2". Maintaining the note on line 7 referencing K28.7 confirms that there was no intent to change the line code.

SuggestedRemedy

On page 38.12, Line 4, change 36A.3 to 36A.2.

Proposed Response Response Status O

CI 38 SC 38.6.3 P38.12 L 7 # 50
 Joe Gwinn Raytheon

Comment Type E Comment Status D

The note about how repeated K28.7 generates a 125-MHz square wave appears to have been overcome by events, both because 36A.3 calls out a different pattern, K28.5, and because such notes probably are better kept in section 36A anyway.

SuggestedRemedy

Move the 125-MHz note to section 36A.2 (not 36A.3).

Add like notes where possible in section 36A, removing them from wherever they are scattered around in the main text. Section 36A.1 comes immediately to mind.

Proposed Response Response Status O

P802.3z Draft 4.2 Comments

Joe Gwinn Raytheon # 51

Comment Status **D**

This note giving the reference to ITU-T G.957 as the source for the fourth-order Bessel-Thompson filter puts us into a bit of a quandry, and does not solve the original problem that this reference was added to solve: Which is normative, the text of section 38.6.5, which levies an impossible requirement in that no actual filter can implement a mathematical ideal, or is it Annex 1 of ITU-T G.957? Strict reading of section 38.6.5 says that it's still the impossible mathematical ideal.

SuggestedRemedy

In line 31, remove the "shall". Reword section to make it informative, and also to make the referenced Annex 1 of ITU-T G.957 normative. Or, reword the entire section such that it levies an achievable requirement.

Proposed Response Response Status **O**

CI 38 SC 38.6.6 P38.12 L 10 # 99003
Joe Gwinn Raytheon

Comment Type **TR** Comment Status **R** RESUBMITTED

What change was made in line 9? There is a change bar, but no evidence of a change. It looks like the fix made to answer my prior TR saying that use of the equation should be mandated failed to make it into the text, in spite of the WG vote to accept the change.

SuggestedRemedy

This comment has been recycled from Draft D4.1 (was #61) Page and Line numbers refer to D4.1.
In line 10, change the "should" to "shall".

Proposed Response Response Status **U**

REJECT.

[Editor's note: We have checked our records and believe Mr. Gwinn is mistaken in his understanding of the committee's previous action. The comment to which he refers is D4/#92. This comment was considered at our Feb. 2-3 interim meeting in Seattle, WA.]

The previous response to this same comment at the February interim meeting (comment D4/#92) was:

PROPOSED REJECT.

If the specified transmitter rise/fall times can be achieved using a filter to meet the transmit eye mask, there is no need to remove the response-time characteristic of the filter.

This PROPOSED REJECT response to #92 was accepted by acclamation, as noted in the minutes of the PMD meeting.

[Editor's note: the effect of the previous committee action was to NOT accept Mr. Gwinn's comment. We cannot explain why he believes the committee voted to accept his change. No change was made to the document as a result of his comment. In light of Mr. Gwinn's new comment D4.1/#61 (this comment) the committee took up the issue once again at our plenary session Mar. 8-12 in Irvine, CA. After careful consideration, a motion was brought forth to re-affirm our previous response to Mr. Gwinn.

The results of that motion were: Y:24 N:0 A:2
The commenter has indicated verbally to the PMD chairman that he is satisfied with our response, however, to ensure that any lingering issues surrounding this comment are widely understood we are choosing to recirculate this comment at this time.]

[Editor's note: In answer to the commenter's first question, there was no change made in line 9, the change bar at that location is merely an artifact of the FrameMaker DIFF utility used to produce this draft.]

59

Comment Status D

Deterministic jitter measurement continues to reference the use of a K28.5 character, yet other subclauses now reference the test patterns of Annex 36A.

SuggestedRemedy

Suggest adding the following statement after the first sentence: "The test shall utilize the mixed frequency test pattern specified in 36A.3."

Suggest replacing lines 37 - 38 with following statement "The method utilizes a digital sampling scope to measure actual vs predicted arrival of bit transitions of the 36A.3 data pattern."

Proposed Response Response Status O

Dan Brown AMP Comment Status D

They are stated correctly in Table 38-11.

SuggestedRemedy

Replace current values for channel insertion loss given in Table 38-5 with following values " 2.33; 2.53; 3.25; 3.43". For each column, increase unallocated margin in link power budget accordingly.

Proposed Response Response Status O

CI 38 SC 38.8.2 P38.18 L 5 # 26 Steven E. Swanson Corning Inc.

Comment Type E Comment Status D

Isn't there another step in the process for international recognition? I understood that IEEE standards, while intended for international standardization, are not initially considered International Standards until further processing.

SuggestedRemedy

Delete "International"

Proposed Response Response Status O

CI 38 SC 38.9 P38.18 L 16 # 27 Steven E. Swanson Corning Inc.

Comment Type E Comment Status D

Since external mode conditioning is not required for SX, there is no need for labeling it.

SuggestedRemedy

Delete "c) Type of external mode conditioning required (if applicable)."

Proposed Response Response Status O

CI 38 SC 38.9 P38.18 L 24 # 28 Steven E. Swanson Corning Inc.

Comment Type E Comment Status D

Since mode conditioning patchcords are required for LX, the labeling should note it.

SuggestedRemedy

Delete "... (if applicable)."

Proposed Response Response Status O

CI 38 SC 38.9 P38.18 L 7 # 20 howard frazier cisco systems, inc.

Comment Type E Comment Status D

This subclause describes PMD labeling requirements, not PHY labeling requirements.

SuggestedRemedy

Change title of subclause to read "PMD labeling requirements".

Proposed Response Response Status O

CI 38 SC Annex 38A P38.31 L 10 # 39 Steven E. Swanson

Comment Type E

The Editor's notes are confusing; Is the Annex staying or not?

SuggestedRemedy

Default: Delete Annex 38A unless needed.

Proposed Response

40

Comment Status **D**

This Annex was useful at one point in the development of the proposed standard. However, given the current requirements for operation over the installed base of fiber with overfilled launch bandwidth specifications, Annex 38B is no longer necessary

Suggested Remedy

Delete Annex 38B.

Proposed Response

Response Status **O**

howard frazier cisco systems # 55

Comment Status D

The text and table describing the Signal Detect function is unnecessarily complex, and subject to misinterpretation. The essential requirements are not obvious, and there is a certain amount of redundancy.

SuggestedRemedy

Replace all of 39.2.3 with the following:

39.2.3 PMD signal detect function

The PMD Signal Detect function shall report to the PMD service interface, using the message PMD_SIGNAL.indicate(SIGNAL_DETECT) which is signaled continuously. PMD_SIGNAL.indicate is intended to be an indicator of electrical signal presence.

The SIGNAL_DETECT parameter shall be set to FAIL under the conditions defined in Table 39-1. The SIGNAL_DETECT parameter shall be set to OK under the conditions defined in Table 39-1, provided that the electrical input is generated by an appropriate electrical transmitter which is transmitting 1000BASE-X code-groups as defined in this standard.

Under all other conditions, the value of the SIGNAL_DETECT parameter is unspecified. This standard imposes no response time requirements on the generation of the SIGNAL_DETECT parameter.

Table 39-1 SIGNAL_DETECT value definition

Receive Conditions	Value
$V_{input,Receiver} < (\text{receiver sensitivity} + \text{worst case local system noise})$	FAIL
$(\text{Receive Sensitivity} + \text{local system noise}) < \text{or} = V_{input,Receiver} < \text{Minimum differential Sensitivity}$	unspecified
OR	
$V_{input, receiver} > \text{Maximum differential input}$	
$\text{Minimum differential sensitivity} < \text{or} = V_{input,Receiver} < \text{or} = \text{Maximum differential input}$	OK

As an unavoidable consequence of the requirements for the setting of the SIGNAL_DETECT parameter, implementations must provide adequate margin between the input optical power level at which the SIGNAL_DETECT parameter is set to OK, and the inherent noise level of the PMD due to cross talk,

power supply noise, etc.

Various implementations of the Signal Detect function are permitted by this standard, including implementations which generate the SIGNAL_DETECT parameter values in response to the amplitude or average power of the 8B/10B modulation of the electrical signal.

Proposed Response *Response Status* O

CI 39 SC 39.3.3 P39.8 L 6 # 19
 howard frazier cisco systems, inc.

Comment Type T **Comment Status D**

As a result of the changes to the jitter budget in clause 38, the NOTE which appears below table 39-5 is no longer true, and it was never very useful in any case.

Delete the note which appears on line 6 of page 39.8

Proposed Response *Response Status* O

CI 39 SC 39.3.3 P39.8 L 6 # 42
 Doug Day VLSI Technology

Comment Type E **Comment Status D**

The note, "The jitter specifications for TP1 and TP4 in Table 39-5 match ... Table 38-10" is not true since 38-10 has been changed.

SuggestedRemedy

Remove the note on page 39.8, lines 6 and 7.

Proposed Response *Response Status* O